OPTIMIZATION OF PRODUCTION VARIABLES GOVERNING YIELD AND STABILITY OF FACTOR VIII IN CRYOPRECIPITATE

by

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This thesis is submitted in fulfilment of the requirements for the Masters Degree in Technology (Medical Technology) in the School of Life Sciences at the Cape Technikon.

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I declare that this thesis is my own work. It is being submitted for the Masters . Diploma in Technology (Medical Technology) at the Cape Technikon, Cape Town.

It has not previously been submitted for any diploma, degree or examination at any other institution. This study was carried out at Western Province Blood Transfusion Service.

In this research the statistical planning and analyses, and recommendations arising from these analyses, have been done with the support of the Institute for Biostatistics of the Medical Research Council.

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4.11.97

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Date

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"The people who get on in life are the people who get up and look for the circumstances they want and if they can't find them, they make them"

George Bernard Shaw (1856 - 1950)

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LIST OF ABBREVIATIONS

ABBREVIATIONS	FULL NAME
AABB	American Association of Blood Banks
ACD	Acid citrate dextrose
ALB	Albumin
ALT	Alanine Aminotransferase
Са	Calcium
Ca⁺⁺	calcium ions
CaCl ₂	Calcium chloride
CI	Chloride
CPD	Citrate phosphate dextrose
CPDA-1	Citrate phosphate dextrose adenine
CPDA-2 (0.5)	Citrate phosphate dextrose adenine (half strength)
CPU	central processing unit
°C	degrees celsius (unit of temperature)
da	daltons
C.V.	coefficient of variation (statistical term)
DCL	Diagnostic Chemical Limited
DF	degrees of freedom (statistical term)
EDTA	Ethylenediaminetetraacetic acid

ABBREVIATIONS	FULL NAME
ELISA	Enzyme linked immunoassay
factor	component of the fractional factorial design
FDP	Fibrin degradation products
FVIII	Factor VIII
FIX	Factor IX
F value	Variance ratio (statistical term)
БрА ГрА	Fibrinopeptide A
9	gram (unit of mass)
g/l	gram per litre
<	less than
НМК	high molecular weight kininogen
HCL	Hydrochloric acid
IS	International standard
IU/ml	International unit per millilitre
kb	kilobase
К	Potassium
>	greater than
М	Molar (unit of concentration)
mEq/l	milli equivalent per litre
Mg	Magnesium

ABBREVIATIONS	FULL NAME
	milligram (unit of weight)
mol/l	mole per litre (unit of volume)
ml	millilitre (unit of volume)
mm Hg	millimetre of mercury
mM	milli Molar (unit of concentration)
mmol/L	millimole per litre (unit of concentration)
MRC	Medical Research Council
mRNA	messenger Ribonucleic acid
NaN ₃	Sodium nitrate
Na	Sodium
NIBSC	National Institute for Biological Standards and Control
nm	nanometre (unit of wavelength)
%	percent
p	probability (statistical term)
PBS	phosphate buffered saline
рН	negative logarithm ಲ್ hydrogen ion activity
PL	phospholipid
SD	standard deviation (statistical term)
Sec	seconds

ABBREVIATIONS	FULL NAME
ТР	Total protein
SE	standard error (statistical term)
μ	micro litre (unit of volume)
µg/ml	micro gram per millilitre
U/di	units per decilitre
U/ml	units per millilitre
variable	key elements being measured in the study
VIII:Ag	Factor VIII antigen
VIII:C	Factor VIII activity
VIII	Factor VIII protein
v/v	volume per volume
vWF	von Willebrand Factor
vWF:Ag	von Willebrand Factor antigen
w/v	weight per volume
WFH	World Federation of Haemophilia
WPBTS	Western Province Blood Transfusion Service
XL-FDP	cross-linked fibrin degradation products

<u>SUMMARY</u>

Cryoprecipitates are used as the raw material for the preparation of Factor VIII (FVIII) for replacement therapy for haemophiliacs. Routinely, cryoprecipitate only recovers 50% of the Factor VIII in the plasma. The purpose of this study, production of cryoprecipitate, was to investigate those variables which play a key role in determining the yield of Factor VIII present in cryoprecipitate. Cryoprecipitate production involves a wide range of variables which could effect the final outcome of the product. These vary from the donor blood group, time of donation, exercise levels of the donor, to a time delay prior to processing, temperature storage conditions, to the method utilised for plasma freezing and thawing. The objective was to explore which combination of variables in the procedure would lead to a process which would optimize the preparation of cryoprecipitate in a routine environment, to yield the highest levels of Factor VIII.

Frequently in scientific investigations, particularly when a practical approach has to be adopted, questions arise in which the effects of a number of different variables in a process, require evaluation. Such questions can usually be most economically investigated, by arranging the analysis according to an ordered plan in which all the factors are viewed in a regular way. Provided the plan has been correctly chosen, it is possible to determine not only the effect of each individual variable, but also the way in which each effect depends on the other factor, by means of an interaction. This makes it possible to obtain a more complete picture of what is happening, than would have been obtained by varying each of the

(xxi)

variables one at a time while keeping the others constant. Designs of this sort lend themselves well to statistical analysis, and provide their own estimates of experimental error. This type of statistical analysis called, 2^K Fractional Factorial Experimental Design, forms the basis of this study in which 14 key variables in the production process of cryoprecipitate were defined as possible areas in which Factor VIII levels in the cryoprecipitate are effected.

Key variables have been identified on an individual basis in previous studies (Burka *et al.*, 1975), however this blended approach to optimise the key variables within the production environment, and define further combinations which could be incorporated into the production, has never been attempted.

The statistical design used in the study was compiled by the Institute for Biostatistics of the Medical Research Council (MRC). Units of blood were collected and processed, from blood donors under the stipulated criteria, corresponding to the study design. The pre, post and final samples obtained were analyzed against selected appropriate assays. The results of all the assays were statistically analyzed by the Institute for Biostatistics at MRC. The results are all tabulated by way of a statistical analysis, with their probability significance portrayed. Significant interactions between the factors were identified.

It is clear from this work that certain factors within the variables are more critical to the cryoprecipitate production than others. Significant variables identified in the FVIII assay, prior to separation of the plasma were, the type of primary anticoagulant used, being that of citrate phosphate dextrose (CPD), in conjunction with a preprocessing time of under six hours with the whole blood maintained at a temperature of 20°C. Of secondary importance, was the duration of the bleed, only if consideration was also given to the donor blood group. Of benefit during the production phase, was a rapid freezing temperature of >-60°C.

The fibrin degradation product assay (FDP) demonstrated the usefulness of performing this assay as an indication of FVIII activation at the time of donation, caused by the technique utilised to insert the donation needle into the vein. The results highlighted that there are seventeen (17) steps in the FVIII production process, to which attention to detail should be paid to optimize yields. Interestingly, WPBTS already comply with twelve (12) of the conditions. Further improvement could be obtained if:

- * only blood Group A donors were bled
- * blood were allowed to reach 20°C prior to separation
- * Fibrinopeptide A (FpA) assays were performed
- * a fast freezing rate (>-60°C) was implemented
- * the starting plasma volume was uniform.

Achievement of the above variables and their factors, not currently used, would determine the optimal production cycle and provide the increased yield of Factor VIII in cryoprecipitate production, this study set out to achieve.

CHAPTER 1

INTRODUCTION

Blood of a haemophiliac is deficient in Antihaemophilic Factor, or better known as Factor VIII. This deficiency can be partially corrected by transfusions of a plasma component, termed cryoprecipitate which contains the Factor VIII. Cryoprecipitate is the cold soluble precipitate obtained from thawed plasma. Factor VIII concentrates are prepared from a number of pooled cryoprecipitate, used in home treatment for haemophiliacs. The better the FVIII quality and yield, the fewer number of cryoprecipitates are required per pool, thus reducing cost and decreasing the donor exposure rate per infusion. This in turn, reduces the infusion risk to the patient.

Factor VIII is a labile coagulation factor which deteriorates rapidly when removed from the human body. Variables influencing the recovery of cryoprecipitate from the plasma are numerous. Improvements in transfusion and fractionation techniques in recent years, have made it possible to produce Factor VIII (FVIII) from blood, while preserving other components in the plasma for fractionation into further products, for use by other patients. The cost of haemophilia treatment relates mainly to the costs involved in producing a product that is of adequate quality, and sufficient in supply (Biggs *et al.*, 1974).

Cryoprecipitate production involves a wide range of variables which affect the final outcome of the product. These extend from variables pertaining to the donation criteria through to the final freezing stages in the production cycle. Variables specific to the blood donation procedure are, donor blood type, exercise levels of the blood donor prior to donation, type of primary anticoagulant used, length of time taken to bleed the unit of blood, time delay prior to separation of the red cells and plasma, and temperature of the blood at the time of separation. Variables which influence the production processing cycle revolve around freezing and thawing temperature, freezing and thawing techniques, precipitation and centrifugation methods. These variables listed above were my choice for the study. Variables chosen for the study were those that could be controlled, whereas those that could not be controlled or remained constant, were excluded.

Since the advent of cryoprecipitate production initiated by Pool in 1964, there has been an active interest by a myriad of researchers, on various aspects of Factor VIII production. Variables influencing the recovery of labile coagulation from human plasma are numerous. Over the years, many attempts have been made to improve the final yield of FVIII by modifying the method of preparation. Cryoprecipitate production involves many variables, as outlined above (Smith and Hodges, 1984).

Additional variables not included in the study ranged from, donor age, type of collection container, volume of the starting plasma, pH of the plasma, the level of anxiety of the donor, the time from collection to freezing, temperature during centrifugation during the final precipitation of the cryoprecipitate, heat exchange,

and determination of the end point of production, all of which can affect the level of coagulation elements present. These were excluded, as the production specifications for these criteria could be determined and regulated to remain constant throughout the study. As many as 90 variables with their appropriate factors have been identified, which could conceivably affect the final cryoprecipitate yield and quality of FVIII levels. Many of these variables and factors have systematically been individually evaluated by investigators since the discovery by Pool in 1964. Each step of the production process must be meticulously carried out, to ensure optimum proficiency, as it could have a cumulative effect on the final yield. To date, no single investigation on FVIII has ever been reported, where as many as fourteen variables were evaluated simultaneously, by a fractional factorial experimental design. A total of 128 regular, volunteer blood donors all meeting the donation criteria were used in this study. The relevant blood donor base in a specified geographical area was stipulated.

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The purpose of this study was to identify and assess those selected variables with dominant factors, which play a key role in determining the yields and recovery of Factor VIII in cryoprecipitate. In order to achieve this objective fourteen key variables in the bleeding and production process were selected. Six of the variables relate to the blood donor, donation and collection techniques and the handling of the whole blood prior to the separation of the red cells and plasma. The other eight variables are concerned with the production process.

The experimental design used in this study was a 2^K Fractional Factorial Design

compiled up by the Department for Biostatistics at the Medical Research Council. The design was compiled in such a manner that enabled all fourteen variables to be compared with each other, simultaneously by using opposite factors. This type of design requires only a fraction of the total number of treatments in a full factorial design. The design would enable the more significant and dominant factors to be highlighted and provide knowledge on how variables effect the cryoprecipitate quality. With this approach it is possible, in addition to optimizing the key variables and their factors, may reveal any previously unobserved interactions between variables which could further enhance FVIII quality.

The study was conducted within the routine cryoprecipitate production environment at the component processing laboratory of the Western Province Blood Transfusion Service, with the intention of providing guidelines which would be suitable in a routine large scale production process.

Assays selected to evaluate the samples were FVIII and von Willebrand Factor (vWF) assays, fibrinogen, pH determination and fibrin degradation product (FDP) assays. Plasma proteins and electrolyte assays were also performed. All the data was analyzed by means of the statistical method, Analysis of Veriance (ANOVA). The Fractional Factorial Analysis resulted in the analysis of effects and interactions which in turn determined the significant variables with the probability confidence limits set at p = 0.05. The results for significant effects and interactions are presented in a table of means. Selection of FVIII, vWF, pH and fibrinogen assays were based on experience over the years. The selection of the FDP assay was

established as a result of a previous study we researched, whereby early activation of FVIII at the time of phlebotomy can be confirmed. The choice of performing the plasma protein and electrolyte assays was due to the fact that no mention of their effects on FVIII yield had yet been reported. Samples for assay were taken from the blood donors prior to donation (termed pre), after the separation of the red cells and plasma (termed post) and from the cryoprecipitate (termed final).

Factor VIII content of cryoprecipitate varies from one unit to the next, with the average potency fluctuating from day to day, resulting in variations in the production process.

This study was undertaken in order to resolve the **objectives** and answer the **hypothesis**:

- * can the Factor VIII content within the packs of cryoprecipitate prepared from individual blood donors, be made uniform?
- * which variables, such as primary anticoagulant, conditions of freezing and thawing, the interval of time between blood collection and processing and donor variation in FVIII level, affect the quality of FVIII in cryoprecipitate and can the FVIII levels be increased?

* what combination of variables in all the technical steps involved in the procedure, will lead to a process which optimizes the preparation of cryoprecipitate, in a practical blood bank environment i.e. were there any variables which had a dramatic effect upon the Factor VIII yield, such that modification or control of them would protect against a poor quality product?

It has been shown by this work that certain variables with their factors, are more critical to the cryoprecipitate production than others. Significant variables identified in the FVIII assay, prior to separation of the plasma were, the type of primary anticoagulant used, that of citrate phosphate dextrose (CPD), and a pre-processing time of under six hours, with the whole blood maintained at a temperature of 20°C. Of secondary importance, was the duration taken to bleed the unit of blood only if consideration was given to the donor blood group. During the production phase, of benefit was a rapid freezing temperature of more than -60°C.

The Fibrin degradation product assay (FDP) demonstrated the usefulness of performing this assay as an indication of FVIII activation at the time of donation. If activation of FVIII was evident, it could have been caused by the technique utilised to insert the donation needle into the vein.

The results highlighted that there are seventeen (17) steps in the FVIII production process, to which attention to detail should be paid to optimize yields. Interestingly, WPBTS already comply with twelve (12) of the conditions. Further improvement could be obtained if:

- * only blood Group A donors were bled
- * blood were allowed to reach 20°C prior to separation
- * Fibrinopeptide A (FpA) assays were performed
- * a fast freezing rate (>-60°C) was implemented
- * the starting plasma volume was uniform.

Implementation of the above variables, would determine the optimal production cycle and provide the increased yield of Factor VIII in cryoprecipitate production, this study set out to achieve.

Study aim : to standardize the production of cryoprecipitate taking into account the critical variables and their factors in order to define a STANDARDISED PRODUCTION METHOD.

CHAPTER 2

LITERATURE REVIEW

2.1 CLASSIC HAEMOPHILIA (HAEMOPHILIA A)

2.1.1 INTRODUCTION

Haemophilia is one of the commonest of the hereditary haemorrhagic disorders resulting from an abnormality in the activity of one of the blood clotting ingredients. Without normal activity, clotting cannot take place and bleeding is prolonged (Biggs *et al.*, 1974). Knowledge of bleeding disorders affecting male members in certain families was recognized as early as the second century, and also documented in the Talmud (Foster and Zimmerman, 1989).

Haemophilia, at the turn of the century was explained by geneticists, as the presence of an abnormal haemorrhagic disorder, however it was unknown whether the cause of the condition was a cellular or plasma deficiency. In 1911 Addis demonstrated that a prolonged clotting time could be rectified by using the globulin fraction of plasma, although at that time, lack of adequate blood banking facilities made whole blood the product frequently used to treat bleeding episodes. Due to the volumes required, patients' systems were often overloaded causing unsatisfactory recoveries (Aronson, 1990). It is a well known fact that Queen Victoria was responsible for the spread of haemophilia among the European royalty. The first successful treatment of haemophilia patients recorded was with

intravenous infusions of plasma in 1924 (Smit Sibinga, 1996).

Step by step through the twentieth century this inherited sex-linked bleeding disorder, its onset and method of treatment was unravelled. It is now known that haemophilia is caused by the partial or complete absence of an essential coagulation component in the blood, called Factor VIII or Antihaemophilic Globulin. The absence of Factor VIII (FVIII) affects males almost exclusively, knows no geographical boundaries and is transmitted in a sex-linked recessive manner. At present there are two forms of haemophilia recorded: Haemophilia A or Classical Haemophilia, characterized by a deficiency of clotting Factor VIII and Haemophilia B or Christmas Disease which is caused by a deficiency in Factor IX. Approximately one in every 10,000 males in all parts of the world suffers from Haemophilia A. Without treatment, very few boys with haemophilia can survive to adulthood. With proper treatment however, they can expect to lead full, normal lives (World Federation of Haemophilia :WFH, 1994).

2.1.2 GENETIC TRANSMISSION

When a haemophilia male marries a normal woman, a defective \succ chromosome is transmitted to all of his daughters, with the result that they will all be carriers of the defective X chromosome, while all the sons will be normal. However, males born to carrier daughters, have an equal chance of being either haemophiliacs or being normal, and daughters born to female carriers, have an equal chance of being either normal or carriers. It is possible that if a carrier female marries a haemophiliac

that a female child with haemophilia can be produced, however this situation is extremely rare. There are two possible explanations for about a third of haemophiliacs having no family history of the disease. A genetic mutation in either the patient or his mother might have occurred. The other possibility is that the family had very few, or no male children in previous generations, and the defective gene which was carried by female children, did not have the opportunity to express itself in the males (Eipe, 1971).

2.1.3 BLEEDING MANIFESTATIONS

Haemophilia is present at the time of birth and a low Factor VIII level can be detected in the umbilical cord blood of a baby boy with haemophilia. In most instances the first bleeding episode only manifests itself at the age of six to twelve months once the child starts to become mobile. The first injuries are in the form of deep bruises and superficial cuts. Haemarthrosis of the knees and ankles and haemorrhages into skeletal muscles occur when the child begins to walk. People with haemophilia suffer painful episodes of bleeding into the joints and muscles over the years. This eventually results in chronic arthritis in the affected areas, whilst brain haemorrhages can be fatal. With the introduction of r liable methods for determining the level of Factor VIII in the blood, it was found that the severity of the disease correlated with the degree of Factor VIII deficiency. Table 2.1 shows the relationship of blood levels of Factor VIII to the severity of haemorrhagic manifestations (Eipe, 1971). Haemophilia can be classified as severe, moderate or mild according to the FVIII level. The average normal level of FVIII is 100 U/dL; the

normal range is about 50 to 180 U/dL (Kasper, 1995).

Level of Factor VIII (%)	Haemorrhagic Manifestations
50 - 100	none
25 - 50 (mild)	tendency to bleed after major injury
5 - 25 (mild 5 -30 U/dL)	moderate bleeding after operations/injury
1 - 5 (moderate 2-4 U/dL)	severe bleeding after minor injury
0 (severe 1 U/dL)	severe haemophilia with spontaneous bleeding into muscles/joints with crippling effect

Table 2.1. Severity of Factor VIII Blood Levels (Eipe, 1971)

In industrialised first world countries boys born with haemophilia start receiving treatment at an early age. This eliminates life-threatening bleeding episodes and allows them to lead normal, productive lives (WFH publication .1994). In countries where diagnosis and treatment are not available, boys continue to suffer and develop orthopaedic problems and die at a young age. It is estimated that 80% of the world population with haemophilia receive inadequate care. Replacement therapy is provided in the form of intravenous infusions of either processed or fractionated plasma products. The raw plasma product is called cry::precipitate, in which Factor VIII is found. This product raises the patient's Factor VIII concentration to a level of haemostasis, for that particular bleeding episode and maintains this status until healing is achieved.

2.2 FACTOR VIII

2.2.1 NOMENCLATURE

In 1985, new recommendations for the nomenclature of FVIII and von Willebrand Factor (vWF) were formulated by an International Committee on Thrombosis and Haemostasis (Marder *et al.*, 1985). The symbol for Factor VIII protein is VIII and not VIII:C. The symbol for Factor VIII antigen is VIII:Ag and is used for the immunologic measurement of FVIII. The symbol for FVIII activity is VIII:C to be used for the functional measurement of cofactor activity.

The symbol for von Willebrand factor is VWF and the antigen VWF:Ag (Foster and Zimmerman, 1989).

2.2.2 STRUCTURE AND SYNTHESIS

Coagulation FVIII is produced from a 289 kb gene consisting of 26 exons which give rise to a 9 kb mRNA. FVIII is a glycoprotein present in the plasma at a low concentration $(0.1\mu g/m!)$, and has a molecular weight of 2 x 10^6 daltons. Its absence or deficiency results in Haemophilia A. The primary structure contains 2332 amino acids and exhibits a triplicated region of 330 amir o acids (A domains) an unique region of 983 amino acids (B domain), and a carboxyl-terminal duplicated region of 150 amino acids (C domain), that are arranged in the order A1-A2-A3-C1-C2 (Bihoreau *et al.*, 1989 and Masure *et al.*, 1978). Figure 2.1 shows a schematic representation of the structure of FVIII.


Figure 2.1. Linear representation of the amino acid sequence of human Factor VIII. There are three A domain repeats (A1, A2 and A3) and two C domain repeats (C1 and C2) (Foster and Zimmerman, 1989).

The gene controlling FVIII is on the X chromosome. The site of synthesis is unknown. Patients with Haemophilia A lack FVIII and usually lack VIII:Ag. Equally poorly understood is how and where FVIII, which is synthesized as a single- chain polypeptide, is converted to the two-chain molecule found in plasma, with a variable heavy chain molecular weight of 210,00 to 90,000 and a light chain of molecular weight of 80,000. The half-life of FVIII after transfusion is eight to twelve hours (White and Shoemaker, 1989), however *in vivo* investigations have indicated a relatively longer biological half -life of FVIII:C in less purified material such as plasma and cryoprecipitate, than in more purified concentrates. It varies between 10 and 20 hours (mean 13.9 hours) for less pure products, and 4.8 to 20 hours (mean 12 hours) in the more purified group. A Factor VIII half life of less than 7 is not acceptable (Allain, 1984).

FVIII circulates in association with von Willebrand Factor (VWF) which stabilises it. Von Willebrand Factor is found in the plasma, megakaryocytes, platelets and endothelial cells, and is required for normal adherence of platelets to injured vessel walls. It is produced under control of autosomal genes. When measured by an immunological test using specific antibodies, it is known as von Willebrand Factor antigen : VWF:Ag (Kasper, 1995).

2.2.3 COFACTOR FUNCTION

FVIII is involved in the activation of Factor IX. Its function is measured by the FVIII activity assay, in which the end point is the formation of fibrin strands. The molecule can be detected as Factor VIII antigen (VIII:Ag, also called Factor VIII coagulant antigen, VIII:CAg) by an immunologic test using homologic antibodies (inhibitors) to human FVIII. Activated FVIII (FVIIIa) is an essential participant in the intrinsic pathway of coagulation (Foster and Zimmerman, 1989). FVIII is the co-factor of IXa in the activating step that converts X to Xa. Phospholipid and calcium are necessary components of this complex (Kabi Vitrum, 1987). The catalytic efficiency of FVIII is greatly increased by activation of thrombin or Factor Xa. FVIII requires thrombin for activation, but does not result in conversion to an active protein. It is inactivated by further exposure to thrombin and activated protein:C (White and Shoemaker, 1989). The endpoint of the carcade is the rapid conversion of fibrinogen into insoluble fibrin to form a clot around a platelet plug (Burke *et al.*, 1986).

The schematic representation in Figure 2.2, portrays the intrinsic coagulation pathway.



Figure 2.2. Schematic representation of the intrinsic pathway of coagulation illustrating the components of the tenase complex and the prothrombinase complex. Coagulation factors are represented by their Roman numerals. Activated coagulation factors are represented by their Roman numerals followed by a small case a. Other abbreviations: high molecular weight kininogen (HMK); calcium ions (Ca⁺⁺); phospholipid (PL) (Foster and Zimmerman's Scheme, 1989).

2.3 IMPROVING FACTOR VIII STABILITY AND YIELDS IN PLASMA

Until 1960, the only effective treatment available for haemophilia was the infusion of plasma. In 1964 cryoprecipitate became available as a product for treatment (Brodniewicz-Proba, 1991). The endeavour to enhance the levels of FVIII in plasma was pursued. Pool *et al.* (1964) discovered that the insoluble gummy material formed in plasma which had been stored at refrigerator temperatures, contained a high proportion of FVIII when measured. Pool realized that the same phenomenon occurred during the thawing of frozen plasma. The precipitate when reduced to a low volume, provided better therapy for Haemophilia A, than plasma. (Pool *et al.*, 1964). The development of cryoprecipitate and improved production techniques now made available a treatment that was less costly and easier for haemophiliacs to administer (Aledort, 1988). The next two decades saw numerous researchers attempt to enhance the FVIII activity in cryoprecipitate, by improving the numerous variables involved in the production of cryoprecipitate. In presenting the final product in an acceptable form, the formulation of the plasma protein must preserve its biological activity during processing. The production process must maintain the product as close as possible to the normal physiological state and minimize physical loss of activity or structural damage to the proteins during manufacture. These aspects of formulation are important in the preparation of cryoprecipitate, because FVIII is a biological labile component of plasma (McIntosh and Foster, 1990). Changes in the collection and processing of plasma have a direct impact on the FVIII concentration in the cryoprecipitate.

Variables influencing the recovery of FVIII from the plasma are numerous (International Forum, 1983). In the production of cryoprecipitate, there can be up to 90 variables involved, ranging from the blood group of the blood donor to the temperature of the centrifuge during final processing, involving numerous technical production steps. Some of these variables and their corresponding factors influence the final quality of the cryoprecipitate to a larger extent than others. (Pool, 1975). Elimination of the less critical stages are advantageous, thus reducing the number of stages, which require vigilant awareness in the attempt to produce a consistently good product. If the production criteria for the preparation of all the Factor VIII present in the plasma is not possible. Modification of the mode

of preparation, over the years, has been attempted to improve the final yield of FVIII in the cryoprecipitate (Reiss and Katz, 1976). Each step in the production process must be carefully accomplished, in order to obtain optimum proficiency at every step of the operation, which in turn, will have a cumulative effect on the FVIII yield.

2.3.1 HIGH POTENCY CRYOPRECIPITATE FROM EXERCISED BLOOD DONORS

FVIII activity increases significantly as a result of short durations of intense muscular exercise. The mechanism of the rise of FVIII activity after exercise is uncertain, but it is thought it may be due to elevated synthesis of FVIII, activation of FVIII already in circulation or a release of FVIII from body stores (Strand *et al.*, 1974). The elevation of FVIII levels peak shortly after exercise is ceased. The benefit of exercising blood donors prior to venisection as a method to raise FVIII, is acceptable to blood donors and achieves results 40% higher than normal (Van Gastel *et al.*, 1973).

2.3.2 PRE-SELECTION OF DONORS BY BLOOD GROUP

Variations in plasma levels of FVIII in individuals with different ABO groups have been reported in the literature (McLellan *et al.*, 1988). In 1964 Preston and Barr ^{demonstrated} that blood group O persons have notably lower FVIII levels than those persons with blood groups A, B or AB. The reason for the variation between

the ABO blood groups is not understood, as there is no relation between the H secretor status and FVIII levels.(Preston and Barr, 1964).

The plasma of group O blood has been reported to contain only 75% of the activity present in the other blood groups (Tomasulo *et al.*, 1980). Again no explanation for the association between the ABO blood group and FVIII in the plasma could be furnished. The FVIII molecule is a glycoprotein containing the A, B, and H antigenic determinants, and the removal of the carbohydrate may affect FVIII and its related activities (Tomasulo *et al.*, 1980). Similar observations were made by Jeremic *et al.* (1976) and Wahlberg *et al.* (1980). Observations were also made that group A female donors, on oral contraception, yielded the highest FVIII levels (Jeremic *et al.*, 1976). Blood group studies carried out by Carlebjork *et al.* (1986a), confirmed previous findings that blood groups (Carlebjork *et al.*, 1986a). Plasmapheresis of individuals with blood groups other than O was recommended as a collection method to obtain plasma with higher Factor VIII levels.

2.3.3 BLOOD COLLECTION

Venipuncture procedures require that blood collection should be performed with a sterile unused donation blood bag system, containing a new needle. The needle entry into the vein should be a clean cut with a blood flow that is rapid throughout donation, and that the mixing of the blood with the anticoagulant, be continuous. The start and end of the bleeding procedure is critical. In the event of activation of

the coagulation system, as a result of the first millilitre of blood being left without anticoagulant, activation of FVIII could follow (Britten *et al.*, 1966). Activation of the coagulation system can best be detected by the Fibrinopeptide A and Fibrin Degradation Products (FDP) assays. During blood coagulation, fibrinogen is converted to fibrin by the action of thrombin which in turn activate FVIII and FXIII. Assay methods have made it possible to monitor whether activation has occurred (Skjonsberg *et al.*, 1986). Random assay of units of blood provides an indication in the accuracy of the bleeding procedure. It has been shown that there is some correlation between the Fibrinopeptide A (FpA) content in plasma and donation time (Prowse *et al.*, 1984). The amount of Fibrinopeptide A present, serves as an indication of the amount of thrombin generated and indirectly as to the extent of activation of FVIII (Pflugshaupt and Kurt, 1983).

Standards recommended by the American Association of Blood Banks (AABB), require that blood collected for the preparation of cryoprecipitate and platelet concentrates, be collected from blood donors bled within eight minutes or less. To date no further recommendations to alter this have been proposed (AABB Standards, 1988). It was felt that the FVIII activity and platelet yield might be drastically diminished if the blood was collected over a period of time, i.e. longer than 8 minutes due to activation of clotting factors (Reiss and Katz, 1976).

The Fibrinogen/Fibrin degradation products (FDP) and D-Dimer are regarded as one of the most useful parameters available to evaluate the fibrinolytic status and degree of coagulation (Sato *et al.*, 1995). Detection of the different fibrinogen and

fibrin derivatives can help identify whether processes involving thrombin, Factor XIII and plasmin, have occurred in the donated blood unit (Proietti *et al.*, 1990). Fibrin formation can be determined indirectly by the determination of released fibrinopeptides, however these can be difficult to analyze as they have short halflives. The results do not give the same information as direct determination of soluble fibrin (Wiman and Ranby, 1986).

2.3.4 EFFECT OF ANTICOAGULANTS ON FACTOR VIII

2.3.4.1 TYPE OF ANTICOAGULANT

FVIII is a calcium linked protein which may dissociate in the presence of calciumchelating anticoagulants such as citrate, with substantial loss in activity. FVIII:C in plasma anticoagulated by citrate, may be stabilised by restoring plasma ionised calcium to physiological levels, combined with secondary anticoagulation by heparin, in other words, by anticoagulant exchange to heparin from citrate (Cumming *et al.*, 1990). Similar findings were reported by Rock *et al.* (1983) and by Krachmalnicoff and Thomas (1983).

Citrate-phosphate-dextrose-adenine (CPDA-1), used in a 1:8 ratio, is a registered anticoagulant for the collection of whole blood. However, reports by Rock *et al.* (1988) indicate, that by using this ratio allows the citrate present to be far in excess of the requirement to prevent clotting. By reducing the citrate level, the yield of FVIII is increased (Rock *et al.*, 1988). The safety of red cells prepared by

half strength citrate anticoagulant (0.5 CPDA-2) as a therapeutic agent was investigated, with the findings of the study being that CPDA-1 and CPDA-2 were comparable (Murphy et al., 1991). These findings are comparable to those of Prowse et al. (1987) who found that the use of half strength citrate, did not impair standard blood donation, collected into CPDA-2, nor were there any incidents of formation of blood clots. To be a useful anticoagulant, half strength citrate (0.5) should have the ability to maintain red cell viability on storage, to the same standard as is currently available with other anticoagulants (Prowse et al., 1987). Griffin and co-workers (1988) were able to show that by collecting blood into 0.5 CPD-A2, the stability of FVIII in plasma or whole blood stored at room temperature was greatly improved. Recent studies have shown that half-strength citrate CPD solution, improves the maintenance of erythrocyte, 2,3 diphosphoglycerate during storage of red cell concentrates, as well as provides a FVIII output of increased stability and concentration (Suontaka et al., 1996). Contrary to the findings of Rock and Palmer (1985), Smit Sibinga and Das (1984), Krachmalnicoff and Thomas (1983) and Morgenthaler et al. (1985) which all found ACD to be a better primary anticoagulant, an independent study by De Wit et al. (1986), concluded that CPD remained the superior anticoagulant over ACD (acid citrate dextrose) and heparin.

The anticoagulant concentration in ACD and CPDA solutions is almost identical, although the higher FVIII activity in CPDA seems to be due to the preferable pH in the CPDA medium. The pH on collection in both solutions are similar, but FVIII loss occurs in ACD, possibly due to the lack of its buffering capacity (Weisert and Jeremic, 1973). In a study carried out by Foster *et al.* (1988), the loss of FVIII in

the final product was due to a citrate induced inactivation, which was avoided by controlling the concentration of ionised calcium.

FVIII travels as a calcium-linked complex which loses activity in the presence of citrate. When subjected to a stronger chelating substance, this complex dissociates completely and all activity is lost. FVIII has shown increased stability when prepared from plasma containing physiological levels of ionised calcium, obtained by the use of heparin as the anticoagulant. No difference in pH was observed in plasma prepared from heparin or citrate (Cumming et al., 1987). Heparin is a potent, rapid acting anticoagulant that catalyses the inactivation of thrombin (Oman and Tejidor, 1993). It acts to prevent the conversion of prothrombin to thrombin in the final step of the clotting procedure. In 1980, Rock patented the technique of using heparin or sodium heparin as the mode of achieving improved FVIII yields in the production of cryoprecipitate. Heparin as an initial anticoagulant furnishes the means for maximum preservation of FVIII:C (Smit Sibinga et al., 1984). When blood is collected into heparin, and combined with the methodology of thaw-siphon and fast-thaw techniques, an even greater improvement in the yield of FVIII is experienced (Smit Sibinga et al., 1984). Collection of blood in heparin, instead of chelating anticoagulants or neutralization of citrate by the addition of Ca⁺⁺ to heparinized CPD plasma, renders VIII:C significantly stable (Mikaelsson et al., 1983). A too high a concentration of Ca⁺⁺ forms a clot after freezing and thawing. instead of the usual precipitate. FVIII:C loses less activity, if blood is collected either directly into heparin or if citrated blood is heparinized, it must be recalcified within 12 hours of blood collection (Morgenthaler et al., 1985). In order to be able

to recalcify the plasma, it is critical to determine a concentration of calcium chloride, which is as low as possible. A concentration of 10 - 14 mM of calcium chloride is the concentration recommended, higher concentrations catalyze fibrin formation (Adolfsen, 1986).

Fibrinogen and fibronectin are major elements in cryoprecipitate in the presence of heparin. Fibronectin molecules have binding sites for heparin, and in conjunction with the vWF, help amplify the concentration of the precipitate. The fibrinogen content is elevated by heparin (Smit Sibinga *et al.*, 1988). Wallevik *et al.* (1989) proved that by collecting blood into heparin, FVIII activity is improved and that the red cell concentrates and remaining plasma products when infused, show no adverse effects *in vivo*.

FVIII produced from cryoprecipitate collected in heparin, is able to produce a high yield intermediate purity product that is able to be heat treated, however, with detrimental consequences to stability and solubility (Palmer *et al.*, 1990). Measurement of FVIII:C activity can only be carried out in the presence of heparin, if the heparin is removed by neutralization with either polybrene or Cellex T (Morgenthaler *et al.*, 1985). FVIII prepared from heparinized plar ma was found to have poor solubility, whereas cryoprecipitates from citrated plasma with the heparin added after plasma separation has a far better solubility (Morgenthaler *et al.*, 1985). The presence of heparin has an inhibitory effect during the measurement of FVIII. Neutralization of heparin can also be achieved by the use of either protamine sulfate or anion exchange filters. The concept of using enzymes such as

heparinase (Hepzyme) also achieves neutralization of heparin (Oman and Tejidor, 1993). Efficient removal of heparin can be achieved by the use of an anionexchange resin in the form of a tablet (Heparsorb^R). Heparsorb^R incubated with 1 ml of heparinized plasma is capable of rapid removal of heparin from the plasma to allow further evaluation of blood coagulation factors (Cowan *et al.*, 1981). Due to reliability of results reported in the literature, and ease of use, Heparsorb^R is recommended as the assay to follow (Thompson and Counts, 1976).

0.5 CPD-A2 is not a licensed anticoagulant in South Africa, so had to be excluded from the study. On the other hand, although not used as the primary anticoagulant, heparin was considered for use as a comparative factor.

2.3.4.2 INFLUENCE OF pH

Factor VIII is stable in a narrow pH range around 7. It dissociates reversibly in the presence of high salt concentrations (International Forum, 1983). pH and salt concentration can influence the thrombin-fibrinogen reaction (Morrison, 1966). The pH of the plasma influences the stability of FVIII during the collection and storage of blood and maximum stability is achieved at a pH of 6.9. The pH of the anticoagulant solution used is important and should be maintained between 6.7 and 7.0 (Vermeer *et al.*, 1976a). The precipitation stage of the FVIII production should be performed at a slightly acidic pH instead of the neutral pH of 7.0, as an improved product is obtained having better solubility and greater stability (Liu *et al.*, 1980). Similar conclusions were made during a study in Norway (Skjonsberg *et al.*,

1987). pH of heparin solutions are 6.5, while the pH of ACD solutions are 4.9 and that of CPD solutions are 5.5 (Rock *et al.*, 1979b). 40% loss of FVIII activity was experienced if cryoprecipitates were prepared from acidified plasma (Shanberge, *et al.*, 1972).

A rise in pH from 7.2 to 7.7 is experienced when fresh frozen plasma is stored at room temperature for an extended amount of time. This can be explained by the possible diffusion of CO_2 from the polyvinylchloride bags containing the plasma (Smak-Gregoor *et al.*, 1993).

2.3.5 EFFECT OF DELAYED PROCESSING PRIOR TO PRODUCTION

The effect of delaying the separation of the red blood cells from plasma is one of the many variables affecting the final outcome of the recovery of FVIII in the production of cryoprecipitate.

Standards recommended by the American Association of Blood Banks (AABB) require that blood collected for the preparation of cryoprecipitate and platelet concentrates, be collected from blood donors and the plasma sc parated from the red blood cells, and frozen within 6 hours (Hughes *et al.*, 1988).

Several reports by Avoy *et al.* 1978; Burka *et al.* 1975; Slichter *et al.* 1976 and Sohmer *et al.* 1982 demonstrated that delaying refrigeration for up to eight hours only minimally influences the final activity of FVIII. Extension of the holding time

for the units of whole blood, from six to eight hours at room temperature can provide enhanced flexibility in the preparation of cryoprecipitates (Moraff et al., 1990). However, other researchers failed to demonstrate any significant difference between four to six hour old plasma, as well as eighteen hour old plasma as raw materials for cryoprecipitate. The possible explanation is the longer second phase half-life of FVIII (Wensley and Snape, 1980). The delay in the separation of red blood cells and plasma does not prove to be significant unless related directly to whether the whole blood was stored at 4°C or 20°C (Pepper et al., 1978). Storage of whole blood at between 1°C - 6°C is inferior to storage at between 20°C - 24°C, when these temperatures are rapidly imposed on the blood by forced cooling, which in turn could have a detrimental effect on the cryoprecipitate present as well as the resultant FVIII. Storage at 20°C - 24°C does not result in higher risks of microbiological contamination (Allersma et al., 1996). A low citrate content in 0.5 CPD improves the stability of FVIII plasma of whole blood held at room temperature for 8 hours prior to separation (Suontaka et al., 1996).

2.3.6 EFFECT OF PRE-PROCESSING STORAGE TEMPERATURES

FVIII at 4°C decays in a bi-phasic fashion. A rapid decrease of FVI'. with a half-life of five hours is followed by a more stable phase. This accounts for the rapid loss of activity within the first five hours after collection of up to 39%, decreasing to 14% at eighteen hours, with the whole blood being stored at 4°C (Pepper *et al.*, 1978).

In a study by Slichter *et al.* (1976), it was shown that the FVIII yield in cryoprecipitate made from whole blood stored for six hours at 4°C was reduced by 10%. This was also indicated by the instability of FVIII by *in vivo* and *in vitro* studies. Pietersz *et al.* (1989) and Booth *et al.* (1982) reported benefits from the storage of whole blood in a controlled environment at 20°C, prior to the preparation of cryoprecipitate. The temperature of the whole blood was rapidly cooled to the ambient temperature of 20°C. FVIII levels were well preserved at 24 hours with recoveries of 80%, compared to a yield of only 65% at 4°C. This was a significant finding, as for the first time it permitted blood collected at donation facilities, to be transported overnight to the production centres and processed the next day, without refrigeration of the whole blood.

2.4 IMPROVING FACTOR VIII RECOVERIES DURING PROCESSING

The potency of cryoprecipitate is affected partially by the technique of processing and partially by donor elements (Kasper *et al.*, 1975).

2.4.1 THAWING OF FACTOR VIII IN RELATION TO TEMPERATURE.

The thawing conditions of frozen plasma determine the FVIII recovery. When thawing is carefully controlled in rate, heat exchange and timing, the non-cold precipitable constituents redissolve, leaving the cryoprecipitate in a gel state. The cold-insoluble cryoprecipitate shows a temperature range over which solubility changes from the gel phase to complete resolution. Literature reports that the differences observed in the FVIII activity when using the "refrigerator-thaw" technique, compared to the "bath thaw" technique, are vast (Orthner and MacPherson, 1984). The "bath thaw" method using circulating water at 4°C, for up to 90 minutes is accepted as the route to follow.

2.4.2 FREEZING RATE OF SEPARATED PLASMA

Fast freezing under conditions of optimal heat exchange, yield an improved FVIII recovery compared to slow freezing. An important criterion for consideration, is the rate at which the core of the plasma mass is solidly frozen. During slow freezing, the water crystallizes from the outer layers towards the inside, increasing the concentration of ions, proteins and other substances, resulting in changes to osmolarity and pH. The freezing point drops and the FVIII molecular structure is altered (Smit Sibinga, 1986). Components which influence freezing are, rate of freezing, heat exchange, eutectic point, temperature control and time. The shape of the frozen packs is an important consideration, as uniformity would allow an optimal thawing process of the plasma mass. In 1978, Mason introduced an improved freezing technique whereby the plasma packs, prior to freezing were placed between metal sheets in order to achieve plasma slaps of equal and minimum thickness. A slow freezing rate results in a cryoprecipitate with a FVIII yield which is twice that of a fast frozen cryoprecipitate (International Forum, 1983). A heavier cryoprecipitate results in a FVIII with lower activity. It is however recommended that plasma be completely frozen within 30 minutes of separation.

2.4.3 THE STABILITY OF FACTOR VIII IN THE FROZEN STATE

The optimal temperature for preserving FVIII in plasma is minus 30°C. The eutectic point of plasma is minus 23°C. At any temperature below minus 23°C, there is an irregular mixture of water/ice and pools of unfrozen concentrated protein in hypertonic salt solution (Britten and Grove-Rasmussen, 1966). Attempts to bring frozen plasma from a storage temperature of minus 40°C to a complete thaw within 30 minutes results in the preparation of a poor quality cryoprecipitate. If the frozen plasma is warmed to minus 10°C prior to thawing the quality of the product is enhanced (Foster *et al.*, 1984).

Storage temperature conditions of fresh-frozen plasma have a significant effect on fibrinogen levels in cryoprecipitate. The fibrinogen is a major protein constituent in cryoprecipitate, as cryoprecipitate is used as a fibrinogen supplement as well as for its FVIII properties. Enhancement of fibrinogen can be achieved by allowing the frozen plasma to "warm" over a period of sixteen hours to minus 5°C prior to thawing (Farrugia *et al.*, 1992). The estimated range of fibrinogen is between 100 - 300 mg per 10 ml volume of cryoprecipitate. There is no evidence to indicate that the fibrinogen content is directly proportional to the amount of FVI'. present in any given cryoprecipitate (Ness and Perkins, 1980).

2.4.4 FREEZING TECHNIQUE OF PLASMA

Temperature changes in plasma during freezing can be separated into three parts, namely a very slow decrease near freezing point, followed by two rapid events before and after freezing. The final stage, close to the freezing point takes the most time. The first stage is a rapid fall to freezing point. At freezing point the change from liquid to solid occurs and a temperature plateau is formed, the plateau is caused by the need of a large amount of energy transport at the conversion. Hence the requirement for competent freezing equipment, in order to minimise the delay in temperature decline. Handling of the frozen plasma must be quick and efficient to avoid temperature fluctuations and better freezing conditions are experienced when ethanol baths are utilised. FVIII recovery depends mainly on the time of the phase change at the freezing point, therefore rapid freezing rates result in higher recoveries of FVIII (Carlebjork *et al.*, 1984 & 1986b).

Placement of plasma in a freezer, with a temperature below minus 40°C has been found not to be suitable as a freezing technique (Farrugia and Prowse, 1985). Plasma frozen in a minus 70°C ethanol bath or below minus 85°C produce a better quality cryoprecipitate. When using a freezer, care must be taken not to stack the plasma bags on top off each other as freezing will be prolonged. The time taken to freeze the plasma, under 60 minutes, is more critical than the type of freezing equipment used (Slichter *et al.*, 1976).

When the temperature of plasma is lowered, tiny ice crystals form and solutes such as the proteins and salts become concentrated in the inter crystalline spaces. If the temperature is lowered further, the salt concentration reaches a stage at which some of the protein elements become insoluble and precipitate. Cryoprecipitation is a process of salting out at subzero conditions where sodium chloride is the predominant salt in the plasma with a eutectic point at minus 23°C. At temperatures above this, small salt pockets will remain in the liquid solution (Rock and Tittley, 1979). When plasma is frozen in different thicknesses and not in slabs, the thinner portions thaw more quickly, thus losing FVIII content before the rest of the plasma reaches its liquid state (Rock and Tittley, 1977).

2.4.5 SEPARATION OF RED BLOOD CELLS AND PLASMA BY CENTRIFUGATION

Red cell contamination during separation of the plasma for cryoprecipitation production is an important consideration. One of the side effects of frequent infusion of cryoprecipitates is immunization of the patient. A high spin centrifugation of 4500 - 5000 x g for 20 - 30 minutes is suggested as a crucial production criteria (International Forum, 1983). FVIII levels in the cryoprecipitate were compared between platelet rich plasma, prepared by a relatively soft centrifugation spin and that of fresh frozen plasma, prepared at high speed centrifugation. Both centrifugation techniques produced acceptable FVIII levels (Smith and Hodges, 1984).

2.4.6 POST-THAW HOLDING TIME OF CRYOPRECIPITATE

It is the period instantly post-thaw, when the physico-chemical change from the solid form has just transpired, that is the determining factor in FVIII recovery (Rock and Tittley, 1977).

2.4.7 THAWING TECHNIQUE OF FROZEN PLASMA

FVIII can be lost in two ways during thawing. Dissolution of the precipitate occurs when the temperature at the solid-liquid interface exceeds the FVIII solubility limit. The second way involves inactivation of FVIII by enzymic degradation or other instabilities occurring from hostile physico-chemical environments (Burka *et al.*, 1975). In order to prevent the above from happening, thawing must be achieved immediately with temperature control being vital. The problem is that overheating occurs and in order to avoid this, an optimal thaw/temperature rate is necessary. In order to maximise thawing, a large surface area at the point of exposure to the heat, with even distribution is required, to prevent excessive heat on any one point of the surface area (Foster *et al.*, 1982 and 1984).

The presence of ice crystals in the plasma during thawing is a critical phase, to which close attention must be given (Burka *et al.*, 1975). An increase of 20% in FVIII yield was obtained by the careful regard for detail.

Rapid thawing can be obtained by rocking the frozen plasma packs in a water bath in which the temperature of the water is held constant. This method is known to enhance the yield and activity of FVIII (Margolis and Eisen, 1986). Rapid thawing of the frozen plasma is usually achieved by submerging the packs in a circulating water bath at temperatures between 4°C and 8°C, with a thaw time of 120 minutes. A major drawback of this technique is that the end-point of thawing "soft ice" stage, associated with high yields, can simply be overlooked (Wensley and Snape, 1980).

According to Kang (1980), the thaw-siphon technique yields the best recovery of FVIII above all other thawing methods, although it is labour intensive on a large production scale, with a critical stage being the end stage at the "soft ice" phase. The fast-thaw is an adequate thawing technique also requiring attention during the final thawing stages.

2.4.8 PRECIPITATION

The thaw siphon thawing technique described by Mason (1978), has become a well accepted thawing technique over the years. The procedure exploits the Le Chatelier equilibrium principle, in which the equilibrium of the two-phase system (ice - water) is continually displaced to the right by constant removal (by siphoning) of the thawed phase. There is little contact between FVIII and the liquid phase, because the contents of the pack remain frozen. *In vivo* studies of cryoprecipitate, prepared by this technique, confirm that the survival of FVIII compares well to that

of an intermediate purity concentrate (Toolis et al., 1980).

In the thaw-siphon procedure, the temperature gradient between the "hot" 3°C bath water and the frozen plasma is responsible for a continuous flow of heat , via the walls of the plastic packs from the water to the frozen mass. Pressure from the water supports the contact with the reducing plasma mass. The thin plastic layer of polyvinyl chloride foil intensifies the continued heat exchange. The outflow of the thawed plasma is sometimes interrupted as the volumes reduce, and the sides of the plastic bags are sucked together. This is overcome by inducing puckering, by the use of elastic bands (Mason et al., 1981). This siphoning technique has benefits in that the plasma protein is removed during the initial stages, and the precipitate is washed free from any trapped soluble plasma protein, thus enhancing the final purity. The fast processing by the continuous thaw-siphon technique by Mason et al. (1981) allows fast processing at controlled low temperatures without the use of a centrifuge. The rise in FVIII experienced, is due to reduced redissolution and reduced regradation of FVIII, due to maintenance of temperatures below 4°C and the fast processing. Trapping of the cryoprecipitate within the plasma mass, also contributes to the improved yield (Prowse and Mc Gill, 1979). Alternately, the thawed plasma can be sedimented by a 4°C centrifulation step for ¹⁵ minutes at 4733 x g. (Tomasulo *et al*, 1980). Sedimentation of cryoprecipitate is completed after 5 minutes centrifugation at 1500 x g. Further centrifugation for an augmented period produces no further precipitation and only prolongs production time (Vermeer et al., 1976a).

Cryoprecipitate appears to form a dense and heavy solid phase, which should be easy to separate from the liquid, but attention to the type of centrifugal equipment is important. Fine precipitate particles are sometimes present in the supernatant plasma and if not precisely centrifuged, by the use of adequate separation forces, cryoprecipitate can be wasted (Foster *et al.*, 1984). Another important factor is the requirement to control temperature at the point of sedimentation. If too cold, freezing will occur, thus reducing FVIII recovery. If too warm, the precipitate will redissolve. The supernatant plasma is drained from the precipitate in a 4°C cold room to minimize the redissolving of the precipitate to a final volume of 10 ml (Slichter *et al.*, 1976).

The final volume of the cryoprecipitate has a direct influence on the final FVIII and fibrinogen content. A final volume of 10 - 12 ml produces a cryoprecipitate with high FVIII and fibrinogen content, diminished of excess of plasma proteins. A final volume less than 10 ml results in lower recoveries (Hoffman *et al.*, 1987). Frozen cryoprecipitates once thawed and pooled, have an expiry time of six hours, due to bacterial contamination possibilities and also due to the unstable nature of the FVIII. Fibrinogen on the other hand is an extremely stable plasma protein if stored at 1 - 6°C for several days (Howard *et al.*, 1991).

The AABB recommendation prior to 1989, was that thawed cryoprecipitate should be stored at room temperature for up to six hours, if not used immediately. This was subsequently changed after researchers showed that cryoprecipitate and fibrinogen were better stored at 1 - 6°C (Spivey *et al.*, 1992). Adequate levels of

Factor VIII are preserved in thawed cryoprecipitated FVIII that has been thawed at room temperature for up to 24 hours. Precipitation of fibrinogen and FVIII occur at temperatures 1°C - 6°C. Loss of FVIII occurs on thawing, so if required for accurate FVIII determination, samples should be tested immediately (Saxena *et al.*, 1991).

2.5 STANDARDIZATION OF FACTOR VIII ASSAYS

The determination of Factor VIII proagulant activity (this means the total or partial lack of production of the FVIII protein), is the most common specific coagulation factor assay performed and is used to diagnose Haemophilia A (Brandt *et al.*, 1988), as well as determination of FVIII activity in cryoprecipitates.

As the emphasis of this research work revolves around Factor VIII activity, it was important to review the literature and the problems encountered with FVIII assays and assay types available, before commencing the study in order to determine reproducibility, accuracy and reliability of results.

The number of variables that may affect the Factor VIII results are well documented in the literature. Elements such as clot detection methods, technical staff, specimen handling, data detection methodology and analytical parameters are but a few of the criteria to be carefully considered when choosing the assay type to be used. Analytical parameters related to type of buffer systems, aPTT reagent, substrate plasma and reference standards are major determinants of the precision and

accuracy of the assay. One of the most important options is the selection of FVIII:C deficient substrate plasma. The use of different types of deficient plasma has been implicated as the cause of variability of one stage assays (Wasi *et al.*, 1994). Clotting assays for the determination of Factor VIII activity suffer from low precision and limited accuracy (Carlebjork *et al.*, 1987).

It is of great significance that the appropriate kind of FVIII:C standard, according to the sample being assayed, be used. In other words, a concentrate standard when assaying FVIII concentrates and a plasma standard when assaying plasma samples should always be used (Lusher et al., 1984). Concentrate standards should be used for the assay of therapeutic concentrates. Calibration of the plasma standard against the international standard concentrate has led to discrepancies between assay methods: one and two stage assays, (Barrowcliffe, 1984). Several collaborative studies organized by the National Institute for Biological Standards and Control (NIBSC) in Great Britain, have demonstrated that one-stage and twostage methods do not give the same results when comparing dissimilar preparations: plasma and concentrates, (Mikaelsson and Oswaldsson, 1984). Standardization of the FVIII plasma standard used, is either frozen or freeze dried normal plasma which has been calibrated against the International Reference Standard Plasma or other national standards. The plasma standard should always ^{be} stored at below minus 30°C. The first International Standard (IS) for Factor VIII established in 1971 by Bangham and colleagues was a major step forward in the standardization of measurements of Factor VIII clotting activity.

Most investigators use the one-stage Factor VIII:C method, although the two-stage method gives higher yields (Kjellman, 1984). The estimation of specific activity depends on the Factor VIII assay which varies significantly between the two-stage and one-stage assay (Allain *et al.*, 1980). It is generally accepted that the two-stage assay method provides a more precise and less artificial evaluation of FVIII content. The two-stage assay has not been routinely used as it is difficult to automate, and the test plasma requires absorption prior to assay (Rock and Palmer, 1985). Brandt *et al.* (1988) recommended that whatever plasma sample is used to construct the standard curve, it should be standardized against a reference plasma with known activity, preferably one based on the International Reference Plasma.

In an investigation by Mikaelsson and Oswaldsson (1984), a comparison of various assay methods was undertaken which included a chromogenic substrate assay. The findings were that the new chromogenic substrate assay provides both accurate and precise measurement of FVIII:C. The assay was found to be superior to all other FVIII coagulation assays. Validation of the Kabi chromogenic assay against the one-stage clotting assay was carried out, with good correlation between the assays. The chromogenic assay was found to be both cost effective and less labour intensive (Pool, 1992).

The advent of chromogenic substrates has led to great progress concerning methods for determining important coagulation parameters. A method was developed that is simple to perform, requires no defibrination, contains reagents with stability and produces results that would be accurate and reproducible. Hence

the Coatest^R for FVIII detection was developed ((Rosen, 1984).

The Coatest^R Factor VIII Kit was evaluated by a collaborative clinical survey (4 laboratories participated) against the one-stage clotting assays. Precision was higher with the chromogenic method (Rosen et al., 1985). The Coatest^R was adapted to a microplate technique which is inexpensive and convenient. Many plasma samples are able to be tested at the same time, hence less labour intensive. This test kit is not dependent on the use of Haemophilia A plasma as test substrate (Lethagen et al., 1986). The Coatest^R, however requires maintaining the temperature at 37°C, concise timing of reagent addition and in pipetting techniques. The technique has a further advantage in that all the reagents are of animal or synthetic origin. Variations in use of the kit, by diluting reagents which result in longer incubation times, can be utilized, thus allowing up to 96 tests, compared to 50, if used according to the manufacturer's instructions (Prowse et al., 1986). This assay design is now in routine use in the quality control of the production of FVIII. The simplicity of the microplate assay, in combination with the high resolution at all Factor VIII levels, makes it quite suitable for screening blood donors. Selection of donors with high Factor VIII levels for plasmapheresis, would increase the quality of plasma intended for the production of cryopre lipitates. The microplate method is advantageous over classical coagulation assays. No reagents of human origin are used, thus decreasing the risk of virological contamination. Large amounts of samples can be assayed in a short period of time. The technique is easy to perform with high precision, even with personnel not trained in blood coagulation assays (Carlebjork et al., 1987).

2.6 2^k FRACTIONAL FACTORIAL EXPERIMENTAL DESIGN

A full 2^k factorial design requires all combinations of two versions of each of k variables. If a variable is continuous, the two versions become the high and low level factors of that variable. The notation using plus and minus signs are used and the list of experimental runs is called the design matrix. The design matrix contains k columns and N = 2k rows. There is a column for each of the k variables, and each row gives the combination of versions for each run (Box and Hunter, 1961a & b). A complete factorial experiment is one in which all possible combinations of all the levels of the different variables, are investigated. This would involve a large number of tests when the number of variables is greater than five. It is possible to investigate the main effects of the variables and their interactions in a fraction of the number of tests required for the complete factorial experiment (Box et al., 1963). The object of fractional factorial designs is to obtain information on the main effects, and as many of the interactions with a smaller number of tests than would normally be required. This type of design is particularly valuable in a production environment when there are a large number of variables implicated. It is a worthwhile means of establishing which variables are playing a dominant role in producing an effect. It is used where certain variables, which may interact, are ^{to be} studied simultaneously with other variables whose influence, if any, can be described by main effects only.

A weakness of this design is that it provides no way of detecting all interactions, ^{especially} if several variables are playing a dominant role in producing an effect.

Nevertheless it is effective in identifying dominant variables in a cost effective manner (Hendrix, 1979). When a number of variables are to be compared, they should be compared under the same conditions. Any extraneous variation will add to the experimental error. Replication of an experiment is a means of providing an unbiased estimate of the experimental error variance and more reliable estimates of the effects (Dykstra, 1959). The basis of all interpretations in this type of experimental design is the assumption that the variables which have high loadings of a factor, have something in common. Fractional factorial designs depend just as much upon the formulation and testing of the hypotheses as any other form of research (Adcock, 1954). Confounding is the process by which unimportant comparisons are deliberately confused for the purpose of assessing the more important comparisons with greater precision.

Statisticians can therefore be of major help in study design. The more the ^{researcher} knows what is going on, the more the statistician can be of help in ^{study} design (Boen, 1993).

CHAPTER 3

MATERIALS AND METHODS

This chapter describes the experimental design utilized and covers, sample collection, bleeding procedures, production variables with their factors and the assay techniques employed in an attempt to produce an improved quality cryoprecipitate.

3.1 EXPERIMENTAL DESIGN

This study was based on a statistically recognized experimental design called *Fractional Factorial Experimental Design*. Fractional Factorial Experimental Design is employed when a myriad of variables with their factors are used in any one production process, all of which could have an influence on the outcome of the product. To commence a table was compiled of the production variables, using opposing criteria, called factors. Units of blood were collected and processed into cryoprecipitate, from blood donors under the stipulated criteria, corresponding to the study design. The pre, post and final samples obtained were ana!yzed against selected appropriate assays. The results of all the assays were statistically analyzed. The results are presented in the form of tables of means together with standard errors and least significant differences. Interactions between the significant variables were identified. In selecting this design, the OBJECTIVE was to:

- * gain understanding on how the variables affect product properties
- uncover variables which influence the FVIII yield in the cryoprecipitate, in
 order to achieve an improved product
- * find "winning" combinations of variables and their factors.

•

The statistical design was proposed, compiled and analyzed by the Institute for Biostatistics at the Medical Research Council (MRC). The variables were coded as a chart of experiments with (+) and (-) signs, representing high and low levels of each factor (Hendrix, 1979). The chart is shown in Table 3.1

Fourteen production variables were identified as critical steps in the production process. These are indicated as V1 to V14 in Table 3.2. The purpose of the Fractional Factorial Experimental Design in Table 3.1 is to enable all two-factor interactions to be estimated. In order to achieve this, a total of 32 production runs were required. For the purpose of obtaining reliable estimates of factor means, the size of the donor base of 52,000 blood donors was considered. It was accepted that the 32 production runs would have to be repeated four times over, to be of value. The study variables selected are shown in Table 3.2, with their specific factor for each of their high and low levels. The first six variables relating to blood donor, primary anticoagulant, delay prior to processing, and temperature storage conditions, all conditions relating to pre commencement of the production of cryoprecipitate.

NO.	V1	V2	٧3	V4	V5	V6	V7	V8	V9	V10	V11	V12	V13	V14
1.	+	9	÷	-	+	+	+	-		-	+	+	-	+
2.	-		+	16 16	+	1 2 1	÷	4	÷	+		-	+	-
3.	+		+	+	+	-		+		+		+	+	2
4.	+	+	-	+	-	+		+	-	-	÷	+	+	+
5.	+	12	+	+	-	+	+	-	+	-	-	-	-	+
6.	+	i n		+	+	+	-	-	-	+	-	-	-	+
7.	+	+	-	+	+	-	+	÷	+	+	+		-	+
8.	-	+	-	+	+	+	+	-		-	-	+	+	+
9.	+	-	-	-	-	+	-	-	+	+	+	+	-	+
10.	+	+	+	+	-						+	-		-
<u>.</u>	-	+	-	.	+	-	-	+	-	+	+	+	-	-
14.	+	+	-	-	-	-	+	-	-	+	-	+	Г.,	-
10.	+	+	+	-	-	+	+	+	-	+	-	-	+	+
4.	+	+	+	+	+	+	+	+	+	+	+	+	+	+
10.		+	-	+		-	-	+	+	+	-	-		
17	-	-	+	_		+		+	-		-	+	-	+
18	+	+	-		+	+	-	+	+			-	+	+
10	+	-	+			-	-	+	+	+	+	-	+	-
20		-	-	+	-	+	+	+	-	+	+	-	0=0	+
21		-	+	+	-		+	-		+	+	+	+	-
22		+		-	-	+	+		+	-	+	-	+	+
23		+	+	-		-	+	+	+	-	+	+	7	-
24		+	+		+		-	-	+		-	+		-
25.		+	+			+	-	-	+	+	-	+	+	+
28.	+	+	+	-	+	+	-	-		+	+	-	+	+
27.			-	-	+		+	+			+	-	+	-
28.	-			-				-		-	-	-	+	
29.	-			+	+		-		÷	-	+	+	+	-
30.	-		-		+	+	+	+	+	+	-	+	-	+
31	+		+	+	+	+		+	+	-	Ť	-		+
32.	-		-	+		-	+	+	+	-		+	+	
		+	+	+	+	-	+	+	-	-	_	-	-	-

Table 3.1

Fractional Factorial Design. V1 - V14 are the different variables used and no 1 -32 the different production runs, the (+) is the high level factor (-) the low level factor of each variable.

The other eight variables deal with the production stages of the cryoprecipitate process. They were, temperature for freezing and thawing of plasma, freezing and thawing techniques, centrifugation speeds, precipitation methods and rate of thawing. The variables and their factors were selected primarily, according to the current production process at WPBTS, but the latest technology outlined in the more recent literature also influenced our decision when making the selection. Variables which could be monitored to remain constant were not considered.

	VARIABLE NAME	HIGH LEVEL (+) FACTOR	LOW LEVEL (-) FACTOR
V1	DONOR EXERCISE LEVELS	EXERCISE	NONE
V2	DONOR BLOOD GROUP	GROUP A	GROUP O,B,AB
V3	BLEEDING TIME	< 8 MINUTES	> 8 MINUTES
V4	ANTICOAGULANT	CPD	HEPARIN
V5	PRE-PROCESS DELAY	< 6 HOURS	12 HOURS
V6	PRE-PROCESS STORAGE	4°C	20°C
V7	THAWING TEMPERATURE	4°C	8°C
V8	FREEZING RATE	SLOW (2 hours)	RAPID (1 hour)
<u>V9</u>	FREEZING TEMPERATURE	>-60°C	-35°C
V10	FREEZING TECHNIQUE	ALCOHOL/DRY ICE	LIQUID NITROGEN (-60°C)
V11	CENTRIFUGATION	RAPID 4733 x g	SLOW 2415 x g
V12	HOLDING TIME	NONE	0°C (1 hour)
V13	THAWING TECHNIQUE	MOVING WATER	MOVING PACKS
V14	PRECIPITATION	SECOND SPIN	SYPHON

Table 3.2 Study variables with their factors.

V1 - V6 are the pre production variables with their factors - Stage A.
 V7 - V14 are the production variables with their factors - Stage B.

Variables required to remain consistent throughout all the production runs were that:

- * the same phlebotomist place the donation needle into the donors arms
- the donors donate at the same clinic
- * there be regular mixing of the blood packs during donation
- the starting volume of 450 ml of each pack of blood be constant for each donor bled
- the final volume of the cryoprecipitate be 10 ml.

3.2 **PRODUCTION VARIABLES AND FACTORS**

3.2.1 DONOR FACTOR VIII (V1)

The blood donors with the requisite for the high (+) factor level for the variable of donor FVIII, were required to exercise for 5 minutes, using an ergometer set on a moderate difficulty rate, prior to donation. FVIII activity increases significantly as a result of short durations of intense muscular exercise (Strand *et al.*, 1974). No difference was allowed between male and female donors. The pulse rate and blood pressure of each of these donors was taken pre and post exercise. This was to ensure that the exercise did not elevate the physical state of the donc. to outside the normal specifications required for blood donation. The pulse and blood pressure of each donor varied according to the fitness and age of the donor. Criteria for blood donation at WPBTS are a pulse rate of between 60 - 84 beats per minute and blood pressure of a minimum of 100/60 mm Hg and a maximum of 160/95 mm Hg.

The requisite for the low (-) factor level was no exercise, an immediate medical check was performed, followed by the donation of blood. The medical investigation involved checking the medical history, taking the blood pressure and pulse rate and performing the iron test for determination of adequate iron levels prior to donation.

3.2.2 DONOR BLOOD GROUP (V2)

Groups O, B and AB were given the low level (+) factor for this variable. Blood Groups O, B and AB were given the low level (-) factor. On attendance at the clinic, the donors, if agreement was obtained to participate in the study, were allocated a design number according to their blood group.

3.2.3 BLEEDING TIME (V3)

This variable was induced by the application of a sphygmomanometer cuff at varying pressures. Normal bleeding time was considered to be < 8 minutes with the pressure at 60 mm Hg. This was allocated the high level (+) factor for the variable of bleeding time. In order to induce a condition for the bleeding time of low level (-) factor, the pressure of the sphygmomanometer was reduced to less than 40 mm Hg. This prolonged the bleeding time to greater than 8 minutes.

3.2.4 ANTICOAGULANT (V4)

The primary container of a triple blood pack contains regular Citrate-Phosphate-Dextrose anticoagulant/preservative (CPD) solution. This anticoagulant, first described by Gibson *et al.* (1957) has been recommended as an excellent blood preservative and is still used in modern transfusion services to-day. The formula is given in (3.1) below.

rmula (3.1)	
Sodium Citrate	2.630 g
Citric Acid	0.327 g
Monobasic Sodium Phosphate Monohydrate	0.222 g
Dextrose	2.550 g
Distilled Water to make	100 ml
Volume for use in collecting 450 ml of blood is	63 ml CPD.

As CPD is the standard anticoagulant registered in South Africa for the collection of blood , it was automatic that it be utilised in the model of the high level (+) factor for the variable of anticoagulant. Heparin, a naturally occurring complex organic substance, possesses the property of retarding *in vitro* coagulation of blood. It was selected as the alternative anticoagulant for the low leve: (-) factor. Due to the configuration of the standard blood pack system, CPD was used as the primary anticoagulant. Heparin was added immediately after the blood donation was complete. The concentration of heparin (Pularin^R Injection, Glaxo) added, was 3 U/ml. This was followed by the addition of 0.5 Mm Calcium chloride (CaCl₂), Formula 3.2.
Formula (3.2) for CaCl ₂ :	
Di-hydrate Calcium Chloride	0.735 g
Distilled Water up to	100 ml

An example for the method for the calculation of the amount of Heparin and CaCl₂ to be added to each unit of blood was as follows: mass of whole blood plus pack = 594 g

minus mass of pack _30 g = 564 g mass of whole blood = density of whole blood 1.05 g/ml = = volume of whole blood mass of blood 564 density 1.05 537 ml =

Amount of Heparin added:			
Pularin 5000 IU/5ml want 3 U/ml final dilution factor	ie. =	1000 IU/ml <u>1000</u> 3 333.3	
Heparin to be added	=	<u>blood volume</u> 333.3 1.61 ml	<u>537</u> 333.3

Amount of CaCl ₂ to be added:	
Stock solution 50 Mm want 0.5 Mm final	<u>50</u>
dilution factor =	100
Volume of 50 Mm CaCl, to be added	
	blood vol./100 + blood volume
	100
=	(537/100) + 537
	100
=	5.42 ml

3.2.5 PRE-PROCESS DELAY (V5)

Units of blood for cryoprecipitate production should be processed within six hours according to the Standards for Blood Banking, to maintain adequate levels of Factor VIII.

The high level (+) factor for this variable was set at < 6 hours, i.e. the plasma had to have been separated from the red cells and frozen within that time. The low level (-) factor time delay for this variable was determined to be 12 hours. The blood during this delay was left at the temperatures decided on according to the next variable.

3.2.6 PRE-PROCESS STORAGE (V6)

After the units of blood had been collected, according to their required high and low factor level, those that pertained to the high level (+) factor were placed immediately in a blood hamper (WPBTS design) whose environment had been cooled to 4°C. The blood remained at that temperature for the time duration as set out in V5, i.e. either processed in less than six hours or after twelve hours. The low evel (-) factor specification for this variable was normal room temperature (20°C). Those units required to remain at their said temperatures for twelve hours, were all bied late in the afternoon and further processed the next morning.

3.2.7 THAWING TEMPERATURE (V7)

This phase of the process followed the freezing stages which were covered under variables V8, V9 and V10. The choices of temperature variety for this variable were limited, due to this crucial production stage where cryoprecipitate was lost when temperatures of extreme nature were utilized. The high level (+) factor for the thawing temperature was set at exactly 4°C, and that of the low level (-) factor at 8°C. This thawing step was carried out in thermostatically controlled stainless steel water-baths, into which the frozen plasma packs were placed. A further description is given under variable V13.

3.2.8 FREEZING RATE (V8)

^{Variables} V8, V9 and V10 are closely interlinked. This variable deals with the speed ^{at} which the plasma was frozen. This stage followed the centrifugation step, ^{Variable} V11), in the production cycle. After the blood had been centrifuged under ^{the} required specifications, the blood was placed in a plasma extractor. The sterile ^{Seal} was broken and the maximum amount of plasma was transferred to the empty

No.1 satellite container (Figure 3.1). The tubing at the y-connector was sealed and the red cells disconnected from the plasma. The red cells were discarded for the purpose of the study, due to some of the abnormal conditions they would have had to tolerate. The plasma in satellite container 1 and empty satellite container 2, were placed in plastic overwrap bags (Fenwal). This procedure provided protection to the plastic containers during freezing. The plasma bags were compressed between two metal plates, held together with elastic bands on each end to obtain relative uniform thickness during freezing. The freezing rate for the high level (+) factor, was selected to be slow for a time period of two hours. The rate for the low level -) factor, was designated to be rapid for one hour.



Figure 3.1 Triple Blood Pack Configuration

3.2.9 FREEZING TEMPERATURE (V9)

in relation to variable V8, the speed at which the plasma was frozen, was governed by the temperature at which it was stationed. The temperature for the high level (+) factor, was adopted to be -60°C and that for the low level (-) factor at -35°C.

3.2.10 FREEZING TECHNIQUE (V10)

The high level (+) factor freezing technique applied, was a freezing tank filled with a mixture of 70% ethanol prepared from a 96.6% solution (Analar) and nuggets of solid carbon dioxide (Afrox -Dry Ice). The amount of dry ice added was directly proportional to the temperature required, i.e. as indicated in V9, either -60°C or -35°C. The temperature at this phase was monitored by a digital thermometer. The low level (-) factor had two systems for this variable, due to difficulty in obtaining exceptionally low temperatures. When a temperature of -35°C was required, a mechanical freezer was used for the purpose. The compressed plasma slabs were placed onto the shelves under the compressor fans. When the temperature of below -60°C was needed, the plasma slabs were placed inside the uprer layers of the liquid nitrogen tanks. The vapour present yielded the necessary cold environment, and the slabs were instantly snap-frozen.

3.2.11 CENTRIFUGATION (V11)

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The plasma was separated from the red cells in the first of the processing stages. The normal centrifugation criteria employed routinely, was selected as the high level (+) factor. This was at a speed of 4733 x g for 25 minutes. A slower acceleration of 2415 x g for 45 minutes was utilized for the low level (-) factor of this variable. Temperature of the blood was vital at this point of the operation and was maintained at 4° C.

3.2.12 HOLDING TIME (V12)

This holding stage was the final step in the production process. The high level (+) factor for this variable received no holding procedure. The cryoprecipitate was immediately placed between metal plates and snap-frozen at -40°C in alcohol/dry ice for ten minutes. The low level (-) factor required the completed cryoprecipitate to be chilled at 0°C for an hour. Thereafter it was also snap-frozen. The final products were placed at below -23°C until required for assay.

3.2.13 THAWING TECHNIQUE (V13)

This stage of the operation followed after variable V7. The thawing technique was ^{either} one whereby the frozen plasma was placed in a water-bath at the required ^{temperature} viz 4°C or 8°C, and the water circulated by means of jet sprays within ^{the} enclosure. Alternatively the plasma was fixed to the moving arms of a water-

bath known as a "rocking water bath". This resulted in a motion of agitation of the plasma packs, without circulating the water. The duration of the thaw was controlled by the thawing temperature. When all the plasma was in a " soft ice slush", it was considered the end point of the thaw. The cryoprecipitate was visible as a solid matrix of firmly enmeshed strands in the semi-frozen fluid mass. The high level (+) factor for this variable was the system, whereby there was movement of water within the thawing bath, while the low level (-) factor was that of movement of the plasma packs, with no water movement. The thawing time with each of these methods was \pm 90 minutes.

3.2.14 **PRECIPITATION (V14)**

10⁴

The last stage in the production cycle was the precipitation of the cryoprecipitate containing the Factor VIII. It can be procured by centrifugation of the plasma at the soft ice stage. The plasma was centrifuged for a second time at 4733 x g for 15 minutes. The cryoprecipitate strands were forced to the bottom of the pack. After centrifugation, the supernatant plasma was drained into the second satellite container (Figure 3.1), leaving behind 10 ml of plasma to resuspend the cryoprecipitate. This process was used for the high level (+) precipitation factor. The low level (-) precipitation factor eliminated the centrifugation step by substituting it with a siphon method. During thawing the seal was removed from the satellite empty bag. As the plasma gradually thawed, siphoning commenced, and the supernatant plasma was transferred to the empty bag. The duration of the siphoning depended on the thawing technique and temperature, but on average

took \pm 90 minutes to complete. The final product was further drained until 10 ml remained. The cryoprecipitate was then snap frozen at -60°C in alcohol/dry ice and stored at -30°C until required for assay purposes.



Figure 3.2 Flow Chart summarizing the Production Cycle

BLOOD COLLECTION

3.3

On presentation at the clinic, a worksheet for each donor was completed, capturing the relevant details such as age, sex and medical status (Appendix I). A production run number was allocated randomly (according to Table 3.1), and the design high (+) and low (-) level factor codes for the run recorded onto the worksheet. The donor was phlebotomized accordingly and the blood processed as indicated. Whole blood (480 - 500 ml) was collected from randomly selected blood donors at the Medipark Clinic, Foreshore, Cape Town. Blood was obtained from 128 regular donors in good health and between the ages of 16 and 65 years. The sample size chosen to achieve a level of reliability in the estimation of means was based on the numbers of donors on the HQ panel (5536 in total). No distinction was made between male and female donors. The donation was made into a 2,3-ethyl, hexyl-phthalate plasticized polyvinylchloride triple bag system with 70 ml CPD as the anticoagulant (Fenwal).

The donation procedure after complying with the medical check, followed the bleeding specifications outlined on the worksheet. The phlebotomy was performed by the same nursing sister throughout, and the needle was inserted into the arm in a single movement so as not to activate the haemostasis pathways. Adequate mixing of the blood was maintained throughout the donation. After donation, the weight of each pack was recorded.

SAMPLE COLLECTION

Blood samples were taken from each donor's non-donating arm, prior to any exercise or medical checks being performed. 5ml was taken into tubes containing no anticoagulant for determination of the electrolyte and plasma protein base lines of the donors. 10 ml of blood was taken into EDTA for the evaluation of the Factor VIII (FVIII), Fibrinogen, von Willebrand Factor (vWF), Fibrin degradation products (FDP) and pH base line levels. The plasma was alloquoted in 1 ml quantities in plastic tubes, labelled with the relevant design number and frozen at below -23°C, until the assays were ready to be performed. These samples were labelled the PRE specimens. POST samples (10 ml) were taken from each unit after the centrifugation (V11) stage of the production cycle, once the red cells and plasma had been separated. Again the plasma was alloquoted into 1 ml quantities and frozen. The cryoprecipitate was considered to be the FINAL sample, but was only alloquoted when the Factor VIII assay was ready to be performed. Each of the 128 production runs effectively, had a PRE, POST and FINAL sample for assay.

3.5 ASSAYS

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The following analyses were performed on each sample: Factor VIII, Fibrinogen, ^{von} Willebrand Factor, Fibrin Degradation Products, Ph, Electrolytes and Plasma ^{Proteins}, including Sodium, Chloride, Total Protein ,Calcium, Magnesium, ^{Potassium}, Albumin and Alanine Aminotransferase. Testing was performed in such ^a way that all the specimens for a particular production run were completed before

58

3.4

commencing the assays for the next production run. A total of four production runs were carried out in order to obtain reliable estimates of the mean effects and interactions. FVIII, VWF and fibrinogen assays were included in the study, due to the fact that, from experience, they played an important role in determining the yields in the cryoprecipitate. Ph determination is not routinely included as a routine assay, but due to the variation in anticoagulants, I felt it important to include. FDP assay provides a clear indication to whether FVIII activation has occurred, at the time of phlebotomy. Plasma proteins and electrolytes have not been reported on in previous studies and I felt significant findings might come to light by including this set of assays in the study.

3.5.1 FACTOR VIII ASSAY (VIII:C)

3.5.1.1 PRINCIPLE

A chromogenic assay technique was selected for the determination of Factor VIII ^{coagulant} activity (VIII:C), in plasma and blood fractions. The assay was designed ^{to} give a linear correlation between Factor Xa, generated and Factor VIII:C content ^{of} the sample. In the presence of calcium and phospholipids, Factor X was ^{activated} to Factor Xa by Factor IXa. This generation was greatly stimulated by ^{Factor} VIII, which may be considered as a cofactor in this reaction. By using ^{optimal} amounts of Ca²⁺ and phospholipids and an excess of Factor Ixa and X, the ^{rate} of activation of Factor X was solely dependent on the amount of Factor VIII:C ^{content} of the sample. FXa hydrolyses the chromogenic substrate S-2222, liberating the chromophore p-nitroaniline (pNA). The chromophore absorbs light at 405 nm. This reaction is simplified below.

Factor X	Factor Ixa, Ca2	phospholipid Factor Xa
	Factor V	
Substrate	Factor Xa	peptide + PNA

The colour intensity was considered proportional to the Factor Xa in the reaction mixture. Factor Xa was considered proportional to the Factor VIII:C content in the sample. The colour intensity of the reaction was thus an indirect measure of the Factor VIII:C content of the sample. The hydrolysis of S-2222 by thrombin in the reaction mixture was prevented by the addition of the synthetic thrombin inhibitor, I-2581, to the reaction mixture. The reaction is displayed diagrammatically in Figure 3.3.



Figure 3.3 Diagrammatic presentation of the Chromogenix Reaction where FVIII is a cofactor in the activating step that converts X to Xa. Phospholipid and Ca²⁺ are components in the complex.

3.5.1.2 *REAGENTS*

The assay kit used was the Chromogenix Coatest^R Factor VIII (Kabi Vitrum, Sweden).

(a) <u>S-2222 + I-2581</u>

Chromogenic substrate (Bz-Ile-Glu(y-OR)-Gly-Arg-PNA), 20 mg and synthetic thrombin inhibitor, 335 μ g with mannitol added as a bulking agent. These were reconstituted with 10 ml sterile water to obtain a concentration of 2.7 mmol/L. This reagent remained stable for 6 months at 2 - 8°C.

(b) Factor Ixa + Factor X

Lyophilized bovine Factors Ixa and X with bovine albumin added as a stabilizing ^{agent} were reconstituted with 10 ml sterile water. This reagent was stable for 12 ^{hours} at 2 - 8°C. This reagent can be alloquoted into small volumes and if frozen ^{at} -20°C, remained stable for a month.

(c) Calcium chloride (Ca Cl₂)

Calcium chloride was supplied in a 0.025 mmol/L solution, remained stable if stored at a temperature of between 2 - 8°C.

(d) Stock Buffer Solution

A new buffer working solution was prepared each day. One volume of stock buffer solution was diluted with 9 volumes of sterile water before utilizing. The

constituents of the diluted buffer are Tris 0.05 mmol/L, Ph 7.3 and 0.2% bovine albumin. The opened stock solution vial remained stable for one month at 2 - 8°C.

(e) Phospholipid

This reagent consisted of a phospholipid emulsion prepared from porcine brain, with sodium azide added as a preservative. An open vial remained stable for one month at 2 - 8°C.

3.5.1.3 *EQUIPMENT*

The following additional materials were required for this assay:-

plastic test tubes (5 ml) vortex mixer laboratory assay timer polystyrene microtitre plates (flat-bottomed) heat incubator 37°C Titertek Multiskan PLUS plate reader (405 nm filter) Automatic microliter pipettes and tips

Multiskan PLUS is an eight-channel vertical light path filter photometer designed to measure the absorbances of liquids. In vertical photometry, the absorbance of light is proportional to the amount of light absorbing substance in the well. The Multiskan plate reader has a programmable calculation mode. Recall Programme 1 being that for the cryoprecipitate and Recall Programme 0 for the plasma. The calculation mode was set as follows :-

Standard 1	0%	0.00 U/ml FVIII	0.000	0 000
Standard 2	25%	0.25 U/ml FVIII	0.237	5 000
Standard 3	50%	0.50 U/ml FVIII	0.475	10 000
Standard 4	100%	1.00 U/ml FVIII	0.950	20 000

Once the programme has been recalled, the start key is pressed, the plate inserted and enter selected. The user then enters the concentrations and Multiskan PLUS calculates a standard line with the help of concentrations and absorbances of these standards, using the method of least squares. Measured absorbances of the samples are converted to concentration units by the use of this line. Concentrations obtained and the standard line are sent via the interface. A printout of the results can finally be obtained.

3.5.1.4 STANDARD PREPARATION

A standard curve was prepared for each microtitre plate. Standards were prepared using either plasma (WP plasma std, in-house), or cryoprecipitate, depending on the samples to be assayed. The FVIII standard was prepared according to WPBTS standard operating procedures. The pre-assayed standard was pre-diluted to 1 U/ml Factor VIII in buffer. This was further diluted as shown below in Table 3.3 for the plasma standard, and Table 3.4 for the cryoprecipitate standard. All the dilutions were made in plastic tubes. Each dilution was mixed on the vortex mixer before being used for the next dilution.

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Table 3.3 Dilutions for plasma standard.

Cryoprecipitate	Standard		
Pre dilution (1)	100 wil onvo std	+ 1450 /d buff	
Pre dilution (2)	50 μl of dil.1	+ 300 μl buffe	31
100% (3) 50% (4)	25 µl of dil.2 500 µl of dil.3	+ 1000 µt buff + 500 µl buff	er *
25% (5)	500 μ l of dil.4	+ 500 µl buffe	ar 🕈
* these d	ilutions were used in	the assay	

 Table 3.4
 Dilutions for cryoprecipitate standard

3.5.1.5 SAMPLE PREPARATION

Samples were thawed at 37°C. They were assayed within 30 minutes of the dilutions being made. As a result only one plate was set up in a run. The dilutions for the plasma and cryoprecipitate samples were made as shown in able 3.5.

Plasma Sample		
Pre dilution (1)	50 μ l test sample + 300 μ l buffer	
100% (2)	25μ of dil 1 + 1000 μ buffer *	
Pre-dilution (1)	7.2 ul test sample + 1000 ul buffer	
100 (2)	25 μ l of dil.1 + 1000 μ l buffer *	
* denotes	the dilution used in the assay	

Table 3.5 Sample dilutions for plasma and cryoprecipitate.

15 μ l Cryoprecipitate sample was applied into each of duplicate wells on a 96 well plate. 15 μ l of each standard was applied to each well, commencing with buffer (0%) to act as a control, followed by the 25%, 50% and 100% standard dilutions. The reader had been programmed to read in that order. The last two wells of the plate were filled with a back standard (100% standard dilution), which acted as control and check versus the standard's calibrated value. For the cryo samples this consisted of the undiluted cryo standard, whereas for the plasma the 100% dilution ^{Was} used. The plate arrangement is displayed in Figure 3.4.

	1	2	3	4	5	6	7	8	9	10	11	12
A	0%	3	7	11	15	19						
B	25%	3	7	11	15	19		Ì				
с	50%	4	8	12	16	20						
D	100%	4	8	12	16	20						
E	1	5	9	13	17	21						
F .	1	5	9	13	17	21						
G	2	6	10	14	18	STD						
H	2	6	10	14	18	STD						

Figure 3.4 Layout of microtitre plate. The plate is numbered 1 -12, horizontally, and A - H vertically for easy identification when reading results.

3.5.1.6 ASSAY

The assay is demonstrated by a diagrammatic flow chart in Figure 3.5.

- (i) The phospholipid solution and Factor IXa + X bovine mixture were mixed in the ratio 5:1 v/v. Three volumes of $CaCl_2$ were added to this blend.
- (ii) 40 μ l Of this mixture were added to each well.
- (iii) The plate was then covered, gently tapped to mix, and incubated at 37°C for
 10 minutes.
- (iv) 30μ l Of the substrate solution (S-2222) was added to each well. The plate was covered, gently tapped to mix, and incubated at 37°C for a further 10 minutes.
- (V) The plate was read on a Multiskan plate reader at wavelength 405 nm using the calculation mode.

Preperation

- 1. PREPARE STANDARDS
- 2. DILUTE SAMPLES

Keep on ice



Figure 3.5 Diagrammatic Flow Chart of FVIII Assay.

3.5.1.7 INTERPRETATION OF RESULTS

Firstly, the standard readings obtained against the programme linear standard calculation, were checked to ensure that the results correlate. The back standard was checked to see that it fell between the range of 18 - 22 U/ml. If it was out of the specification range, a correction factor was calculated and the average of the sample readings adjusted accordingly. An example of a correction factor is given in Table 3.6. Duplicate sample readings were compared for accuracy and the mean result calculated and expressed in U/ml for each sample.



Table 3.6 Calculation for correction factor.

3.5.1.8 THE EFFECT OF HEPARIN ON ASSAY

^{The} inhibitory effects of heparin require neutralization before an accurate F VIII ^{assay} can be performed. Those plasma and cryoprecipitate samples that were spiked with heparin during the production process, were treated with Heparsorb^R (Organon Technika) in the following way:-

- (i) 35 mg Heparsorb_B was added to 0.5 ml plasma/cryoprecipitate sample;
- (ii) incubated at room temperature for ten minutes while rotating on a rotator mixer;
- (iii) centrifuged for five minutes at 1200 x g at room temperature, and
- (iv) supernatant removed and assayed according to F VIII instructions above.

Expected Ranges: 0.5 - 1.0 U/ml

3.5.2 FIBRINOGEN ASSAY

3.5,2.1 PRINCIPLE

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A rapid technique based on the Clauss technique for thrombin clotting time (Clauss, 1957) was employed. The principle of this method was that the clotting time of plasma was inversely related to fibrinogen concentration. The enzyme thrombin, ^{converts} the soluble plasma protein fibrinogen into its insoluble polymer, fibrin. At high thrombin concentrations (100 NIH units/ml), and low fibrinogen concentrations ^(5-80 mg/dl), the reaction was determined by the fibrinogen concentration. The use ^{of} diluted plasma and a relatively high concentration of thrombin, results in little ^{interference} by fibrin degradation products (FDP) or heparin, unless present in large ^{amounts}. The thrombin clotting time of test plasma was converted to fibrinogen concentration by use of a calibration curve, derived from a range of fibrinogen concentrations, clotted by a fixed concentration of thrombin. When plotted on loglog paper, the thrombin clotting time was linear when compared to the fibrinogen concentration.

3.5.2.2 REAGENTS

100

<u>Data-Fi^R Thrombin Reagent</u>

This reagent is a lyophilized preparation of bovine thrombin (approximately 100 NIH units/ml) with stabilizers and buffers (Dade, Baxter Diagnostics - Ridge SA). 1 ml sterile water is used to reconstitute the reagent. The vial is re-stoppered and aliowed to stand until dissolved. It is then inverted gently to mix. Shaking is not permitted. The reagent remains stable for 8 hours at room temperature or for 5 cays at 2 - 8°C.

b) Imidazole Buffer

 Formula (3.3)

 Dissolve
 3.40 g Imidazole(glyoxaline)

 5.85 g Sodium Chloride

 make up to
 500 ml

 Add
 186 ml Hydrochloric Acid (0.1 mol/l)

 Make up to
 1000 ml with Distilled Water

 Check with a pH meter
 pH 7.3

This reagent remains stable at 4°C and at room temperature for 24 hours if stored in a polystyrene tube.

(c) Standard Plasma

(**19**1) (1911)

> An in-house fibrinogen standard was used, which had been determined by replicate analysis of plasma by the Ratnoff and Menzie technique (Hall and Malia, 1974).

3.5.2.3 *EQUIPMENT*

The following additional materials were required for this assay:-

plastic test tubes (5 ml) vortex mixer timer heat incubator at 37°C Automatic microliter pipettes and tips Log/log graph paper

3.5.2.4 ASSAY

Preparation of Standard Graph

- A range of dilutions of the plasma standard were prepared in the imidazole buffer. Dilutions of 1:5, 1:10, 1:20 and 1:40 were prepared.
- (ii) 0.2 ml of each dilution were warmed to 37°C and 0.1 ml of thrombin was added.
- (iii) The clotting times were recorded. The expected range was between 6 -20

seconds. Duplicate measurements were made.

(iv) Using log/log graph paper, thrombin clotting times were plotted against the fibrinogen content (g/l) of each dilution. A linear plot was obtained.

A new graph was prepared whenever a new batch of thrombin was utilized. Multiple clotting times of the control normal plasma were determined. The mean value ± 2 SD was obtained with the control plasma when each batch of tests was executed.

Preparation of Sample for Testing

- The test plasma was diluted 1:10 in imidazole buffer. Duplicate thrombin clotting times were obtained.
- (iii) 0.2 ml of each test sample was warmed to 37°C
- (iii) 0.1 ml of thrombin reagent added and the clotting time recorded.

3.5.2.5 INTERPRETATION OF RESULTS

The plasma fibrinogen value was derived by extrapolation of the mean of the duplicate values read against the standard graph. If the value of the test was ^{outside} the limits of the standard graph (6 - 22 seconds), the test plasma was diluted and a correction factor applied. This was determined in the same way as that of the FVIII assay. Example is given in Table 3.6. (page 68)

Expected Range: 2 - 4 g/l.

3.5.3 VON WILLEBRAND FACTOR ASSAY (vWFAg)

3.5.3.1 *PRINCIPLE*

Von Willebrand Factor is necessary in the primary haemostasis for the proper formation of the haemostatic plug and normal bleeding time. The presence of the antigen can be detected and measured by the double antibody sandwich enzymelinked immunoassay (ELISA) technique. Wells of microtitre plates are coated with specific antibody and incubated with plasma dilutions. Antigen bound to the antibody is detected by a second antibody labelled with peroxidase.

3.5.3.2 **REAGENTS**

(a) <u>Buffers</u>

(i) Coating Buffer: 0.05 M Carbonate Buffer; pH 9.6 Formula (3.4) Sodium Carbonate 1.59 g Sodium Hydrogen Carbonate 2.93 g Dissolve in distilled water 1000 ml Add Thiomersal or Sodium Azide 0.02% w/v

(ii) Phosphate Buffered Saline (PBS) 0.01 M; pH 7.2

Formula (3.5)	
Sodium Dibudrogen Phoenhate	A 245 a
Disodium Hydrogen Phosphate	2.680 g
Sodium Chloride Dissolve in distilled water	8.474 g 1000 ml

(iii) Citrate Phosphate Buffer 0.1 M; pH 5.0



(b) Enzyme Substrate

		<u> </u>
F0/ mula (3.7)		
		2
1.2 Ortho Pher	vienediamine Dihydrochloride(OPD) 80 mg	
Dissolve in Citi	ite Phosphate Buffer 15 ml	
Add Hydrogen	eroxide (20 vol) 10 µl	
IMMEDIATELY	BEFORE USE	

(c) Sulphuric Acid($H_2 SO_4$) 1 M

To obtain a 1 M concentration, 28 ml H_2SO_4 was added to 972 ml distilled water

(d) Antisera

(i) <u>Rabbit Anti-Human von Willebrand Factor (2 ml)</u>

^{Rabbit} Anti-Human von Willebrand Factor, Dako-A082 (Denmark) is the purified ^{immunoglobulin} fraction of rabbit antiserum suspended in a solvent comprising of ^{0.1} M Sodium chloride (NaCl) and 15 mmol Sodium nitrate (NaN₃). The protein ^{concentration} is 5.4 g/l.

Dako-P226 Peroxidase Conjugated Rabbit anti-Human von Willebrand Factor is the purified immunoglobulin fraction of rabbit antiserum conjugated with horseradish peroxidase of very high specific enzymatic activity. The solvent for this reagent is comprised of 0.05 M Tris/Hydrochloric acid (HCL) and 15 mmol Sodium nitrate (NaN₃). pH 7.2. The immunoglobulin concentration is 1.3 g/l.

3.5.3.3 EQUIPMENT

The following additional materials were required for this assay:-

plastic test tubes (5 ml) vortex mixer electronic timer polystyrene microtitre plates and covers (flat-bottomed) Titertek Multiskan PLUS plate reader with 492 nm filter Automatic microliter pipettes and tips Linear logarithmic graph paper Tupperware container to serve as moist chamber

The principle of the Multiskan was previously explained under section 3.5.1.3 (see

^{page} 62), the only difference being that a different filter was selected viz. 492 nm.

3.5.3.4 PREPARATION OF DILUTIONS

^{Test} plasma and cryoprecipitate samples were diluted in PBS, from 1:50 to 1:200

(i.e. 3 dilutions). Normal pooled plasma was diluted in PBS, from 1:25 to 1:3200

(i.e. 8 dilutions). These plasma dilutions were used to plot the standard curve on

linear logarithmic paper.

3.5.3.5 ASSAY

4.4.5

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- (i) 100 μ l Anti-vWFAg, diluted 1:500 in coating buffer was added to each well of a 96 well microtitre plate.
- (ii) The plate was incubated in a moist chamber at room temperature for 2 hours.
- (iii) The antiserum was then aspirated and the wells washed three times in PBS containing 0.05% (v/v) Tween 20.
- (iv) 100 μ l Of each plasma standard dilution was added to row A on the plate. 100 μ l Of each diluted test sample was added as illustrated in Figure 3.6 below.
- (v) The plate was re-incubated in the moist chamber at room temperature for a further hour.
- (vi) The plasma samples were aspirated and the plates washed as in step iii.
- (vii) 100 μ I Of peroxidase-conjugated anti-vWFAg, diluted 1:500 in PBS containing 0.1% (v/v) Tween 20 was added to each well. The plate was again incubated in the moist chamber at room temperature for one hour.
- (viji) The plate was aspirated and washed as in step iii.
- (ix) The plate was given a further wash with Citrate Phosphate Burfer.
- (x) 100 μ I Of freshly mixed substrate solution (OPD) was added to each well. The plate was incubated at room temperature for 20 minutes.
- (xi) At this stage colour development was observed. The reaction was stopped by adding of 150 μ l 1 M Sulphuric acid to each well.
- (xii) Absorbance readings were determined by reading the plate on the Multiskan

.

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		2	3	4	5	6	7	8	9
A	1:2 5	1:50	1:100	1:200	1:400	1:80 0	1:160 0	1:32 00	1:64 00
₿			1	2	2	2	3	3	3
С	4	4	4	5	5	5	6	6	6
D	7	\overline{J}	7	8	8	8	9	9	9
Е	10	10	10	11	11	11	12	12	12
F	13	13	13	14	14	14	15	15	15
G	16	16	16	17	17	17	18	18	18
н	19	19	19	20	20	20	21	21	21

Figure 3.6 Layout of microtitre plate for vWFAg assay.

3.5.3.6 INTERPRETATION OF RESULTS

The absorbance readings were plotted against vWFAg standard concentrations on linear-logarithmic graph paper. A straight line should be obtained with the pooled plasma (1.0 unit vWFAg per ml), diluted 1:8 to 1:256, indicating that the assay was sensitive to at least 0.01 unit vWFAg per ml. The absorbances of the test plasma samples were read off the graph and recorded as a percentage.

Expected Result : 100%

3.5.4 FIBRIN DEGRADATION PRODUCTS (FDP)

3.5.4.1 *PRINCIPLE*

During blood coagulation, fibringgen is converted to fibrin by the action of The resulting monomers polymerize to form a soluble gel of nonthrombin. crosslinked fibrin. This fibrin gel is then converted to crosslinked fibrin by thrombin activated Factor VIII, to form an insoluble clot. The fibrinolytic enzyme plasmin, eleaves both fibrinogen and fibrin to yield degradation products (FDP). Only the degradation products from cross-linked fibrin (XL-FDP) contain D-dimer. This process is illustrated in Appendix IV. The green section is that of the Fibrinolytic System. Abnormal levels of XL-FDP in plasma indicate reactive fibrinolysis. The presence of XL-FDP in the circulation was first demonstrated by immunoprecipitation and gel electrophoresis techniques (Schifreen et al., 1985). The Dimertest^R Latex Assay (Agen Biomedical Ltd, Australia) uses highly specific D-dimer monoclonal antibody attached to latex particles. Reactive fibrinolysis was demonstrated by latex agglutination at a plasma concentration of approximately 0.25 mg/l XI-FDP. The objective for performing this assay, was to determine whether the coagulation process had been activated at the point of the needle being inserted into the donor's arm, due to poor phlebotomy technique.

3.5.4.2 *REAGENTS*

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(a) Latex Reagent (2 ml)

One dropper bottle containing a suspension of latex particles coated with mouse monoclonal Anti D-dimer antibody, containing 1 g/l Sodium azide as a preservative.

(b) Positive Control (0.6 ml)

A solution containing human D-dimer, stabilisers and preservative.

(c) Negative Control (0.6 ml)

A solution containing buffer and preservative.

(d) Phosphate buffer Solution (PBS 20 ml)



(e) <u>Test Cards</u>

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¹⁰ Disposable black 9 well reaction cards, with 60 disposable plastic stirrers for ^{mixing}. The reading surface of the test cards must not be touched with the

fingers.

Test reagents and samples are equilibrated at room temperature (20°C - 25°C), before testing commences. Reagents are mixed by inversion immediately prior to use in the assay. The reagents remains stable if stored at 2°C - 8°C.

3.5.4.3 *EQUIPMENT*

The following additional materials were also required:

Precision micropippettes and tips: 20 μ l and 100 μ l Plastic test tubes and rack Centrifuge

3.5.4.4 ASSAY

All the samples were tested by the Qualitative Screening Test (Koopman *et al.*, 1987) initially, and those that tested positive were then tested by the Semiquantitative Method (Mirshahi *et al.*, 1986).

Qualitative Screening Test

(i) Samples were thawed at 37°C and centrifuged before testing.

- ^(ji) Positive and Negative controls were included in each batch of testing. The same assay procedure was followed for the controls as was for the test samples.
- (iii) One disposable test card was selected, holding the dropper bottle vertical one drop of Latex reagent was added to the card.
- (iv) 20 μ I Of undiluted plasma or control solution were added adjacent to the latex droplet.

- (v) The latex and plasma sample/control were mixed with the plastic stirrer, until the latex was uniformly distributed.
- (vi) The card was gently rotated for 3 minutes.

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(vii) At precisely 3 minutes the test was checked under a strong light source for agglutination. Agglutination was indicative of a positive result and no agglutination of a negative result.

Examples of the results are displayed in Figure 3.7

3+Numerous large clumps Background clear Neg.(- or 0) No agglutination Background very cloudy

Figure 3.7 Illustration of the FDP reaction results.

Semiquantitative Screening Test

العازيات إسا

- (i) If a positive result was obtained, the following procedure was followed:
- (ii) Doubling dilutions of the test plasma were prepared as shown in Table 3.7.

DILUTION	PLASMA VOLUME (//)	PBS VOLUME (µ)
UNDILUTED	100	NONE
1:2	100	100
1:4	100 of dil 1:2	100
1:8	100 of dil 1:4	100

 Table 3.7
 Dilutions for the semiquantitative screening test

- (iii) Steps iii to vii for the Qualitative Screening test were then carried out on each dilution.
- (iv) The highest dilution in which visible agglutination occurred was taken as the titre.

3.5.4.5 INTERPRETATION OF RESULTS

Elevated levels of plasma XL-FDP were indicative that activation of the coagulation ^{system} had occurred (reactive fibrinolysis), which will cause agglutination of ^{Dimertest} Latex as shown in Table 3.8.

		SAMPLE DILUTION			
TITRE	TITRE APPROXIMATE XL-FDP		1:2	1:4	1:8
0	img/ii NOBMAL	_	-	_	-
1	0.25 - 0.5	+			
2	0.5 - 1.0	+	+	-	-
4	1.0 - 2.0	+	+	+	-
8	2.0 - 4.0	+	+	+	+

Table 3.8Fibrin Degradation Products (FDP)Results for quantitative method"+" = agglutination"-" = no agglutination

Levels greater than 4.0 mg/l were calculated by extending the dilutions beyond 1:8. The crosslinked fibrin degradation products, D-dimer, D-dimer E and high molecular ^{weight} derivatives were all recognized by the Dimertest monoclonal antibodies. No ^{binding} was found to the fibrinogen degradation products X, Y, D, E to 20 mg/l or ^{to} fibrinogen to 1000 mg/l.

Expected Result: Negative

3.5.5 pH DETERMINATION

3.5.5.1 **PROCEDURE**

^{pH} value is the logarithm of the reciprocal of the hydrogen ion concentration; p for ^{power} and H for hydrogen. pH values range from 0 to 14, i.e. from very acidic to ^{very} alkaline. Water contains hydrogen and hydroxyl ions, the relative ^{concentration} of the ions are important. The product of the hydrogen and hydroxyl ^{ion} concentration in water at 25°C must always equal 10⁻¹⁴ gm/ion litre of solution. If the hydrogen ion concentration exceeds the hydroxyl concentration the water is acidic. If the concentrations are equal, the water is neutral. When the hydroxyl ion concentration is greater than the hydrogen, the water is alkaline Jackson and Morton, 1979).

The PRE, POST and FINAL samples' pH were measured using a Zeiss Model 300 pH meter, utilizing a N 60 A micro-electrode to determine the degree of acidosis in the samples.

Expected Value: 7.4

3.5.6 PLASMA PROTEINS AND OTHER SUBSTANCES

The chemistry parameters are preprogrammed on the Technicon Dax System. The Technicon Dax is a multiple chemistry analyzer which utilizes photometry techniques for the plasma protein and assays of other substances. The appropriate system values(SSVs) for the calibrators are entered into the calibrator parameter table and are shown in Table 3.9 for each of the assays selected. A quality control programme is performed daily on the machine to ensure the controls for each assay falls within the required specifications.
5.6.1 PARAMETERS FOR PLASMA PROTEINS AND OTHER SUBSTANCES

TEST	Mg	тр	ALT	ALB	CA
WAVELENGTH	660 700 пт	548 628 nm	340 380 nm	604 700 nm	572 628 nm
SAMPLE VOLUME	3.0 <i>µ</i> l	5.0 <i>µ</i> I	14.0 µl	2.5 <i>µ</i> I	10 <i>µ</i> l
REAGENT/ VOLUME	150/150 <i>µ</i> l	250 <i>µ</i> l	250/50 <i>µ</i> l	400 <i>µ</i> i	300/100 <i>µ</i> I
INCUBATION TIME	150 sec.	330 sec.	288 sec.	30 sec	66 sec.
TEMPERATURE	37°C	37°C	37°C	37°C	37°C
TOTAL READ TIME	-	-	180 sec.	-	-

Table 3.9 Plasma protein parameters and other substancesMg = MagnesiumTP = Total ProteinALB = AlbuminCa = CalciumALT = Alanine Aminotransferase

3.5.6.2 ASSAY PRINCIPLES FOR PLASMA PROTEINS AND OTHER SUBSTANCES

Magnesium

^{Magnesium} ions form a red chelate with Xylidyl Blue in an alkaline medium which ^{results} in a spectral shift. The change of absorbance at 660 nm ,is directly ^{proportional} to the magnesium concentration, and can be quantified by an endpoint ^{measurement}. The peptide bond of proteins forms a coloured complex with Cu²⁺ ions in alkaline solution. The shift of spectral adsorption is measured photometrically, and is directly proportional to the protein concentration of the sample. This assay is based on the Biuret method.

(iii) Alanine Aminotransferase

The reaction is initiated by the addition of the reagent to the patient sample. The rate of decrease in the concentration of NADH, is directly proportional to the ALT activity in the sample. The reaction is monitored at 340 nm as a zero-order kinetic assay.

(iv) Albumin

^{BCG} preferentially binds albumin at pH 4.2 causing a shift in the absorbance ^{spectrum}. The increase of absorbance measured at 604 nm after 30 seconds, is ^{directly} proportional to the concentration of complexed albumin.

(V) Calcium

Acidic calcium reagent is added to the serum sample and incubated to ensure the release of protein-bound calcium. An initial absorbance reading is taken before

adding reagent 2 to minimize the effects endogenous interfering substances. Addition of the second reagent, forms an alkaline medium wherein cresolphthalein complexone forms a coloured complex with calcium ions. Absorbance is measured at 572 nm. The 8-hydroxyquinoline in the reagent binds the free magnesium ions, thus minimising the possibility of their interference in the calcium assay.

3.5.6.3 *REAGENTS*

(i) Magnesium

<u>Beagent 1</u> (diluent) containing 153 mmol Potassium carbonate.

<u>Beagent 2</u> (colour reagent) containing Xylidyl blue-1 0.39 mmol; Buffer; Surfactant; Ethylene bis (oxyethylenenitrile) tetraacetic acid 0.09 mmol.

The Technicon Omnipak Magnesium Reagents are ready-to -use as supplied and no ^{preparation} is required. After opening, the reagent remains stable for fourteen (14) ^{days} at 2 - 8°C.

(ii) Total Protein

Total Protein Reagent contains Sodium hydroxide 200 mmol; Sodium potassium tartrate 50 mmol; Cupric sulfate pentahydrate 12 mmol; Stabilizers. The Technicon Omnipak Total Protein Reagent is ready-to-use as supplied and no preparation is ^{required}. After opening the reagent remains stable for thirty (30) days at room temperature.

(iii)

Alanine Aminotransferase

<u>ALT Reagent 1</u> contains Lactate dehydrogenase (porcine muscle) 3206 U; L-Alanine 675 mmol; NADH 0.32 mmol; Buffer; Stabilizer.

<u>ALT Reagent 2</u> contains a-Ketoglutarate disodium 101 mmol.

These reagents must be reconstituted with the stipulated amount of deionized water before use. After opening, this reagent remains stable for twenty-one (21) days in the refrigerated compartment of the Technicon Dax system.

(iv) Albumin

<u>Albumin Reagent</u> contains Bromcresol green 0.30 mmol; Preservative; Surfactant and Buffer. The Technicon Omnipak Albumin Reagent is ready-to-use as supplied and no preparation is required. After opening, this reagent remains stable for thirty (30) days at room temperature.

(V) Calcium

<u>Calcium Reagent 1</u> contains 8-Hydroxyquinoline 11.3 mmol; Cresolphthalein ^{complexone 0.08 mmol.}

<u>Calcium Reagent 2</u> contains AMP Buffer. The Technicon Omnipak Calcium Reagents are ready-to-use as supplied and no preparation is required. After opening this reagent remains stable for fourteen (14) days in the refrigerated compartment of the Technicon Dax system.

3.5.6.4 ASSAY PROCEDURE

- (i) Dilution of samples for these assays were not required. The frozen samples were thawed at room temperature before using.
- (ii) Those samples which appeared turbid, were centrifuged prior to insertion into the analyzer.
- (iii) The samples and reagents were placed into the various allocated holders and channels in the analyzer and the relevant assay programmes selected.
- (iv) The readings were sent via the interface to the printer. They were calculated in the computer, and a printout containing all the assay results per sample, were printed on a separate page per sample.

Expected Values:

Magnesium	1.8 - 2.6 mg/dl
Total Protein	6.4 - 8.8 g/dl
Alanine Aminotransferase	5.0 - 43.0 U/L
Albumin	3.0 - 5.5 g/dl
Calcium	9.2 - 10.9 mg/dl

3.5.7 **ELECTROLYTES**

The chemistry parameters are pre-programmed on the Technikon Dax System. The Technicon Dax is a multiple chemistry analyzer which utilizes electrode analysis for the electrolyte determination. A quality control programme is performed daily on the machine to ensure the controls for each assay falls within the required specifications.

3.5.7.1 PRINCIPLES FOR ELECTROLYTES

(i) Sodium (ISE)

The Technicon Dax system sodium method is based on an indirect potentiometric procedure using an ion-selective electrode. The sodium ion-selective electrode responds selectively to sodium ions according to the Nernst equation (Eisenman, 1967). The serum sample is mixed with ISE buffer, thereby providing a constant pH and a constant ionic strength solution. As the buffered sample flows past the ion-selective electrode, changes take place in the electrical potential. These electrical potential changes are automatically measured against the potential of a reference electrode, in order to derive the correct analog value for that sample. The electrical potentials are proportional to the logarithm of the respective sodium ion concentrations in the sample. The analog/digital signals for each sample are processed and then sent to the Technicon Dax system CPU, where the software converts the data to reportable concentration units.

(jj) Potassium (ISE)

The Technicon Dax system potassium method is based on an indirect potentiometric procedure using an ion-selective electrode. The potassium ionselective electrode responds selectively to potassium ions according to the Nernst ^{equation} (Eisenman, 1967). The serum sample is mixed with ISE buffer, thereby providing a constant pH and a constant ionic strength solution. As the buffered ^{sample} flows past the ion-selective electrode, changes take place in the electrical

potential. These electrical potential changes are automatically measured against the potential of a reference electrode, in order to derive the correct analog value for that sample. The electrical potentials are proportional to the logarithm of the respective potassium ion concentrations in the sample. The analog/digital signals for each sample are processed and then sent to the Technicon Dax system CPU, where the software converts the data to reportable concentration units.

(iii) Chloride (DCL)

The serum sample is mixed with chloride reagent. This reagent, an equilibrium solution of ferric, mercuric and thiocyanate ions, when combined with the chloride ions in the serum, undergoes a double displacement reaction, forming a red-brown chromophore, ferric thiocyanate. The absorbance is proportional to the concentration of the chloride in the sample.

 $2CI + Hg(SCN)_2$ HgCl₂ + 2SCN 3SCN + Fe3 Fe(SCN)₃ (red-brown)

^{3.5.7.2} *REAGENTS*

(i) Sodium and Potassium

<u>ISE Buffer</u> contains buffer and preservative.

ISE Mid Range Calibrator contains 14 mmol Sodium; 0.4 mmol Potassium and a

Preservative.

Se Detergent Diluent contains 140 mmol Sodium; 4 mmol Potassium and 44 mmol Sodium azide.

After opening, these three reagents are stable for thirty (30) days at room temperature.

ISE Calibrator Serum Low contains 120 mmol Sodium; 2.0 mmol Potassium and a stabilizer.

<u>SE Calibrator Serum High</u> contains 160 mol Sodium; 8.0 mmol Potassium and a stabilizer.

These two reagents are used for calibration of the machine.

SE Detergent contains Surfactant.

After opening, the ISE Calibrator Serum High and Low are stable for twenty-four ⁽²⁴⁾ hours at 2 - 10°C. A working ISE Detergent preparation is made with 12.0 ^{ml} of detergent diluent added to 12 ml of ISE detergent. The blend is mixed gently ^{by} inversion until completely dissolved.

(ii) Chloride

<u>DCL Chloride reagent</u> contains 0.8 mmol Mercuric nitrate; 1.8 mmol Potassium ^{thiocyanate}; 35 mmol Ferric nitrate and 108 mmol Nitric acid. No stabilizers or ^{preservatives} are added. After opening, this reagent remains stable for thirty (30) ^{days} in the refrigerated compartment of the Technicon Dax system. The Technicon

Dax system requires programming for this reagent. The following parameters are

entered on the Colour Reagent Screen:-

Test Name	Cl
Type	End-up
Wavelengths	476/572 nm
M.point	3
Туре	Standard
Sample Volume	4.0 <i>µ</i> ì
Reagent 1 volume	CL 400 <i>µ</i> I

3.5.7.3 ASSAY PROCEDURE

- Dilution of samples for these assays were not required. The frozen samples were at room temperature before using.
- (ii) Those samples which appeared turbid, were centrifuged prior to insertion into the analyzer.
- (iii The samples and reagents were placed into the various allocated holders and channels in the analyzer, and the relevant assay programmes selected.
- (iv) The readings were sent via the interface to the printer. They were calculated in the computer, and a printout containing all the assay results per sample, were printed on a separate page per sample.
- Reported values were calculated from the Nernst Equation automatically. The software contains a series of detectors and limits, to assure that the sample had been aspirated correctly, diluted accurately and that the electronic modules were balanced according to assigned specifications. As results were reported, abnormal values were flagged.

Expected Values:

Sodium	136 - 144 mEq/l
Potassium	3.2 - 4.8 mEq/l
Chloride	99 - 106 mEq/l

3.6 STATISTICAL ANALYSIS

The data from all the assays were extrapolated from the various worksheets into a Lotus 123 spreadsheet. The results are displayed in Appendix II for each of the assays in the following order: FVIII, Fibrinogen, von Willebrand Factor, Fibrin Degradation Products, pH determination, Magnesium, Total Protein, Albumin, Calcium, Alanine aminotransferase, Sodium, Potassium and Chloride. The results were entered into columns according to the run number, against their production run number reflected in the rows. Those results falling outside the assay specification ranges are termed outliers, and are displayed with a * next to the data result.

The information was supplied on computer disk to the Department for Biostatistics of the Medical Research Council, for analysis. The statistical method applied to the data was:- *Analysis of Variance (ANOVA)*. The **Fractional Factorial Analysis** ^{involved} the estimation and testing for significance of all main effects of the ^{variables} and all two-factor interactions. The results obtained, are shown in ^{Appendix III}.

CHAPTER 4

RESULTS

The results of the assays, determine whether donor and production variables play a role in contributing to an improved final FVIII yield, were analyzed by the method of Analysis of Variance. This was applied to all the measurements in each assay category of the variables and their factors considered.

A total of 128 blood donors were used for the study, 32 were required for each complete reproduction of the design (Materials & Methods, Table 3.1 Fractional Factorial Design), which was repeated four times to obtain reliable estimates of factor means. Healthy blood donors between the ages of 18 - 65 years, who fell within the bleeding criteria, were used. The selection of the volunteer blood donors was on a random basis, in that as they presented themselves at the selected cleeding venue and met with the acceptance donation criteria, were used for the study.

^{The statistical data based on the results of all assays was analyzed by the Institute ^{for Biostatistics} of the MRC. The results were supplied on disc, via the computer ^{programme} Lotus 123 spreadsheet. The results of all the assays performed are ^{cresented} in Appendix II.}

A complete exposition of all the statistical results for the study is presented in

Appendix III. A significance level of 0.05 was used in the statistical analysis. Samples were drawn at three stages, from the time the donor was bled, until the eryoprecipitate was complete. The first sample was taken from the donor prior to donation and was labelled the PRE SAMPLE. The second was taken after the plasma and red blood cells were separated (V6), and labelled POST SAMPLE. The mird sample was the cryoprecipitate itself, which was the final finished product and was labelled PRODUCTION SAMPLE.

Interpretation of certain of the results. When applied to the data, V6 and V14 dave the same value and as a consequence the effect for V6 is always identical to the effect of V14. The factors are said to be confounded. As a result it was not always frown whether the value obtained, represents the effect of V6 or V14, or the effect of both. Some of the variables and the interactions, in the production phase. This hould not have caused any problems if one could have assumed that there were the corry-over effects. In other words, if the variables in the pre-post phase had no filuence on the data in the production phase.

^{The levels of the variables are indicated by (+1) and (-1), coinciding with high and ^{OW} factors reflected in Table 3.2 (page 45). In the analysis the (+) and (-) factor ^{levels} indicate which data are added and which data are subtracted, to produce a ^{measure} of effect of a factor. Effect is the influence of that variable on the factor} level (+1) or factor level (-1), being measured. Due to the nature of the design, in order to recognize significant effects, the results are expressed as a table of means with a standard error (SE) of marginal means and SE of body of table means for each variable. A table of means for the interactions between all the variables for EVE, Fibrinogen and Von Willebrand Factor assays, are displayed. For the pH determination, plasma proteins and electrolytes, tables for only the significant variables are displayed. Graphs were not used to illustrate the results, since the factors have only two levels, and thus not very illuminating.

^{the production} cycle, for all the assays performed, variables V7, V9 and V11 are ^{free} of confounding. The same applies to interactions V7 by V13, V9 by V13 and V11 by V13.

For the purpose of the statistical analysis, all the PRE results were used to set the paseline levels, in each assay performed. The POST results were then analyzed against the PRE results and the outcome displayed in Appendix III as "POST - PRE" data. For the analysis of the PRODUCTION results, the POST results were used as the baseline levels and the PRODUCTION results analyzed against them. The outcome of these results are shown in Appendix III, as "PRODUCTION" data.

A key for the variables used in the tables is given for easy reference during this napter.

	POST - PRE ANALYSIS STAGE A		PRODUCTION ANALYSIS STAGE B
V1	Donor Exercise	V7	Thawing Temperature
∨2	Blood Group	V8	Freezing Rate
√3	Bleeding Time	V9	Freezing Temperature
\/4	Anticoagulant	V10	Freezing Technique
\√5	Pre-process Delay	V11	Centrifugation
¥6	Pre-process Storage	V12	Holding Time
		V13	Thawing Technique
		V14	Precipitation

4.1 FACTOR VIII

Using the data from Appendix III, under Factor VIII - Post/Pre, the standard errors (SE) for the means in Tables 4.1 to 4.15 in Stage A are as follows:

SE of marginal means : 0.027 SE of body of table means : 0.039

-east significant difference (5%) between body of table means: 0.108

^{The table} of means for each of the interactions for variables V1 to V6 (Stage A) are ^{summarized} below in Tables 4.1 to 4.15. The interpretation of the significant ^{-ariables} and two-factor interactions are addressed at the end of Stage A.

			V2		
erenera a energenda		(-1)	(+1)	Means	
V1	(-1)	0.081	0.069	0.075	
an a garden and	(+1)	0.071	0.045	0.058	
Means		0.076	0.058	0.067	

Table 4.1Donor exercise levels (V1) vs Donor blood group (V2)

			V3		
		(-1)	(+1)	Means	
V1	(-1)	0.058	0.092	0.075	
	(+1)	0.044	0.072	0.058	
Means		0.051	0.082	0.067	

Table 4.2Donor exercise levels (V1) vs Bleeding time (V3)

	<u> </u>		V3		
		(-1)	(+1)	Means	
V2	(-1)	0.101	0.051	0.076	
	(+1)	0.001	0.113	0.057	-
Means		0.051	0.082	0.067	

Table 4.3Donor Blood group (V2) vs Bleeding time (V3)

			V4		
		(-1)	(+1)	Means	
V1	(-1)	-0.054	0.204	0.075	
	(+1)	0.026	0.090	0.058	
Means		-0.014	0.147	0.067	

Table 4.4Donor exercise levels (V1) vs Anticoagulant (V4)

			V4	
		(-1)	(+1)	Means
V2	(-1)	-0.028	0.179	0.076
	(+1)	-0.000	0.115	0.057
Means		-0.014	0.147	0.066

Table 4.5Donor blood group (V2) vs Anticoagulant (V4)

			V4		
		(-1)	(+1)	Means	
V3	(-1)	-0.025	0.128	0.051	
	(+1)	-0.003	0.167	0.082	
Means		-0.014	0.147	0.067	

Table 4.6Bleeding time (V3) vs Anticoagulant (V4)

			V5		
		(-1)	(+1)	Means	
V1	(-1)	-0.060	0.210	0.075	
	(+1)	-0.053	0.169	0.058	
Means		-0.056	0.189	0.067	

Table 4.7Donor exercise levels (V1) vs Pre-process delay (V5)

	······································		V5		
		(-1)	(+1)	Means	
∨2	(-1)	-0.039	0.191	0.076	
	(+1)	-0.073	0.187	0.057	
Means		-0.056	0.189	0.067	

Table 4.8Donor blood group (V2) vs Pre-process delay (V5)

			V5		
		(-1)	(+1)	Means	
V3	(-1)	-0.060	0.163	0.051	
	(+1)	-0.052	0.216	0.082	
Means	· · · · · · · · · · · · · · · · · · ·	-0.056	0.189	0.067	

Table 4.9Bleeding time (V3) vs Pre-process delay (V5)

			V5	
		(-1)	(+1)	Means
V4	(-1)	-0.133	0.105	-0.014
	(+1)	0.021	0.273	0.147
Means		-0.056	0.189	0.067

Table 4.10Anticoagulant (V4) vs Pre-process delay (V5)

			V6	
		(-1)	(+1)	Means
V1	(-1)	0.140	0.010	0.075
	(+1)	0.089	0.067	0.058
Means		0.115	0.018	0.067

Table 4.11Donor exercise levels (V1) vs Pre-process storage (V6)

			V6			
		(-1)	(+1)	Means		
V2	(-1)	0.140	0.012	0.076		
	(+1)	0.090	0.025	0.058		
Means		0.115	0.018	0.067		

 Table 4.12
 Donor blood group (V2) vs Pre-process storage (V6)

			V6				
		(-1)	(+1)	Means			
V3	(-1)	0.072	0.031	0.051			
	(+1)	0.158	0.006	0.082			
Means		0.115	0.018	0.067			

Table 4.13 Bleeding time (V3) vs Pre-process storage (V6)

			V6		
		(-1)	(+1)	Means	
V4	(-1)	0.017	-0.045	-0.014	
	(+1)	0.212	0.082	0.147	
Means		0.115	0.018	0.067	

Table 4.14Anticoagulant (V4) vs Pre-process storage (V6)

			V6	
		(-1)	(+1)	Means
V5	(-1)	0.024	-0.136	-0.056
	(+1)	0.206	0.173	0.189
Means		0.115	0.018	0.067

*

Table 4.15Pre-process delay (V5) vs Pre-process storage (V6)

The results showed that the significant variables in the pre - post phase in the Creparation of FVIII were variables V4 (p = 0.0001), being the type of acticoagulant used, V5 (p = 0.0001) being the pre-process time delay and V6 (p = 0.0142) being the pre-process storage temperature.

 74 was the type of anticoagulant, which yielded a higher value for factor level $^{-1)}$, which was the anticoagulant CPD, than over factor level (-1), being heparin.

V5 was the variable controlling the pre-processing time delay and here once again, the factor level (+1) being a processing time under 6 hours, gave a higher value than the factor level (-1) which was a processing delay of 12 hours. V6 showed the opposite effect in which the factor level (-1), being a storage temperature of 20° C prior to processing, gave a significantly higher value than the factor level (-1), which was a storage temperature of 4° C. In addition there were two significant interactions, that in Table 4.3 and Table 4.4.

Table 4.3 reflects a significant interaction between the donor blood group (V2) and the electing time (V3) (p = 0.0376). A significant interaction indicates that the ^{a fference} between the levels of one factor, is not the same at each level of the second factor. For example, in Table 4.3 the difference between V3 at factor level 10^{-10} of V2 were 0.051 - 0.101 = -0.050, whilst at factor level (+1) of V2, the ^{2 ference} was 0.113 - 0.001 = 0.112. This is a difference which is to be ^{compared} with the value 0.108. The analysis indicated that the difference of these 2 "erences is 0.112 - (-0.050) = 0.162, which was significant and measures an nteraction. It can be seen that the effect of variable V3 was not consistent over the levels of variable V2, when we measured the effect of a factor by the ^{ofference} in the variable levels. Equivalently, it could be said that the effect of rariable V2 was not consistent over the factor levels of V3, and the difference in two-factor levels for variable V2 was different for each factor level of variable $^{/3.}$ In practical terms, if a high measurement of FVIII was to be achieved, then as far as variables V2 and V3 were concerned, both variables at (-1) factor level or coth at (+1) factor level were not a viable option. The ideal combination would be one of two options: Group A donors bled in a bleeding time of longer than 8 minutes or other blood groups, other than A, bled in under 8 minutes.

The only other significant interaction in this phase was the association of donor exercise levels (V1) with the type of anticoagulant used (V4), presented in Table 4.4 'p = 0.0136). This table shows that at level (-1) of V1, level (+1) of V4 was significantly greater than level (-1) of V4. At level (+1) of V1 there was no significant difference between the factor levels of V4. Clearly the combination of -10 of V4, CPD anticoagulant and level (-1) of V1 with no degree of donor exercise, produced the highest value of FVIII.

Using the data from Appendix III, under Factor VIII - Production, the standard errors SE for the means in Tables 4.16 to 4.28 in Stage B are as follows:-

er of	marginal means :	1.069
SE of	body of table means :	1.511

-east significant difference (5%) between body of table means: 5.92

The interpretation of the data was outlined.

			V11		
		(-1)	(+1)	Means	
V7	(-1)	10.85	10.22	10.53	
	(+1)	11.51	13.00	12.26	
Means		11.18	11.61	11.40	

Table 4.16Thawing temperature (V7) vs Centrifugation (V11)

			V11		
		(-1)	(+1)	Means	
V8	(-1)	11.76	10.38	11.07	
	(+1)	10.59	12.89	11.72	
Means		11.18	11.61	11.40	

Table 4.17Freezing rate (V8) vs Centrifugation (V11)

	<u>. </u>		V11		
		(-1)	(+1)	Means	
V9	(-1)	8.61	10.63	9.62	
	(+1)	13.75	12.59	13.17	
Means		11.18	11.61	11.40	

Table 4.18Freezing temperature (V9) vs Centrifugation (V11)

	<u> </u>		V11		
		(-1)	(+1)	Means	
V10	(-1)	10.27	9.70	9.99	
	(+1)	12.09	13.53	12.81	
Means		11.18	11.61	11.40	

Table 4.19Freezing technique (V10) vs Centrifugation (V11)

		V12			
		(-1)	(+1)	Means	
V11	(-1)	10.77	11.59	11.18	
	(+1)	11.56	11.66	11.61	
Means		11.16	11.63	11.40	

Table 4.20Centrifugation (V11) vs Holding time (V12)

		V13		
		(-1)	(+1)	Means
V7	(-1)	9.59	11.48	10.53
	(+1)	12.50	12.01	12.26
Means		11.05	11.75	11.40

 Table 4.21
 Thawing temperature (V7) vs Thawing technique (V13)

		V13			
		(-1)	(+1)	Means	
V8	(-1)	10.80	11.35	11.07	
	(+1)	11.29	12.15	11.72	
Means		11.05	11.76	11.40	

Table 4.22Freezing rate (V8) vs Thawing technique (V13)

		V13			
		(-1)	(+1)	Means	
V9	(-1)	9.71	9.53	9.62	
	(+1)	12.38	13.96	13.17	
Means		11.05	11.75	11.40	

 Table 4.23
 Freezing Temperature (V9) vs Thawing technique (V13)

		V13		
		(-1)	(+1)	Means
V10	(-1)	9.38	10.60	9.99
	(+1)	12.72	12.90	12.81
Means		11.05	11.75	11.40

 Table 4.24
 Freezing technique (V10) vs Thawing technique (V13)

			V13			
		(-1)	(+1)	Means		
V11	(-1)	11.28	11.08	11.18		
	(+1)	10.81	12.41	11.61		
Means		11.05	11.75	11.04		

Table 4.25Centrifugation (V11) vs Thawing Technique (V13)

			V13		
		(-1)	(+1)	Means	
V12	(-1)	13.98	8.35	11.16	
	(+1)	8.11	15.14	11.63	
Means		11.05	11.75	11.40	

Table 4.26Holding Time (V12) vs Thawing technique (V13)

			V14			
		(-1)	(+1)	Means		
V11	(-1)	9.38	12.97	11.18		
	(+1)	11.24	11.98	11.61		
Means		10.31	12.48	11.40		

Table 4.27Centrifugation (V11) vs Precipitation (V14)

			V14			
		(-1)	(+1)	Means		
V13	(-1)	9.46	12.63	11.05		
	(+1)	11.17	12.32	11.75		
Means		10.31	12.48	11.40		

 Table 4.28
 Thawing technique (V13) vs Precipitation (V14)

Variable V9, that of freezing temperature, proved to be significant in this FVIII assay (p = 0.0207). The level (+1) produced a significantly higher value of 13.17 than level (-1) with a value of 9.62.

In the assay results, a large outlier of 51.09 U/ml had an influence on the results of variable V10, freezing technique. There was some indication of a difference between the levels of V10 (p = 0.0696), freezing in either an alcohol/dry ice bath, or freezing in the vapour of a liquid nitrogen tank. The variable was confounded, so the significance is uncertain, but at the same time the difference was less marked when the outlier was omitted (p = 0.1159).

There was a confounded interaction evident in Table 4.26 with the interaction of folding time (V12) versus thawing technique (V13). Due to the confounding by V4, the type of anticoagulant used, the effect was uncertain but the significance was cossibly due to the type of thawing technique used (p = 0.0001).

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4.2 FIBRINOGEN

^{-Sing} the data from Appendix III, under Fibrinogen Post/Pre, the standard errors ^{SE)} for the means in Tables 4.29 to 4.43 in Stage A are as follows:-

SE of marginal means : 0.050 SE of body of table means : 0.071 -sast significant difference (5%) between body of table means: 0.199

^{The table} of means for variables V1 to V6 for the fibrinogen assay are given in ^{Tables} 4.29 to 4.43. Significant variables and their two-factor interactions are ^{Explained} at the end of the section.

			V2		
		(-1)	(+1)	Means	
V1	(-1)	-0.195	-0.069	-0.132	
	(+1)	-0.098	-0.053	-0.075	
Means		-0.147	0.060	-0.103	

Table 4.29Donor exercise levels (V1) vs Donor blood group (V2)

			V3		
		(-1)	(+1)	Means	
V1	(-1)	-0.183	-0.080	-0.131	
	(+1)	-0.094	-0.056	-0.075	
Means		-0.139	-0.068	-0.103	

Table 4.30Donor exercise levels (V1) vs Bleeding time (V3)

			V3	
		(-1)	(+1)	Means
V2	(-1)	-0.185	-0.108	-0.147
	(+1)	-0.093	-0.028	-0.060
Means		-0.138	-0.068	-0.103

Table 4.31Donor blood group (V2) vs Bleeding time (V3)

			 V4	
		(-1)	(+1)	Means
V1	(-1)	-0.184	-0.080	-0.132
	(+1)	0.008	-0.158	-0.075
Means		-0.088	-0.119	-0.103

Table 4.32Donor exercise levels (V1) vs Anticoagulant (V4)

			V4		_
		(-1)	(+1)	Means	
V2	(-1)	-0.154	-0.139	-0.147	
	(+1)	-0.023	-0.098	-0.060	
Means		-0.088	-0.119	-0.103	

Table 4.33Donor blood group (V2) vs Anticoagulant (V4)

			V4		
		(-1)	(+1)	Means	
V3	(-1)	-0.132	-0.146	-0.139	
	(+1)	-0.045	-0.091	-0.068	
Means		-0.088	-0.119	-0.103	

Table 4.34Bleeding time (V3) vs Anticoagulant (V4)

			V5	
		(-1)	(+1)	Means
V1	(-1)	-0.155	-0.108	-0.132
	(+1)	-0.071	-0.079	-0.075
Means		-0.113	-0.094	-0.103

Table 4.35Donor exercise levels (V1) vs Pre-process delay (V5)

			V5		
1 		(-1)	(+1)	Means	
∨2	(-1)	-0.196	-0.098	-0.147	
	(+1)	-0.030	-0.091	-0.060	
Means		-0.113	-0.094	-0.103	

Table 4.36Donor blood group (V2) vs Pre-process delay (V5)

			V5	
		(-1)	(+1)	Means
V3	(-1)	-0.113	-0.165	-0.139
	(+1)	-0.113	-0.023	-0.068
Means		-0.113	-0.094	-0.103

Table 4.37Bleeding time (V3) vs Pre-process delay (V5)

			V5	
		(-1)	(+1)	Means
V4	(-1)	0.024	-0.200	-0.088
	(+1)	-0.250	0.012	-0.119
Means		-0.113	-0.094	-0.103

Table 4.38Anticoagulant (V4) vs Pre-process delay (V5)

			V6	
		(-1)	(+1)	Means
V1	(-1)	-0.002	-0.261	-0.131
	(+1)	-0.058	-0.093	-0.075
Means	-	-0.030	-0.177	-0.103

 Table 4.39
 Donor exercise levels (V1) vs Pre-process storage (V6)

			V6		
		(-1)	(+1)	Means	
V2	(-1)	-0.031	-0.262	-0.147	
	(+1)	-0.029	-0.092	-0.060	
Means		-0.030	-0.177	-0.103	

Table 4.40Donor blood group (V2) vs Pre-process storage (V6)

			V6	
	_	(-1)	(+1)	Means
٧3	(-1)	-0.031	-0.247	-0.139
	(+1)	-0.028	-0.108	-0.068
Means		-0.030	-0.177	-0.103

Table 4.41Bleeding time (V3) vs Pre-process storage (V6)

			V6	·······	
		(-1)	(+1)	Means	
V4	(-1)	0.005	-0.181	-0.088	
	(+1)	-0.064	-0.173	-0.119	
Means		-0.030	-0.177	-0.103	

Table 4.42Anticoagulant (V4) vs Pre-process storage (V6)

			V6	
	_	(-1)	(+1)	Means
V5	(-1)	-0.038	-0.188	-0.113
	(+1)	-0.022	-0.166	-0.094
Means		-0.030	-0.177	-0.103

Table 4.43Pre-process delay (V5) vs Pre-process storage (V6)

^{Chiy} one variable, V6 was significant independently of the other variables in this ^{chase}, that being the storage temperature prior to the separation of the red cells ^{and} plasma (p = 0.0402). The factor (+1) level, the temperature of 4°C produced ^a slightly lower value than the factor level (-1) with a temperature of 20°C.

^{Chiy} one interaction, that in Table 4.38, was significant (p = 0.009) and another ^{Table} 4.32 was close to significance (p = 0.060). Table 4.38, the highest value was produced when the factors were at the same revels, and the lowest value when they were at different factor levels. The significant interaction indicated in this table was the combination of the type of anticoagulant (V4) in conjunction with a time delay prior to processing (V5). In Table 4.32, the interaction between donor exercise levels (V1) and the type of anticoagulant used (V4), was close to significance. In the table of means for this interaction, the reverse was observed. The lowest value was produced when the factors were at the same levels, and the highest value when the factors were at different levels. Thus the lowest level was obtained when the CPD anticoagulant was used with exercised donors, and heparin with non exercise i blood donors. The

exercised blood donors.

Using the data from Appendix III, under Fibrinogen Production, the standard errors (SE) for the means in Tables 4.44 to 4.56 for Stage B are as follows:-

^{high} level resulted when CPD was used on non exercised donors and heparin on

 $\frac{52}{52}$ of marginal means : 0.54 $\frac{52}{52}$ of body of table means : 0.77

Least significant difference (5%) between body of table means: 2.16

^{display.} Of importance in this assay is that there are no carry-over effects from the production Stage B.

			V11		
		(-1)	(+1)	Means	_
V7	(-1)	6.88	8.48	7.68	
	(+1)	9.30	9.66	9.48	
Means		8.09	9.07	8.58	

Table 4.44Thawing temperature (V7) vs Centrifugation (V11)

			V11		_
		(-1)	(+1)	Means	
V8	(-1)	7.17	8.91	8.04	
	(+1)	9.00	9.23	9.12	
Means		8.09	9.07	8.58	

Table 4.45Freezing rate (V8) vs Centrifugation (V11)

			V11		
		(-1)	(+1)	Means	
V9	(-1)	6.47	8.30	7.39	
	(+1)	9.70	9.84	9.77	
Means	······	8.09	9.07	8.58	

Table 4.46Freezing temperature (V9) vs Centrifugation (V11)

	· · · · · · · · · · · · · · · · · · ·		V11		
		(-1)	(+1)	Means	
V10	(-1)	7.34	7.53	7.44	
	(+1)	8.83	10.61	9.72	
Means		8.09	9.07	8.58	

Table 4.47Freezing technique (V10) vs Centrifugation (V11)

			V12		
		(-1)	(+1)	Means	
V11	(-1)	7.42	8.76	8.09	
	(+1)	8.85	9.29	9.07	
Means		8.13	9.02	8.58	

Table 4.48Centrifugation (V11) vs Holding time (V12)

			V13		
		(-1)	(+1)	Means	
V7	(-1)	7.78	7.57	7.68	
	(+1)	9.79	9.17	9.48	
Means		8.79	8.37	8.58	

Table 4.49Thawing temperature (V7) vs Thawing technique (V13)

			V13	
		(-1)	(+1)	Means
V8	(-1)	8.19	7.88	8.04
	(+1)	9.38	8.86	9.12
Means		8.79	8.37	8.58

Table 4.50Freezing rate (V8) vs Thawing technique (V13)

			V13		
		(-1)	(+1)	Means	
V9	(-1)	6.38	8.39	7.39	
	(+1)	11.19	8.35	9.77	
Means		8.79	8.37	8.58	

Table 4.51Freezing Temperature (V9) vs Thawing technique (V13)

			V13	
	<u></u>	(-1)	(+1)	Means
V10	(-1)	7.39	7.48	7.44
	(+1)	10.18	9.26	9.72
Means		8.79	8.37	8.58

Table 4.52Freezing technique (V10) vs Thawing technique (V13)

			V13		
	<u> </u>	(-1)	(+1)	Means	
V11	(-1)	8.87	7.31	8.09	
	(+1)	8.71	9.44	9.07	
Means		8.79	8.37	8.58	

Table 4.53Centrifugation (V11) vs Thawing Technique (V13)

			V13		
		(-1)	(+1)	Means	
V12	(-1)	8.27	8.00	8.13	
	(+1)	9.31	8.74	9.02	
Means		8.79	8.37	8.58	

Table 4.54Holding Time (V12) vs Thawing technique (V13)

	<u> </u>		V14		
		(-1)	(+1)	Means	
V11	(-1)	6.59	9.58	8.09	
	(+1)	8.82	9.32	9.07	
Means		7.71	9.45	8.58	

Table 4.55Centrifugation (V11) vs Precipitation (V14)

	-		V14		
		(-1)	(+1)	Means	
V13	(-1)	7.41	10.16	8.79	
	(+1)	8.00	8.74	8.37	
Means		7.71	9.45	8.58	

Table 4.56Thawing technique (V13) vs Precipitation (V14)

The variables V7 (thawing temperature p = 0.0211), V9 (freezing temperature p = 0.0025)), V10 (freezing technique p = 0.0038) and V14 (precipitation p = 0.0255), were all significant. Nevertheless, V10 and V14 were confounded. In each case, level (+1) had a significantly higher value than level (-1). To explain further, the thawing temperature at 4°C, the freezing temperature at >-60°C, the freezing technique in alcohol/dry ice and precipitation by means of a second spin, all produced a higher value, but due to the confounding effect of V10 and V14, is difficult to comment on their relevance.

The interaction between the freezing temperature (V9) and the thawing technique $\frac{1}{13}$ in Table 4.51, was significant and was not confounded (p = 0.0021). Although the freezing temperature was significant when used in combination with the thawing technique, it is only at the factor level (-1) of V13 that V9 showed significance. The factor level (-1) of the thawing technique was that of the plasma backs placed on a moving rack in a water bath of constant water. Therefore the freezing temperature only became relevant under this thawing condition, to produce hotable fibrinogen results.

4.3 VON WILLERBRAND FACTOR

Jsing the data from Appendix III, under vWF Post/Pre, the standard errors (SE) for the means in Tables 4.57 to 4.71 in Stage A are as follows:

SE	of	marginal means :	5.07
SE	of	body of table means :	7.18

Least significant difference (5%) between body of table means: 20.13 The tables of means for variables V1 to V6 for vWF are shown in the Tables 4.57 to 4.71. The significant variables and their two-factor interactions are discussed at the end of the section.

			V2		
		(-1)	(+1)	Means	
V1	(-1)	4.03	-11.17	-3.57	
	(+1)	-5.14	1.20	-1.97	
Means		-0.55	- 4.98	-2.77	

Table 4.57Donor exercise levels (V1) vs Donor blood group (V2)

			٧3		
		(-1)	(+1)	Means	
V1	(-1)	-15.38	8.23	-3.57	
	(+1)	- 2.17	-1.77	-1.97	
Means		-8.77	3.23	-2.77	

Table 4.58Donor exercise levels (V1) vs Bleeding time (V3)

			V3	
		(-1)	(+1)	Means
V2	(-1)	-8.92	7.81	-0.55
	(+1)	-8.63	-1.34	-4.98
Means		-8.77	3.23	-2.77

Table 4.59Donor blood group (V2) vs Bleeding time (V3)

			V4	
		(-1)	(+1)	Means
V1	(-1)	1.17	-8.31	-3.57
	(+1)	-7.55	3.61	-1.97
Means		-3.19	-2.35	-2.77

Table 4.60Donor exercise levels (V1) vs Anticoagulant (V4)

	· · · · · · · · · · · · · · · · · · ·		V4		
.		(-1)	(+1)	Means	
V2	(-1)	-1.23	0.13	-0.55	_
	(+1)	-5.14	-4.83	-4.98	
Means		-3.19	-2.35	-2.77	_

Table 4.61Donor blood group (V2) vs Anticoagulant (V4)

			V4		
		(-1)	(+1)	Means	
V3	(-1)	-9.64	-7.91	-8.77	
	(+1)	3.27	3.20	3.23	
Means		-3.19	-2.35	-2.77	

Table 4.62Bleeding time (V3) vs Anticoagulant (V4)

			V5		
		(-1)	(+1)	Means	
V1	(-1)	-2.66	-4.48	-3.57	
	(+1)	-8.33	4.39	-1.97	
Means		-5.49	-0.05	-2.77	

Table 4.63Donor exercise levels (V1) vs Pre-process delay (V5)

			V5		
		(-1)	(+1)	Means	
V2	(-1)	-9.74	8.63	-0.55	
	(+1)	-1.25	-8.72	-4.98	
Means		-5.49	-0.05	-2.77	

Table 4.64Donor blood group (V2) vs Pre-process delay (V5)

		I	V5			
		(-1)	(+1)	Means		
V3	(-1)	-19.52	1.97	-8.77		
	(+1)	8.53	-2.06	3.23		
Means		-5.49	-0.05	-2.77		

Table 4.65Bleeding time (V3) vs Pre-process delay (V5)

			V5		
		(-1)	(+1)	Means	
V4	(-1)	-0.133	0.105	-3.19	
	(+1)	0.021	0.273	-2.35	
Means		-5.49	-0.05	-2.77	

Table 4.66Anticoagulant (V4) vs Pre-process delay (V5)
			V6	····	
		(-1)	(+1)	Means	
V1	(-1)	4.50	-11.64	-3.57	
	(+1)	-8.88	4.94	-1.97	
Means		-2.19	-3.35	-2.77	

Table 4.67Donor exercise levels (V1) vs Pre-process storage (V6)

			V6		
		(-1)	(+1)	Means	
V2	(-1)	1.84	-2.95	-0.55	
	(+1)	-6.22	-3.75	-4.98	
Means		-2.19	-3.35	-2.77	

Table 4.68Donor blood group (V2) vs Pre-process storage (V6)

			V6			
		(-1)	(+1)	Means		
V3	(-1)	-10.97	-6.58	-8.77		
	(+1)	6.59	-0.13	3.23		
Means		-2.19	-3.35	-2.77		

Table 4.69Bleeding time (V3) vs Pre-process storage (V6)

			V6	
		(-1)	(+1)	Means
V4	(-1)	0.188	-6.56	-3.19
	(+1)	-4.56	-0.14	-2.35
Means		-2.19	-3.35	-2.77

Table 4.70Anticoagulant (V4) vs Pre-process storage (V6)

			V6		
		(-1)	(+1)	Means	
V5	(-1)	-3.47	-7.52	-5.49	
	(+1)	-0.91	0.81	-0.05	
Means		-2.19	-3.35	-2.77	

Table 4.71Pre-process delay (V5) vs Pre-process storage (V6)

None of the variables V1 to V6 in Stage A, Tables 4.57 - 4.71, in this assay were significant when viewed individually. This then indicated that either the factor level -1 or (+1) of each variable, may have been chosen. However, two interactions were significant, one in Table 4.65 and the other in Table 4.67. The interaction in Table 4.64 was close to significance (p = 0.0749).

The table of means for Table 4.65, which involves the variables relating to cleeding time (V3) and pre-process delay (V5), the interaction effect was clear (p \approx 0.0276). If one were looking for the factor level of each variable separately which produced the highest value, then the level (+1) for each variable would have ceen selected. However, Table 4.65 indicated that the level (-1) should be taken for V5, if V3 was taken at level (+1). In other words a pre-process delay for 12 hours in combination with a bleeding time of less than 8 minutes was signific ant.

¹ the table of means for Table 4.67, the interaction between donor exercise levels V1 and pre-process storage temperatures (V6) was also significant (p = 0.0394). ^{There} was very little difference between the factor levels of each variable when considered separately, but in combination, a high value was obtained when the factors were at the same level (-1) for V1 and V6, or level (+1) factor for V1 and V6. This implies that, non exercised blood donors produced a high value when their blood was stored at 20°C prior to processing, or exercised blood donors produced a high value when their blood was stored at 4°C.

There was an indication of an interaction in Table 4.64 between the donor blood group (V2) and the pre-process time delay prior to processing (V5), in that it approached significance (p = 0.0749). In the table of means the marginal mean (5.07) suggested that the lowest value was obtained with factor level (-1) of V5 and factor level (+1) of V2, but the table indicated that a low level value was obtained when the variables were at the same factor levels. The interpretation geing that Group A blood donors, in conjunction with a pre-process delay of less than 6 hours, was meaningful as well as when other blood groups (other than Group A) were linked with a pre-process delay of 12 hours.

^{Using} the data from Appendix III, under von Willebrand Factor Production, the ^{Standard} errors (SE) for the means in Tables 4.72 to 4.84 in Stage B are as ^{follows:-}

35 07	of	marginal means :	5.42
SE	of	body of table means :	7.66

<u>~</u>~

^{48ast} significant difference (5%) between body of table means: 21.23

The tables are first displayed and then explanation of the significant variables and their two-factor interactions are addressed.

			V11		
		(-1)	(+1)	Means	
٧7	(-1)	-38.03	-17.27	-27.65	
	(+1)	-27.21	-15.42	-21.32	
Means		-32.62	-16.35	-24.49	

Table 4.72Thawing temperature (V7) vs Centrifugation (V11)

			V11		
		(-1)	(+1)	Means	
V8	(-1)	-35.94	-14.33	-25.14	
	(+1)	-29.30	-18.36	-23.83	
Means		-32.62	-16.35	-24.49	

Table 4.73Freezing rate (V8) vs Centrifugation (V11)

			V11		
		(-1)	(+1)	Means	
V9	(-1)	-46.38	-28.55	-37.47	
	(+1)	-18.86	- 4.14	-11.50	
Means		-32.62	-16.35	-24.49	

Table 4.74Freezing temperature (V9) vs Centrifugation (V11)

			V11	
		(-1)	(+1)	Means
V10	(-1)	-40.11	-30.79	-35.45
	(+1)	-25.13	- 1.91	-13.52
Means		-32.62	-16.35	-24.49

 Table 4.75
 Freezing technique (V10) vs Centrifugation (V11)

			V12	
		(-1)	(+1)	Means
V11	(-1)	-40.91	-24.33	-32.62
	(+1)	-15.80	-16.89	-16.35
Means		-28.36	-20.61	-24.49

Table 4.76Centrifugation (V11) vs Holding time (V12)

			V13	
		(-1)	(+1)	Means
V7	(-1)	-28.44	-26.86	-27.65
	(+1)	-19.22	-23.41	-21.32
Means		-23.83	-25.14	-24.49

 Table 4.77
 Thawing temperature (V7) vs Thawing technique (V13)

			V13		
		(-1)	(+1)	Means	
V8	(-1)	-27.51	-22.77	-25.14	
	(+1)	-20.16	-27.51	-23.83	
Means		-23.83	-25.14	-24.49	

Table 4.78Freezing rate (V8) vs Thawing technique (V13)

			V13		
		(-1)	(+1)	Means	
V9	(-1)	-33.82	-41.12	-37.47	
	(+1)	-13.84	- 9.16	-11.50	
Means		-23.83	-25.14	-24.49	

 Table 4.79
 Freezing Temperature (V9) vs Thawing technique (V13)

			V13	
		(-1)	(+1)	Means
V10	(-1)	-35.00	-35.89	-35.45
	(+1)	-12.66	-14.38	-13.52
Means		-23.83	-25.14	-24.49

 Table 4.80
 Freezing technique (V10) vs Thawing technique (V13)

			V13		
		(-1)	(+1)	Means	
V11	(-1)	-27.97	-37.27	-32.62	
	(+1)	-19.69	-13.00	-16.35	
Means		-23.83	-25.14	-24.49	

Table 4.81Centrifugation (V11) vs Thawing Technique (V13)

			V13		
		(-1) (+1) Means			
V12	(-1)	-18.85	-37.87	-28.36	
	(+1)	-28.81	-12.41	-20.61	
Means		-23.83	-25.14	-24.49	

Table 4.82Holding Time (V12) vs Thawing technique (V13)

	<u> </u>	V14		
		(-1)	(+1)	Means
V11	(-1)	-37.08	-28.16	-32.62
	(+1)	-23.04	- 9.66	-16.35
Means	•	-30.06	-18.91	-24.49

Table 4.83Centrifugation (V11) vs Precipitation (V14)

			V14			
		(-1) (+1) Means				
V13	(-1)	-30.38	-17.28	-23.83		
	(+1)	-29.73	-20.54	-25.14		
Means		-30.06	-18.91	-24.49		

Table 4.84Thawing technique (V13) vs Precipitation (V14)

In the production phase, variables V9 (p = 0.0010), V10 (p = 0.0051) and V11 p = 0.0361) were significant. Both V9 and V11 were free of confounding, but V10 was confounded in that it experienced a carry over effect V3/V13. In each example of these variables, the level (+1) had a significantly higher value than the evel (-1). As a result, a freezing temperature of >-60°C, a rapid centrifugation of 4733 X g for 25 minutes and a freezing technique in alcohol/dry ice, were identified as production criteria which positively influenced the vWF assay.

The interaction of the holding time (V12) and thawing technique (V13) in Table $^{4.82}$, was significant (p = 0.0228), but was confounded with the carry over effect of the anticoagulant V4.

4.4 FIBRIN DEGRADATION PRODUCTS (FDP)

^{These} results were not be analyzed by statistical means as all the samples were ^{tested} by the qualitative screening test. Of the 128 samples analyzed, 7 were ^{found} to be reactive by means of an agglutination technique. The results are shown in Appendix II, 6 of the positive results were found in the pre sample taken from the blood donor prior to donation, indicating the presence of abnormal levels of XL-EDP in the plasma and that fibrinolysis was in progress. No semiqualitative tests were carried out on the positive samples because the degree of fibrinolysis was of no relevance at the time.

Of significance was the fact that Design Number 11 whose blood donors were Group A and not exercised, yielded a positive result with Run 1 and 3. In Run 3 Design 11, a positive result was also detected in the post sample (the sample taken prior to the separation of the red cells and plasma), but a negative result obtained in the final product. Despite the evidence of fibrinolysis, the FVIII yield was 18.66 U/ml, however heparin was the anticoagulant used, which could have accounted for the excellent FVIII result. The positive result in the pre sample taken from Design 21 was also from a Group A non exercised donor. The donors were cied over a timeframe of eight weeks, however care was taken to ensure that personnel remained constant, in order to avoid differences in phlebotomy techniques. The positive results obtained, had no influence on the vWF and "brinogen assay results.

^{4.5} pH

^{The} pH results ranged between 7.25 - 8.10, indicating that the myriad production ^{variables}, did not cause significant changes in pH fluctuations. The statistical ^{assessment} demonstrated that during Stage A, prior to separation of the red cells

In the plasma, the storage temperature (V6) had a significant influence on the i(p = 0.0095). The interaction of donor exercise levels (V1) and pre-process storage temperature (V6) approached significance (p = 0.0649), and the table of means is as follows:

SE of	marginal means :	0.026
SE of	body of table means :	0.037

Least significant difference (5%) between body of table means: 0.105

	V6				
		(-1) (+1) Means			
V1	(-1)	0.099	0.267	0.183	
	(+1)	0.121	0.150	0.136	
Means		0.110	0.208	0.159	

 Table 4.85
 Donor exercise levels (V1) vs Pre-process storage (V6)

^{Variable} V6 was significant at level (-1) of V1. There was no significant difference ^{att}evel (+1). In other words V6, being the pre-process storage temperature, was ^{significant} at the (-1) level. This involved a storage temperature of 20°C prior to ^{separation}, but not at the (+1) level which was a temperature of 4°C, when joined ^{with} V1, which were exercised blood donors.

When examining the data from the final samples, variables V7 (thawing temperature p = 0.0247), V8 (freezing rate p = 0.0032), V10 (freezing technique c = 0.0373) and V14 (precipitation p = 0.0461) were all found to be significant as individual variables. However V8, V10 and V14 were confounded. The interaction of the holding time (V12) by the thawing technique (V13), was

significant, but also confounded V4, the type of anticoagulant used (p = 0.0003). The interaction of the freezing technique (V9) by the thawing technique (V13) was significant and free from confounding (p = 0.0079). The table of means for these variables is displayed in Table 4.86 below.

	<u> </u>		V13	
		(-1)	(+1)	Means
V9	(-1)	-0.146	-0.062	-0.104
* 	(+1)	-0.077	-0.123	-0.100
Means		-0.112	-0.092	-0.102

Table 4.86Freezing temperature (V9) vs Thawing technique (V13)

SE of marginal means :	0.017
SE of body of table means :	0.024

Least significant difference (5%) between body of table means: 0.067

The interpretation of this interaction was that the freezing temperature at either ^{-35°}C or >-60°C, was meaningful in unification with the thawing technique in ^{which} it made no difference whether the water in the thawing bath was circulating ^{or} whether it was stationary.

4.6 EVALUATION OF PLASMA PROTEINS AND ELECTROLYTES

The following plasma proteins and electrolytes were measured and evaluated. Each assay was also analyzed by statistical means.

- Magnesium (Mg)
- Total Protein (TP)
- ^{*} Albumin (ALB)
- Calcium (Ca)
- Alanine Aminotransferase (ALT)
- Sodium (Na)
- Potassium (K)
- Chloride (CI)

4.6.1 MAGNESIUM

The statistical analysis demonstrated that during Stage A, prior to separation of the red cells from the plasma, that the type of anticoagulant used (V4), had a close to significant (p = 0.0518) influence on the magnesium determination. Level (+1), peing CPD, produced a higher value than level (-1) which was heparin. The atteraction of donor exercise levels (V1) and donor blood group (V2), and the pre-processing time delay (V5) and pre-process storage temperature (V6), were significant (p = 0.0373 and 0.0294) and the table of means is as follows:

SE of ma	rginal means :	0.016
SE of boo	ly of table means :	0.022

	Least significant dif	fference (5%)	between body	/ of table me	eans: 0.062
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			V2		
		(-1)	(+1)	Means	
V1	(-1)	-0.166	-0.093	-0.130	
	(+1)	-0.083	-0.103	-0.093	
Means		-0.124	-0.098	-0.111	

Table 4.87Donor exercise levels (V1) vs Donor blood group (V2)

	<u></u>		V6	
		(-1)	(+1)	Means
V5	(-1)	-0.096	-0.119	-0.107
	(+1)	-0.152	-0.078	-0.115
Means		-0.124	-0.099	-0.111

Table 4.88Pre-process delay (V5) vs Pre-process storage (V6)

^a Table 4.87, the smallest value was produced when both the variables were at ^e/el (-1). In summary, this occurred when blood donors were not exercised and ^{their} blood group was other than Blood Group A. There was no difference between ^{other} combinations of the variables.

^{Table 4.88} demonstrates that the smallest value was created when V5 was at level (-1) and V6 was at level (-1). To expand further, when a pre-processing delay of ^{<6} hours was used in conjunction with a pre-storage temperature of 20°C, the ^{nteraction} was of notable importance. There was no difference between other ^{associations} of the variables.

When the data of the production phase was analyzed for this assay, no effects were found to be significant. The interaction V12 and V13, which was confounded, approached significance (p = 0.0653).

4.6.2 TOTAL PROTEIN

The review of the data for this assay in Stage A of the manufacturing process, prought to light the significance of variables V1, donor exercise levels p = 0.0358) and V4, type of anticoagulant used (p = 0.0075). In both instances the level (+1) resulted in a higher value than the level (-1), i.e. these were exercised blood donors who were bled into donation packs containing CPD as the anticoagulant.

There was some indication of an interaction between V1 and V2 (p = 0.0903). The data for these factors were skewed and on transformation to normality, the Interaction became significant ((p = 0.0410). The table of means for the original Cata is as follows:

			V2	
		(-1)	(+1)	Means
V1	(-1)	-10.00	-4.38	-7.19
	(+1)	- 2.81	-3.60	-3.20
Means		- 6.41	-3.98	-5.201

Table 4.89Donor exercise levels (V1) vs Donor blood group (V2)

SE of marginal means : 1.32 SE of body of table means : 1.87

Least significant difference (5%) between body of table means: 3.72

In Stage B, one of the results was an outlier in comparison to the other results seen in Appendix II, Total Protein Production Run 4, Sample 15, with a reading of 9.0 g L. The analysis, with and without this value, produced no significant results, although with the outlier there was some indication of an interaction between V10 and V13, but was also confounded. In the analysis of carry-over effects, there was some indication of V5 having a significant carry over effect. This variable was not confounded.

4.6.3 ALBUMIN

^{There} was evidence of non-normality with the assay results for the data in Stage ^A of the manufacturing process. Analysis of the transformed data yielded ^{comparable} results. Variables V1 (p = 0.0167) and V4 (p = 0.0133) were ^sgnificant, being donor exercise levels and type of anticoagulant used. In each ^{case} the level (+1) produced a significantly higher value than the (-1) level. ^{Explained} in ordinary terms, this involved exercised blood donors being bler⁴ into ^{cicod} packs containing CPD. The same trend was evident for V6, which ^{approached} significance (p = 0.0699).

The interaction of V3 and V6 also approached significance (p = 0.0657) and the table of means is as follows:

			V6	
		(-1)	(+1)	Means
V3	(-1)	-4.12	-4.16	-4.14
	(+1)	-7.25	-3.22	-5.23
Means		-5.69	-3.69	-4.69

Table 4.90Bleeding time (V3) vs Pre-process storage (V6)

SE of marginal means : 0.77 SE of body of table means : 1.09

-east significant difference (5%) between body of table means: 3.06

From the analysis of all the results in the production phase, the data reflected V10 p = 0.0601) and V12 (p = 0.0558) being close to significance, however both /ariables were confounded. Four outlier results were recorded. The interaction of /10 and V13 although confounded, was significant (p = 0.0301). In the absence of the 4 outliers, V10 and V12 were no longer near significance, the interaction cetween V10 and V13 moved to only close to significance. The interaction between V12 and V13, although confounded, then became significant.

4.6.4 CALCIUM

^{In Stage} A of the calcium assay, only the type of anticoagulant used (V4), had a ^{Significant} effect (p = 0.0023). The level (-1) produced a higher value than the ^{Value} for level (+1). The level (-1) of V4, involved use of heparin as the ^{anticoagulant}. Calcium chloride had to be added to certain of the plasma in which ^{Geparin} had been added. The indication was that this had an influence on the data.

In Stage B of the manufacturing process, the presence of outliers was once again observed. No reasonable explanation for the cause was able to be established. With the omission of the outliers V10, freezing technique and V14, the precipitation method (confounded) became significant. It was also logical to accept that the oteraction between V10 and V13 represented a real effect and was significant. These two variables represent the freezing and thawing techniques.

4.6.5 ALANINE AMINOTRANSFERASE

^{14.} anticoagulant in Stage A was close to significance (p = 0.0587), with factor ^{evel} (-1) producing the larger value than (+1) factor level. The (-1) factor level for ^{In s} factor was heparin as the anticoagulant. Three interactions were significant, ¹⁴ by V3, V3 by V5 and V4 by V5.

The table of means for the three interactions is as follows:

SE of marginal means :1.66SE of body of table means :2.35

-^{east} significant difference (5%) between body of table means: 6.58

			V3		
		(-1)	(+1)	Means	
V1	(-1)	5.28	1.47	3.38	
	(+1)	-0.44	5.09	2.33	
Means		2.24	3.28	2.85	

Table 4.91Donor exercise levels (V1) vs Bleeding time (V3)

			V5		
		(-1)	(+1)	Means	
VЗ	(-1)	6.81	-1.97	2.42	
	(+1)	1.97	4.59	3.28	
Means		4.39	1.31	2.85	

Table 4.92Bleeding time (V3) vs Pre-process delay (V5)

			V5		
		(-1)	(+1)	Means	
V4	(-1)	9.16	1.03	5.09	
	(+1)	-0.38	1.59	0.61	
Means		4.39	1.31	2.85	

Table 4.93 Anticoagulant (V4) vs Pre-process delay (V5)

The data for this set of assay results contained four influential outliers. The rifuence of the outliers is discussed after the dialogue of the data analysis. The largest value was obtained in Table 4.91 when the variables were on the same -1) or (+1) factor levels. In other words, exercised blood donors bled within 8 minutes, or alternately non exercised blood donors who were bled in a bleeding time of longer than 8 minutes. The scenario in Table 4.92 was similar to the one above, in that V3 by V5 obtained the highest value when similar levels were ^{cbserved}. A unit of blood bled within 8 minutes, when processed within 6 hours, ^{produced} high yields. The reverse, being a bleeding time of longer than 8 minutes ^{processed} at 12 hours, also showed favourable results. At factor level (-1) of V4 th Table 4.93, there was a significant difference between the levels of V5, but no significant difference at level (+1) of V4, being heparin with a time delay before processing of up to 12 hours.

The outliers were found in Appendix II, under alanine aminotransferase Pre Run 4, Number 10; Post Run 1, Number 21; Post Run 2, Number 18 and Post Run 4, Number 14. If these are omitted from the analysis the results change as follows. Variable V4 and interaction V4 by V5 are no longer significant. The interaction of V3 by V5 remains the same, while that of V1 by V3 moves close to significance. V5. pre-process time delay by V6, pre-process storage temperature becomes significant.

The analysis of all the data for Stage B, showed V12 (confounded), V14 ^{confounded}) and the interaction V8 by V13 (confounded), to be significant o = 0.0249). In the absence of the outliers, V14 and the interaction V8 by V13, ^{remained} significant. V12, holding time was no longer important. However, V7, ^{thawing} temperature which was not confounded by other variables, became ^{significant}.

4.6.6 SODIUM

^{Variables} V4 and V6 in Stage A of this assay were both significant (p = 0.0001^{and} p = 0.0253). The factor level (+1) of V4, i.e. the use of CPD as the ^{anticoagulant}, produced a higher value than the factor level (-1). Similarly for V6, me pre-process storage temperature of 4°C, had a higher level (+1), than level (-1).

One interaction was significant, that between V1 by V2, with the table of means as follows:

SE of marginal means : 1.78 SE of body of table means : 2.51

Least significant difference (5%) between body of table means: 7.1

			V2	
		(-1)	(+1)	Means
V1	(-1)	31.0	38.9	35.0
	(+1)	40.3	37.5	38.9
Means		35.7	38.2	36.9

Table 4.94Donor exercise levels (V1) vs Donor Blood Group (V2)

^A significantly lower value was evident in Table 4.94, when both variables were ^{at level} (-1) factors. This implies that blood donors who did not exercise prior to ^{conation}, and were of any blood group type (other than Group A) when bled, and ^{their} plasma processed into cryoprecipitate, provided a good FVIII yield. No ^{significant} difference in values were produced by any of the other combinations. ^{The} production data produced no significant effect, although the holding time in ⁷¹², which was confounded, was close to significance (p = 0.0626). There were ^a number of outlying values present which could have had an influence on the ^{results}, but as there was no justification for their omission, they were included.

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Once again there was evidence of four outlying values. The decision was made to analyze the data with these excluded.

^a Stage A, the assay results, when analyzed, indicated three variables as being significant, all independent of each other. They were V3 (p = 0.082), V4 p = 0.0352) and V5 (p = 0.0001). V3, the factor level (+1) was a bleeding time under 8 minutes, having a greater factor level than (-1). For V4, anticoagulant and V5, pre-process time delay level (-1) was significantly greater than level (+1), meaning that heparin as the choice of anticoagulant used in conjunction with a preprocess delay of 12 hours, proved a suitable combination. The interaction of V5 by V6 was significant (p = 0.0112) and the table of means is as follows:

^{>= of} marginal means (approximately):	0.164
Se of body of table means (approx):	0.236

-sast significant difference (5%) between body of table means (approx): 0.662

			V6		
		(-1)	(+1)	Means	
V5	(-1)	-0.675	0.124	-0.276	
	(+1)	-1.106	-1.503	-1.305	
Means		-0.891	-0.690	-0.802	

Table 4.95Pre-process delay (V5) vs Pre-process storage (V6)

 $^{-3}$ Table 4.95, it was observed that the difference in levels of V5 at factor level

-1) of V6, was more than three times the magnitude of the difference at factor evel :-1) of V6.

in the examination of the data for Stage B, once again outliers were demonstrated total of 8), but as with the data of Stage A, these were omitted. No effects were found to be of any importance and no significant interactions were noted. Variables V10 and V14 were confounded, but were of significance, only when the outliers were omitted (p = 0, 0314).

4.6.8 CHLORIDE

The data for Stage A for this assay was skewed and required a transformation to cormality. The results of the analysis of the transformed data were virtually the same, except the transformation brought some interactions closer to significance. ¹⁴, the type of anticoagulant used, was significant (p = 0.0292). V1, V3 and V6 Were close to significance. The interactions of V1 by V3 and V3 by V4 were close to significance and the table of means for them is as follows:

- SE of marginal means : 1.57
- SE of body of table means : 2.26
- -sast significant difference (5%) between body of table means: 6.2

			V3		
		(-1)	(+1)	Means	
V1	(-1)	-23.0	-22.5	-22.8	
	(+1)	-14.8	-22.6	-18.7	
Means		-18.9	-22.6	2.85	

Table 4.96Donor exercise levels (V1) vs Bleeding time (V3)

	<u> </u>		V4		
		(-1)	(+1)	Means	
V3	(-1)	-19.5	-18.3	-18.9	
	(+1)	-26.9	-18.2	-22.6	
Means		-23.2	-18.3	-20.7	

Table 4.97Bleeding time (V3) vs Anticoagulant (V4)

Table 4.96 reflected a small decrease by the combination of factor level (+1) for 41, and factor level (-1) for V3. No other significant difference between the other combinations were seen. This meant that exercised donors bled into heparin anticoagulant, yielded an important effect. Table 4.97 shows that the greatest pecrease was produced by the association of factor level (+1) for V3 and factor evel (-1) for V4. No other significant differences between the other combinations there observed. In this case, of relevance, was a bleeding time of under 8 minutes combined with heparin as the anticoagulant.

⁵ the production stage, a number of outliers (11 in total) were noted and the ^{decision} was made to omit them. Interactions V8 by V13 (confounded) and V10 ^{ov} V13, were found to be significant. The freezing rate and freezing technique ^{'eflected} strong interactions with the technique utilized for the thawing of the ^{oryoprecipitate}.

CHAPTER 5

DISCUSSION

Several studies on the activity and stability of FVIII in blood and plasma have been made, in order to obtain a maximum yield of this labile factor in either plasma or cryoprecipitates (Carlebjork *et al.*, 1983). The aim of this study was to determine which variables actively had an effect on the FVIII yield. Blood collection and separation procedures all involve variables which have the potential of activating the coagulation system, thus affecting the yield of FVIII.

During the analysis of the FVIII data, it was found that variable V4, the type of anticoagulant used, was significant. The level of factor (+1) gave the highest value, which was the use of CPD as the primary anticoagulant, rather than adding heparin /calcium chloride combination after the donation. Although the opinion is that anticoagulants with lower levels of citrate are more beneficial in the generation of FVIII (Rock *et al.*, 1988) and that half strength citrate solutions should be utilised (Prowse *et al.*, 1987), in South Africa the registered anticoagulant viz. SAG-M (Sodium; adenine; glucose and mannitol) was registered in South Africa. It was not used for ^{our} study, as at the time of registration all the technical work had been completed. ^{Previous} studies by Rock *et al.* (1979); Krachmalnikoff and Thomas (1983); Mikaelsson *et al.* (1983) and Cumming *et al.* (1987), all confirmed the beneficial effect of heparin rather than CPD on the stability of plasma FVIII. This effect is due

to the presence of physiological ionised calcium levels in heparinised plasma. In all these studies heparin was the primary anticoagulant, which was not the case in our study due to regulatory implications by the Medicines Control Council (MCC). De Wit *et al.* (1986) on the other hand, found that the use of CPD as the primary anticoagulant was superior than heparin, which correlated well with the findings of our study. The FVIII assay statistical findings in our study indicated better FVIII yields when using CPD rather than heparin.

Variable V5, the pre-processing time delay of < 6 hours and V6 the pre-process storage temperature of 20°C, were both highlighted as significant variables according to the analysis, affecting the FVIII yield in the cryoprecipitate in a positive manner. Rock and Tittley (1979) found FVIII levels were significantly ^{higher} when whole blood was stored between 6 and 24 hours at 22°C, than when it was stored at 4°C before separation, Spivey et al. (1992) reported similar findings. Hughes et al. (1988) found FVIII to be better preserved over a 24 hour period when stored in whole blood at 22°C, than when stored in plasma at 22°C ^{or 4°C}, or in whole blood at 4°C, but at the same time, major losses of FVIII ^{Occurred} after a 6 hour processing delay and were dependent on temperature. FVIII recovery was 100% for 6 hour old plasma and 79% for 18 hour old plasma. Vermeer et al. (1976b) demonstrated that the temperature of stored whole blood should not decrease below 10°C, while Allersma et al. (1996) reported no significant difference in a processing delay of either 3 hours or 12 - 15 hours provided the temperature was 20°C. The investigation by Pietersz et al. (1989) ^{concluded} that the effect of rapid cooling to 20 -24 °C of whole blood immediately

after collection, using "cooling units" with butane-1,4-diol, prolonged storage for up to 24 hours with a 80% FVIII recovery of the initial value, and provided optimal conditions for blood component preparation. The findings in our study correlate well with the findings of the above authors, and is evident that these two variables, i.e. processing whole blood within six hours which has been stored at 20 - 24°C, are critical variables to which precise attention must be given.

The variable relating to blood groups was not found to be a significant variable on ts own. Previous reports by Preston and Barr (1964) and Jeremic et al. (1976), found Blood Group A to have a greater influence on the FVIII yield, although they were only investigating ABO blood group status at the time. However, in this study, blood groups (V2), showed a significance with the interaction of bleeding time (V3), specifically using Blood Group A donors, bled in a donation time of onger than 8 minutes. This correlates well with a study by Reiss and Katz (1976), in which they found no difference in platelet concentrate or FVIII quality from blood ^{collections} lasting between 8 and 12 minutes. It is suggested that the eight minute bleeding time is restrictive, and that blood collected from non-traumatic and freeflowing phlebotomies of up to 12 minutes be acceptable. The possibility of selecting high value donors such as Group A donors, along with the extended bleeding time, clearly are notable variables for the enhancement of FVIII quality. The interaction donor exercise levels (V1) and type of anticoagulant used (V4), was significant. The interaction showed that when using CPD as the anticoagulant, highest yields of FVIII were achieved when the blood donors were not exercised, which is contrary to the findings in the study by Van Gastel et al. (1973) and

Strand et al. (1974), who found that the FVIII activity was increased by 40%, when blood donors were exercised. Burka et al. (1975), proved exercise will double the measurable FVIII level in the donor's blood. The increase in activity is for a relatively short period, following strenuous muscular exercise, and it could well be that in many instances other variables call for a time delay before processing of the blood, which could affect the outcome of the FVIII yield, because the levels had already decreased. If there were some guarantee that all whole blood which was to be processed into cryoprecipitate could be processed within 2 - 3 hours, it would then be feasible to recommend that blood donors be exercised prior to their blood donation. This would also drastically reduce the number of units of blood available for FVIII production, as the majority of the whole blood is collected by mobile units. Transportation of donated blood at mobile clinics to the processing laboratory can be delayed, and not reach the processing laboratory within the deadline required ¹⁰ obtain the high FVIII level that was present on donation. Failure to meet this requirement makes the exercise stage of the donation procedure for the donors. which needs extra time, a worthless recommendation.

The freezing temperature (V9), proved to be significant in Stage B of the production cycle i.e. those variables involved in the process after the separation of the red cells and plasma. The freezing technique (V10), whether to use alcohol / dry ice baths or liquid nitrogen vapour, showed some indication of significance, but there was the presence of a large outlier (51,09 U/ml), which had an influence on the results, and in addition, the variable was confounded, so the significance is uncertain and for this reason no further consideration was given to its importance.

The interaction of the holding time, V12 (the delay before the final centrifugation) and thawing technique, V13 was significant, but due to confounding the effect was uncertain. Due to the nature of the variables, it was thought the effect was due to the thawing technique used, that of using a thawing water bath in which the water circulates at a fixed temperature, or that of the plasma fixed to moving arms of the water bath, in unmoving water. The freezing temperature was reached in two ways, a fast freeze at >-60°C or a slow freeze at -35°C. This study found that the fast freeze gave results that had higher FVIII yields, which compares favourably with a review by Farrugia and Prowse (1985), who also found the fast freeze was better for optimal yields of FVIII.In addition to the fast freeze, the plasma to be frozen must be of the same volume and compressed between metal plates, to make a thin plasma slab with even density, and placed in ethanol baths where energy transport is most effective (Carlebjork et al., 1986b). Kasper et al. (1975) along with Rock and Tittley (1979) found that very low freezing temperatures were unnecessary, however recommendations in later studies, vielded ^{a far} superior cryoprecipitate (Carlebjork et al., 1986b).

^{Many} different FVIII assay methods have been used to date. However, the ^{chromogenic} Coatest^R Factor VIII assay technique is easy to perform, with high ^{precision}, and is routinely used in the quality control of cryoprecipitate in many ^{laboratories} (Carlebjork *et al.*, 1987), replacing the formerly used one-stage clotting ^{method}. It is also in routine use at Western Province Blood Transfusion Service for ^{all} quality control FVIII assays on cryoprecipitates and concentrates.

Quantitatively, fibrinogen is the major protein constituent in cryoprecipitate and is an extremely stable plasma protein compared to FVIII (Howard *et al.*, 1991). Factor VIII and fibrinogen are classified together, because of biologic similarities and because their activity is destroyed during the coagulation process (Ness and Perkins, 1980). Despite these similar characteristics, the levels of fibrinogen and FVIII in a healthy blood donor are not necessarily correlated, i.e. a donor with an elevated level of FVIII may have a relatively low level of fibrinogen. The wide range of values cited in the literature, reflects the number of variables that can influence the yield of fibrinogen in cryoprecipitates. Hoffman *et al.* (1987) obtained an average of 100 mg of fibrinogen in their study. Higher values of 250 mg were acquired by Ness and Perkins (1980). Our result of 10.93 g/l correlated better with that of Smit Sibinga *et al.* (1988), who obtained a value of 15 g/l.

The storage temperature (V6) prior to separation of the red cells and plasma at a temperature of 20°C, showed to have a significant effect on the fibrinogen results in this study. In an earlier study by Hoffman *et al.* (1987), fibrinogen was found to be stable during 4 hours of storage at room temperature, whereas Saxena *et al.* (1991) found the fibrinogen content to decrease when whole blood was stored at 1 - 6°C, prior to processing. The type of anticoagulant, especially heparin, played a role in the determination of the higher fibrinogen content in the cryoprecipitate as well as the delay before processing. Individual variables which demonstrated an effect on fibrinogen levels during the production cycle were: a thawing temperature (V7) at 4°C, the freezing temperature (V9) at >-60°C, and a freezing technique (V10) using a combination of alcohol and dry ice and precipitation (V14), by means

of a second centrifugation spin. The interaction between the freezing temperature (V9) and the thawing technique (V13) was significant, with the emphasis on using a thawing water bath in which the packs were attached to a moving arm, and moved through the water which remained constant. As long as the plasma was frozen, the temperature at which this was carried out was immaterial.

The influence of the variables on the data for von Willebrand Factor, could not be referenced to any work done previously, as nobody has looked at the influence of the production variables on vWF. Variables which influence the outcome of the Von Willebrand Factor assay, prior to the separation of the red cells and plasma are: the bleeding time of the donor, the exercise level of the donor, the delay before separation, and the temperature at which whole blood was stored at before the removal of plasma. These variables were not of importance individually, but only became relevant when they interacted with each other. A donation time (V3) of under 8 minutes was consequential, only if the whole blood was reserved for 12 hours (V5) before processing. Hughes *et al.* (1988), found that the ratios of FVIII to vWF were 1.0 in both plasma and cryoprecipitate, stored for 6 hours prior to further processing, and were 0.7 : 0.5 in 18-hour old plasma.

^{If blood} donors are not requested to exercise (V1) prior to donation, this would only ^{be} significant if their blood were stored at 20°C (V6) before separation. ^{Conversely}, the opposite is also important. If whole blood is to be cooled to 4°C ^{prior} to separation, the blood donors should exercise prior to the donation. Most ^{cryo}precipitate production units usually do not request their donors to exercise

before donation, but attempt to cool the whole blood as much as possible before the plasma is removed, two procedures which seem acceptable on their own, but according to our study data, do not result in adequate vWF yields. The interaction between the blood group of the donor and the delay before separation of the plasma and red cells, was only close to significance (p = 0.0749), and for this reason did not warrant any relevance to the outcome of the study. In the next phase of the production cycle three individual variables became critical. The centrifugation speed to separate the red cells and plasma at 4733 x g (V11), fcllowed by freezing the plasma (V9) at >-60°C in alcohol/dry ice freezing bath V1, were of particular significance on the vWF data. The freezing technique experienced a confounded effect and could not be considered as relevant. The interaction of the thawing technique (V13) and time delay (V12), before finally snap-freezing the cryoprecipitate, was significant, but was confounded by the carry over effect of the type of anticoagulant used, and it was difficult to derive a final conclusion on these two variables.

The plasma concentration of cross-linked fibrin degradation products (FDP ^{containing} the D-dimer domain) in normal donors is usually less than 0.25 μ g/ml, ^{so} the pre starting sample from donors prior to their donation is expected to give ^a negative result. Concentrations of 0.25 μ g/ml FDP or more, will cause ^{agglutination} with the Dimertest^R Latex assay. Elevated D-dimer levels indicate the ^{degree} of coagulation and fibrinolytic activation (Sato *et al.*, 1995). A plasma ^{screening} test for FDP is of diagnostic value in disseminated intravascular ^{coagulation} (DIC), acute vascular diseases and other thrombotic episodes. The

amount of FDP detected in a sample will depend on several factors, such as the degree of coagulation, the rate of cross-linked fibrin formation, and time elapsed prior to testing. The D-dimer latex assay provides a sensitive tool to study the events leading to the production of fibrin from fibrinogen and activation of FVIII. This test, when performed on donor plasma, can provide insight into the variation of haemostatic parameters on individual donors prior to donation. The results obtained in our study indicate that in most instances no activation of FVIII occurs. during blood donation. If activation were to transpire, it would occur initially as a result of improper insertion of the needle into the vein, or when the blood is first drawn through the tubing into the pack (Carlebjork et al., 1983). Of further importance is the initial mixing of the blood and anticoagulant, and personnel should be instructed about optimal mixing procedures and its influence on the FVII present in the plasma. Care in stripping the donation line is also a critical part of the donation procedure, failure in doing so could cause small clots to form, an Indication that fibrinolysis is under way and once again affect the quality of FVIII yield.

⁶ Of the 7 positive results were identified on pre donation samples taken prior to ^{donating} the unit of blood. The reason for this could have been caused by inferior ^{phlebotomy} techniques, an unstable haemostatic condition present in the donor ^{which} had passed undiagnosed, or inadequate mixing with the anticoagulant after ^{the} sample had been drawn. As the same phlebotomist was used throughout the ^{study}, it would be fair to eliminate a reason as being inferior phlebotomy technique. ^{The} unstable haemostatic condition is unlikely given the good health of the blood

donors, however FDP levels can sometimes be elevated during menstruation Carlebjork *et al.*, 1986a). If this test was introduced as a routine test for all donors prior to donation, those donors presenting a positive test result due to a haemostatic condition, could be referred for further treatment and eliminated from donation. In this way, quality plasma for cryoprecipitate production could be sourced.

Factor VIII is stable in a narrow pH range around 7.0, thereafter it dissociates reversibly in the presence of high salt concentrations (International Forum, 1983). Pool in 1967 showed that there was no difference in FVIII recoveries in cryoprecipitate prepared from plasma with pH values between 6.0 and 8.0. The pH results in our study, using either plasma collected into CPD plus heparin, or into CPD alone, ranged between pH 7.25 and 8.10 and correlated well with the ^{outcome} reported by Pool (1967). The design samples whose plasma had heparin ^{added}, had a pH range of pH 7.9 to 8.10 whereas the plasma containing only CPD ^{nad} a range of pH 7.25 to 7.8. There has been no reported significance in the ^{relationship} between the pH of the pre donor plasma and the pH during the ^{prod}uction cycle (Shanberge *et al.*, 1972). The pre storage temperature (V6), had ^a significant influence on the pH determination.

The interaction of the pre storage temperature (V6), in particular that of 20°C, had ^{some} influence on the pH determination, when blood donors who had been ^{exercised} (V1) were used. This relates well to the FVIII analysis, in which the 20°C ^{pre-storage} temperature showed FVIII to be more stable at 20°C than at 4°C.

Similar findings were experienced by Vermeer *et al.* (1976b). During the production cycle, those variables showing significance, independently of each other, were the thawing temperature (V7), freezing rate (V8), freezing technique (V10) and the precipitation step (V14). Unfortunately the freezing rate, freezing technique and precipitation were confounded and their significance difficult to comment on. The thawing temperature experienced no carry over effects from Stage A phase, and was free from confounding by any of the other variables. The thawing temperature of between 4°C and 8°C can play an important role on the final outcome in the pH determination. The interaction of the freezing temperature (V9), and the manner in which the plasma was thawed (V13), was also found to be of relevance. The pH determination is relevant when a freezing temperature range, of between >-60°C or -35°C is used together with a thawing technique involving either circulating water or by moving the packs. No other variables or interactions were significant when determining the pH.

Trace amounts of plasma proteins are present in cryoprecipitate, but their concentrations vary (Smit Sibinga and Das, 1984). It was decided to examine the effect of the variables on the important plasma proteins (total protein and albumin), and others not mentioned in the literature to date. Of the plasma proteins, fibrinogen was analyzed separately and has already been discussed. It was decided not to assay fibronectin due to the cost factor and complications involved in the assay technique (Boughton and Simpson, 1985). The presence of fibronectin in cryoprecipitates has been well documented in the literature by Garelli *et al.* (1986), Horowitz *et al.* (1984) and Amrani *et al.* (1982). The levels of the immunoglobulin

determination (IgG, IgA, IgM, and IgE) and antithrombin-III are often undetectable. insignificant, and costly (Palmer et al., 1990). It was for these reasons that the mentioned assays were excluded. An oversight at the time of planning the study, was the exclusion of Fibrinopeptide A (FpA) assay, which would have correlated well with the FDP results, and detects early activation in the coagulation system Carlebjork et al., 1983). Similarities in the results of certain plasma proteins and electrolytes were found, and will therefore be discussed as one entity. Individual variables rather than interactions were more prominent between the variables, with the majority of variables having more influence during Stage A (prior to production), rather than in Stage B (during production cycle). Variables and interactions that were close to significance, were eliminated. Confounding in many of Stage B interactions were evident, making it difficult to comment on the relevance of the association. The reason being, these plasma proteins and electrolytes are only present in trace amounts and if definite significance was not evident, they would then have little bearing on the outcome of the entire Fractional Factorial Design.

During Stage A, the following variables and interactions played a role on the ^{cutcome} of the plasma proteins. Exercised blood donors (V1) affected the albumin ^{and} total protein results, while a bleed in under 8 minutes (V3) had an influence on ^{the} potassium results. Anticoagulant played a role in all the plasma proteins and ^{electrolytes}, with CPD influencing the magnesium, total protein, albumin and ^{sodium} data, as compared to heparin and calcium chloride influencing the ^{cotassium}, chloride and calcium data. This was evident by the higher assay results ^{being} obtained in those instances when heparin and calcium chloride were added

to the plasma, prior to processing. It would be acceptable to presume that the calcium results that were elevated, were caused whenever heparin and calcium chloride had been added to the plasma. Whole blood stored for 12 hours (V5) would have raised the potassium, which is known to increase on storage. Sodium levels rose when the whole blood was cooled to 4°C, prior to separation of the red cells and plasma. Magnesium, sodium and total protein analysis reflected the same cutcome when the blood donors were not requested to exercise, and blood groups other than Group A were used. The reason for this is not clear. Whole blood that has been stored at a temperature of 20°C and then had the red cells separated from the plasma within 6 hours, constructively influenced the magnesium, ALT and potassium results. A possible explanation for this occurrence could be that those plasma proteins are less unstable at a temperature of 20°C. A whole blood donation with a bleeding time of less than 8 minutes, processed within 6 hours, had a beneficial control over the ALT results.

in Stage B of the production phase, magnesium, total protein and sodium were not biased by any of the variables, although evident in total protein data, was a carry over effect from V5, the pre-process delay variable. V14, the precipitation technique demonstrated a connection with the results obtained from the carcium and ALT assays, but were confounded, and as a consequence, reservation about its significance is expressed. The same applies to the interaction V8 by V13 (freezing rate and thawing technique) for ALT and chloride, V12 by V13 (holding time and thawing technique) for albumin and V10 by V14 (freezing technique and precipitation) for potassium. It is suggested that these plasma proteins and

electrolytes are more sensitive to the freezing and thawing techniques than other plasma proteins and electrolytes.

Significant variables were the freezing technique (V10) for calcium and the thawing temperature (V7) for ALT. The reason for these variables showing significance, is uncertain and further studies on the plasma proteins would be required, if the answer is to be determined. The freezing technique (V10), in conjunction with the thawing technique (V13), play a critical part in the calcium and chloride determinations. Better insight into the plasma proteins and electrolytes and the effect of the many variables on them, has been gained by our study, however only play a limited role in the final yield of FVIII.
CHAPTER 6

CONCLUSIONS

Statistically designed experiments have been used in industrial experimentation for approximately the last 20 years, and more recently in the medical field. Sophisticated designs and methods of analysis have appeared since digital computers and their statistical programmes became available in the mid-1960s Hendrix, 1979). Statistical designs such as the one used in our study, are valuable ostruments, when countless variables need to be assessed at any one given time.

^{ariables} or combination of variables and their factors are significant to optimize the ^{creparation} of cryoprecipitate for FVIII.

ⁿ Stage A, of the production cycle ie. from the time of blood donation, to prior to ^{separation} of the red cells and plasma, variables V4 (anticcagulant), V5 (pre-^{cr}ocess delay prior to separation of red cells and plasma) and V6 (pre-process ^{storage} temperature), all play an important role in FVIII yield when examined as ^{ndependent} variables. Less importance was placed on variables V1 (donor exercise ^{evels}), V2 (donor blood group), and V3 (time taken to bleed the unit of blood) as nd significance was evident for these variables when evaluated as independent ^{rariables}. Donor blood group was significant when interacted with other variables.

CPD as the primary anticoagulant (V4) influenced the FVIII levels by producing superior yields when compared to other anticoagulants used. CPD influenced the pH. fibrinogen, vWF assay results, and majority of the plasma proteins levels, by showing, either no change in the outcome, or an improvement of FVIII yields. necarin appeared to be more suited to the electrolytes, however, this does not appear to be of any significant value, due to the small concentrations present in the plasma.

The pre-process time delay of less than 6 hours before separation was of vital monortance to the FVIII levels, due to the fact that a longer delay resulted in a decrease of FVIII activity. The shorter pre-process time seemed to produce better results in most of the plasma proteins, with the longer delay showing an increase of potassium levels.

^{can}able V6, that of the pre-storage temperature prior to processing, of 20°C is of ^{come} importance. Improved results in the FVIII, pH, fibrinogen, plasma protein and ^{s.actrolyte} assays were detected. Only sodium showed preference for the colder ^{temperature} of 4°C. Currently, in our present production cycle, not much attention ^s paid to variable V6. The temperature of the incoming blood, from mobile clinics, ^{ranges} between 4 - 30°C. This same variable (V6) showed an interaction with ^{aonor} exercise levels (V1) for vWF and pH determination.

³Yo other interactions for the FVIII statistical analysis of data results, were ³ gnificant,

Group A blood donors (V2) bled within 12 minutes (V3)

non exercised donors bled into packs containing CPD

a Stage B of the manufacturing process, variable V8 (freezing rate) was of no significance, with the freezing technique V10 (which was confounded in most instances), the holding time V12, the precipitation step V14 showing only intermittent significance, in relation to fibrinogen and pH. Variable V11, being that of centrifugation, demonstrated relevance only with vWF data.

Variables V7, that of the thawing temperature below 8°C and V9, freezing temperature >-60°C was the most significant in relation to the FVIII analysis. The fast freeze at >-60°C showed significance with the FVIII, fibrinogen and vWF results with increased yields, whereas the thawing temperature affected the pH and forinogen the most. The freezing temperature (V9), displayed interactions for the eH and fibrinogen analysis with the thawing technique (V13). Here either of the two factors of the variables could be relevant to either variable. A slow freezing rate results in a cryoprecipitate which is about twice the weight of a cryoprecipitate obtained by a fast freezing rate. A heavier cryoprecipitate contains FVIII with a ower specific activity.

^{t is} important that FVIII in the cryoprecipitate be in as natural a state as possible. ^{Activation} of FVIII by traces of thrombin will have adverse effects on the quality ^{of} the product. It has been shown that FVIII which has been activated by thrombin, ^{Oses} activity rapidly (Rick and Hoyer, 1978). The amount of FpA in a sample is

proportional to the level of thrombin formation and an indication of the extent of activation of FVIII. FpA is influenced by the method of blood collection, and its assay content is an indication of FVIII activation. Plasma with a low FpA content, is processed more easily and the product remains stable (Pflugshaupt and Kurt, 1983). Care in stripping the donation line is also an important part of the donation crocedure, in ensuring low plasma FpA levels ((Prowse *et al.*, 1984). FpA content also indicates the importance of blood flow through the collecting tube devoid of anticoagulants (Skjonsberg *et al.*, 1986). Fibrinopeptide A determination is a "aluable test, which is able to give indications of the status of the blood donation prior to the commencement of processing and should therefore be incorporated as cart of the routine in bleeding procedure.

The positive results of the FDP D-dimer latex assay in this study, were more likely to be that of a haemostatic condition in the donor possibly caused by menstruation Carlebjork *et al.*, 1986a), than poor phlebotomy techniques. Rather than pursue to s assay in future studies, we would recommend all donations be tested by FpA determination which is a far more practical and sensitive assay method. Detection of a positive result should exclude the unit of donated blood from being batched for processing into cryoprecipitate.

To summarize, the findings of our study indicate that there are 17 simple steps in The FVIII production process, to which attention to detail should be paid to optimize FVIII yields :

the venipuncture should be a first time clean entry into a vein

- * strenuous exercise is not required
- * Group A blood donors should be used for cryoprecipitate production
- * the primary anticoagulant should be CPD
- * blood should be mixed with anticoagulant during phlebotomy
- cryoprecipitate must be prepared from plasma within 6 hours of collection
- * whole blood temperature must be maintained at 20 24°C prior to processing
- * FpA assay should be performed on all donations prior to processing
- * separation of red cells / plasma should be by means of a rapid
 centrifugation at 4733 X g
- * plasma must be frozen using a rapid freeze technique with a temperature of greater than -60°C
- * plasma bags should be placed in a polyethylene over-wrap, immersed
 in a bath of 95% ethanol and dry ice as a recommendation for
 freezing
- * plasma must be of constant volume
- * plasma must be compressed between metal plates to ensure uniform density
- * thawing of the frozen plasma should be below 8°C, in a water environment in which agitation occurs either by movement of the water or plasma packs
- * precipitation must be carried out by means of centrifugation
- * after drainage cryoprecipitate should be refrozen rapidly with dry ice

cryoprecipitate should be stored at below -30°C

Of the 17 steps that have been highlighted above, it is important to communicate that 12 are already being applied during the production process at WPBTS.

Eurther attention must be given to the following areas (in addition to the 12 already used), in order to achieve the optimal quality of cryoprecipitate, containing high vields of FVIII:

- * only bleeding of Group A donors;
- ensuring that the blood reaches a temperature of 20°C prior to separation;
- * performing a FpA assay prior to processing;
- * fast freezing rate of >-60°C;
- * constant starting plasma volume.

^{of the} above five parameters, those most difficult to implement in a large scale ^{Cutine} production laboratory, would be:

- * only bleeding Group A donors for cryoprecipitate production, which would require a much larger donor base, jut plasmapheresis could be an option and would require further investigation of this route;
- monitoring of the whole blood temperature at 20°C;
- introduction of routine FpA testing, as it would increase the cost of production.

However, with modifications to certain procedures, the above could be achieved.

These findings further indicate that fibrinogen is present in therapeutically useful quantities in the cryoprecipitate. Unfortunately fibronectin was not included in the study, but is a recommendation for future work on the production of cryoprecipitate. The plasma proteins and electrolyte assays involve considerable time and cost for relatively inconsequential information, and we advocate to exclude them hereafter in further studies relating to cryoprecipitate.

As additional suggestion, what is required in the future, is that the Fractional Factorial design should be selected so that carry-over effects of the pre-production factors are not confounded with the production factors. This would include altering the design of the two variables that were identical, to avoid future confounding of the factors. When all the corrections have been made, we would repeat the study, factors the plasma protein and electrolyte assays, but including the fibronectin assay. The FDP D-dimer assay would be exchanged for the FpA assay. assay.

¹ conclusion, we wish to report that we were able to achieve our objective, which ^{1/as} to identify those variables and interactions of factors which optimize the ^{1/o}duction of Factor VIII in cryoprecipitate. Our recommendations are feasible for ^{arge} scale cryoprecipitate production. Furthermore, we have gained additional ^{1/o}.vledge of those assays which are relevant when determining FVIII yields and ^{1/o}adility.

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Appendix 1 **BLOOD DONOR DESIGN PROTOCOL**

Design Number		
Date Bled		

A. DONOR INFORMATION

Donor Number	
Date Last Bled	
Sex	
Age	
Blood Pressure	
Pulse	
Medical History	
Iron Level	
Pack Weight (g)	
Plasma Weight (g)	

B. DETAILS OF SPECIFIC DESIGN TYPE

Fariable NO	Variable Category	High (+)/ Low (-)	Explanation & Comments
V1	Donor Exercise		
12	Blood Group		
73	Anticoagulant		
V4	Bleeding Time		
78	Pre-Process Delay		
/6	Pre-Process Storage		
17	Thawing Temperature		
18	Freezing Rate		
13	Freezing Temperature		
710	Freezing Technique		
/11	Centrifugation		
/12	Holding Time		
/13	Thawing Technique		
/14	Precipitation		

Samples Taken (X 2): Samples Taken (X 2) :

YES / NO YES / NO

* índicates an outlier result

Factor VIII (Normal Range 0.5 - 2.00 U/ml; Cryo Normal Range +/- 10.00 U/ml)

		PRE				POST				FINAL		
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	0.88	0.66	1.09	1.36	0.38	0,86	1.45	1.80	2.03	8.44	4.44	12.63
2	0.60	0.83	0.83	0.84	0.36	0.87	1.06	0,70	8.07	16.81	13.03	9.20
3	0,41	0.81	1.02	0.87	0.77	1.11	1.10	1.34	2,98	12.46	3,15	15.02
4	0.58	0.44	1.10	1.05	0.78	0.51	0.76	1.00	12.13	12.15	7.21	29.37
5	0.79	1.23	1.05	0.74	0.66	1,39	0.80	0.61	14,45	24.00	6,42	21.86
6	0.80	1.15	0.54	1.31	1.08	1.71	0.74	1.33	28.33	29.86	3,88	28.00
7	0.50	1.18	1.11	0.86	0.84	1.42	0.77	1.07	14.55	25.43	14.36	39.14
8	0,93	0.37	1,32	1.28	1.24	0,65	1.33	1.34	21.92	1.31	4.76	3.55
9	0.73	0.74	0.64	0.51	0.56	0.37	0.36	0.57	7.84	4.98	5.95	10.23
10	1.04	0.53	0.53	0.64	0.91	0,64	0.49	0.71	1.43	0.59	0.57	2.00
11	0.47	0.66	0,98	0,84	0.42	0,65	0.92	0,80	4.37	7.21	18.66	8.77
12	0.30	0.71	0.78	1.08	0.47	0.52	0.58	1.02	6,90	5.70	8.06	9.81
13	0.64	0.34	0.82	0.47	0.44	0.19	0.51	0.42	7.25	3.21	12.14	2.85
14	1.15	0.62	0.90	0.55	1.25	0.69	0.77	1.00	41.38	9.27	7.01	18.93
15	0.46	0.95	0.74	0.72	0.59	0.87	0.58	0.81	12.04	8.82	9.43	4.71
16	0.96	0.90	0.65	0.77	0.42	0.58	0.48	0.46	5,80	8.21	11.49	5.30
17	0.71	0.85	0.78	0.54	0.83	0.92	0.94	0.76	9.47	9.73	18.91	8.04
18	0.85	0.55	0.55	0.44	0.40	0.60	0.77	0.58	4.27	10.80	14.70	3.34
19	0.82	0.66	0.46	0.57	0.75	0.72	0.41	0.57	12.18	11.48	3,36	35.50
20	0.73	0.66	0.54	1.10	1.00	1.25	0.38	1.15	12.22	19.73	7.31	27.87
21	0,83	0.49	0.59	1.18	0.76	0.33	0.27	0.61	7.72	4.39	4.21	7.49
22	0.71	0.58	1.24	0.98	0.64	0.90	0.88	0.87	8,58	9.04	15,33	10.55
23	0.62	0.68	0.49	1.12	0,49	0.82	0.77	1.84	8,58	0.05	4.57	12.24
24	0.62	0.79	0.78	0.82	1.00	0.87	0.65	0.79	14,16	8.11	51.09	25.35
25	0.30	0.32	1.05	0.53	0.55	0.48	1.09	0.76	10.61	10.77	23.62	10.60
26	0,69	0.73	1.08	0.88	0.78	0.82	1.12	0.80	10.17	25.44	8.88	4.21
27	0.49	1.15	0,57	0.90	0.09	1,33	0.60	1.12	1.74	4.88	1.07	1.30
28	0.60	0.52	0.66	0.71	0.79	1,46	1.13	1.07	11.46	12.59	15.76	17.23
29	0.62	0.74	0.54	0.31	0.49	0.91	0.67	0.98	13.03	24.76	6.22	7.61
30	0.66	0.83	0.81	0.68	0.71	0,98	1.21	0.74	16.83	13.72	27.59	13.33
31	1.06	0.70	1.36	1.11	1.15	1.17	1.22	1.04	15.33	14.64	21.51	39.21
32	0.70	0.87	0.97	0.97	1.16	1.26	2.02	1.35	9.34	7.43	15.03	21.35

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PRE	
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POST

FINAL

NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	1.80	3.26	2.00	2.40	1.50	3.00	2.24	2.58	2.00	9.60	2.58	4.60
2	2 40	2.58	1.55	1.90	1.78	2.49	1.55	1.72	10.32	13.80	5.20	8.20
3	1 72	3.26	2.75	3.00	2.00	2.58	2.49	3.44	10.32	9.60	8,00	7.20
4	2.58	2.00	2.58	2.40	2.58	1.70	2.58	2.49	13.76	10.00	13.00	13.00
5	3.00	2.49	3.60	2.58	2.40	2.06	3.60	2.49	14.40	9.30	19.60	18.00
6	2.40	3.26	2,24	2.58	2.32	3.26	1.78	2.24	17.20	10.30	6.88	10.00
7	2.40	3.00	1,80	2.32	3.44	2.49	1.72	1.90	13.76	6.00	14.40	26.10
8	2.32	2.75	2.58	2.58	2.32	2.58	2.40	2.24	16.00	4.10	3.00	2.58
9	3.26	2.30	2.58	2.00	2.49	2.00	2.58	2.40	17.20	8.60	13.80	19.20
10	3.26	4.00	2.58	2.75	2.49	3.00	2.58	3.26	3.00	3.60	3.44	4.10
11	2.40	2.32	2.40	2.24	2.49	2.00	2.06	1.80	6.88	8.60	12.00	9.30
12	1.46	2.24	2.49	2.75	1.60	2.32	2.40	2.75	7.20	10.30	9.00	14.40
13	1.80	2.32	2.06	1.72	2.24	2.49	1.80	2.58	13.04	19.60	10.30	13.00
14	1.80	1.90	2.06	2.06	1.72	1.80	2.06	1.80	11.00	7.20	9.30	9.00
15	1.90	2.06	2.58	2.24	1,78	1.80	2.75	2.00	6.88	8.60	16.00	2.40
16	2,58	1.80	2.40	3.44	2.24	1.72	2.32	2.00	10.30	12.00	13.00	9.30
17	2.24	2.58	2.06	2.58	1.70	2.40	2.32	2.32	9.60	8.00	9.60	14,40
18	2.75	2.06	1.38	3.26	3.00	2.06	1.55	3.44	8.00	9.60	8.00	13.00
19	4.00	4.30	2.00	2.49	3.44	3.26	2,32	1.80	18.00	19.60	9.00	11.00
20	2.49	2.58	1.80	2.75	2.40	2.58	1.80	2.06	19.60	19.60	9.00	17.20
21	1.50	2.00	1.90	2.40	1.70	2.00	1.80	2.24	6.88	12.00	9.60	13.00
22	2.75	3.44	3.00	2.58	3.00	3.44	3.00	3.26	18.00	13.00	20.40	13.00
23	2.32	2,24	2.40	3.26	2.24	2.32	2.49	2.75	13.04	8,60	12.00	8,60
24	2.40	2.00	1.80	3.26	2.49	1.70	1.78	2.24	6.00	6.88	11.00	13.00
25	2.58	2.00	2.75	3.44	2.49	2.00	2.75	2.75	13.04	13.80	17,20	16.00
26	2 75	2 75	2.58	2.58	3.44	2.40	2.49	2.58	6.88	19.60	9.60	6.00
27	1 90	2 40	1.78	2.58	2.24	2.49	2.00	2.49	2.49	3.00	2.24	4.30
20	2 22	1 46	1.90	1.72	2,40	1.80	2.24	1.40	18.00	8.00	9.00	5.16
20	A 00	2.58	3.26	4.00	3.00	2.40	2.75	3.00	18.00	19.60	13.80	18.00
20	4.00 1.80	2.00	2 40	2.00	2.00	2.40	3.00	2.06	11.00	18.00	13.80	6.00
30	2.06	2.24	4 30	2.49	2.32	2.58	3.00	2.40	14.40	16.00	13.80	16.00
32	2.00	3.00	1.46	0 95	3.26	2.32	2.24	1.12	5.50	8.00	5.20	4.00

von Willebrand Factor (Normal Range 100%)

		PRE				POST				FINAL		
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	110.0	120.5	110.0	190.0	40.0	160.0	170.0	85.0	5.0	65.0	20.0	95.0
2	85.0	110.5	75.0	30.0	22.5	180.5	120.0	90.5	42.5	90.0	60.5	65.0
3	70.5	80.5	95.0	130.0	40.0	140.0	150.0	85.0	75.0	55.0	42,5	47.5
4	110.0	75.0	80.5	110.0	80.0	95.0	190.0	130.5	85.0	55.0	100.0	150.0
5	110.0	110.0	90.0	60.5	85.0	180.0	95.0	50.5	120.0	100.0	55.5	95.0
6	120.0	170.0	120.0	120,0	40.0	320.0	120.0	160.0	120.5	120.0	70.0	170.0
7	90.0	190.0	120.5	90.5	50.0	210.0	100.5	95.0	45.0	120.5	150.0	200.0
8	180.0	95.0	280.0	180.0	110.0	100.5	180.0	140.0	140.0	30.0	32.5	20.0
9	170.0	120.5	80.0	40.0	75.5	110.0	47.5	45.0	80.5	60.0	30.0	85.0
10	95.5	60.0	40.0	60.5	15.0	80.5	80.0	90.5	11.3	10.0	9,4	8.1
11	60.0	75.0	160.0	60.5	75.5	90.0	110	42.5	27.5	40.0	90.0	47.5
12	85.0	95.5	75.0	170.0	37.5	90.0	95.5	90.0	60.0	80.0	40.0	95.0
13	75,5	75.0	170.0	55.0	42.5	120.5	110.0	47.5	50.0	18.8	70.0	32.5
14	130.0	60.5	90.0	65.0	85.0	42.5	130.0	85.0	170.5	70.0	65.0	95.0
15	60.0	90.0	90.0	100.5	25.0	160.5	95.0	70.0	27.5	90.0	70.0	25.0
16	110.0	100.0	60.0	55.0	42.5	180.0	80.0	60.0	45.5	90.0	50.0	55.5
17	90.5	95.5	75.5	60.0	110.0	190.0	100.5	75.0	75.5	85.5	80.0	80.0
18	85.0	47.5	85.0	85.0	65.0	100.0	85.0	80.5	37.5	55.0	75.5	55.0
19	100.0	160.5	100.5	50.5	50.5	95.0	55.5	80.5	70.5	120.5	40.0	85.0
20	100.0	95.5	60.5	110.0	70.0	190.5	50.5	110.0	110.0	160.5	40.0	170.0
21	120.0	120.0	40.5	120.0	90.0	42.5	42.5	55.0	60.0	30.0	22.5	90.0
22	65.5	140.0	120.5	70.0	42.5	160.5	180.0	120.5	85.0	47.5	140.0	85.0
23	120.0	170.0	70.5	130.0	35.0	170.0	95.5	150.0	60.0	37.5	70.0	100.5
24	120.0	45.0	65.0	70.5	75.0	120.5	80.0	75.0	85.0	140.0	85.0	100.0
25	90.0	50.0	180.5	90.5	55.0	35.0	200.0	110.0	47.5	42.5	170.0	110.0
26	140.5	95.0	90.0	170,0	50.0	9 0.0	160.0	190.0	50.0	85.5	47.5	45.0
27	60.0	220.0	47.5	90.0	22.5	190.5	60.0	100.0	7.5	15.0	12.5	12.5
28	60.0	160.0	75.5	70.0	27.5	190.0	130.0	60.0	60.5	170.5	100.0	75.5
29	80.0	60.0	55.0	85.0	42.5	110.5	100.0	70.0	65.0	90.0	90.0	50.0
30	140.0	95.0	80.0	70.5	30.0	160.5	160.5	47.5	100.0	140.0	170.0	42.5
31	160.0	260.0	150.0	70.5	85.0	190.0	120.5	80.0	120.5	190.5	120.0	80.0
32	160.5	120.5	170.5	150.0	90.0	160.0	90.0	160.0	42.5	110.0	65.0	95.5

Fibrin Degradation Products (Normal Range "-")

PRE					POST			FINAL				
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	-	-	-	-		-	-	•	-	-	-	-
2	•	-	-		-	•	-	•	-	-	-	-
3	-		-	-	-		-	-	-	-	-	-
4		-	-	-			-	-	-	-	-	-
5		-	-	-		-	-	-	-	-	-	-
6	-		•	-	-	+	-	-	-	-	•	-
7			•	-	-	•	-	-	•	•	-	
8		-	-	-	•	-	-	-	-	-	-	-
9		•	-	-	-	-	-	-	-	-	•	-
10	+	-	•	•	•	-	-	-	•	-	-	-
11	+	-	+	-	-	-	+	•	-	•	-	-
12	•	•	-	*	•	•	•	-	-	-	•	•
13	-		-	-	-	•	•	-	-	-	•	۰
14	-	-	•	•	-		•	-	•	-	•	•
15	-	-	-	-		-	-	-	-	-	•	-
16	•	-	*	-	-	•	•	-	-	-	•	-
17	-	-	•	-	-	-	•	-	•	-	•	•
18			•	-	-	•	•	-	+	-	-	+
19		-	-	•	•	•	•	-	•	•	•	•
20		-	•	+	-		•	•	-	-	•	•
21	-	-	•	+	*	•	-	•	-	-	•	•
22	-	•	-	-	-	-	•	-	-	•	•	-
23	-	-	-	-	-	•	-	-		•	•	+
24		-	-	-	-	-	•	-	-	-	•	-
25	-			-	•	•	-	•	-	-	•	•
26	+	-	•	-	-	•	•	-	-	•	•	-
27	-	-		-	-	-	•	-	-	-	•	-
28				-	-	-	-	-	-	-	•	•
29	•		-	-	-	•	•	•	-	•	•	-
30	-		-	-	-	-	-	•	-	-	•	-
31	•			-		-	-	-	+	-	•	•
32	-		-	-	-	-	-	•	-	-	٠	•
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pH (Normal Range +/- 7.43)

		PRE				POST				FINAL		
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	7 88	7.73	7:72	7,57	8.10	7.91	7.95	7.98	7.83	7.66	7.80	7.76
2	7.80	7.84	7.82	7.72	7.77	7.94	7.53	7.44	7.83	7.75	7.68	7.61
3	7.33	7.92	7.91	7.58	7.48	7.75	7.92	7.93	7.90	7.75	7.82	7.71
4	7.25	7.66	7.74	7.28	7.80	7.66	7.85	7.76	7.81	7.75	7.89	7.74
5	7.66	7.56	7.87	7.84	7.83	7.94	7.98	7.82	7.72	7.87	7.64	7.62
6	7.70	7.86	7.93	7.85	7.97	7.94	7.88	7.87	7.65	7.85	7.71	7.64
7	7.74	7.88	7.71	7.41	7.76	7.76	7.73	7.83	7.71	7.70	7.82	7.71
8	7.56	7.83	7.64	7.73	7.91	7.73	7.73	7.72	7.75	7.57	7.75	7.66
9	7.77	7.56	7.73	7.70	7.89	7.92	7.70	7.87	7.65	7.76	7,68	7.76
10	7.56	7.52	7.62	7.32	7.75	7.74	7.55	7.52	7.57	7.67	7.52	7.59
11	7.51	7.54	7.77	7.62	7.98	7.74	7.94	7.97	7.77	7.65	7.75	7.77
12	7.56	7.76	7.91	7.79	7.86	8.02	7.62	7.82	7.63	1.11	7.67	7.00
13	7.90	7.97	8.06	7.62	7.85	7.88	7.72	7.87	7.76	7.88	7.77	7.75
14	7.33	7.69	7.88	7.56	7.78	7.80	7.60	7.76	7.84	7.77	7.76	7.00
15	7.95	7.40	7.53	7.35	7.77	7.49	7.63	7.52	7.51	7.81	7.58	7.55
16	7.54	7.96	7.93	7.76	8,12	8.04	7.83	8.06	7.61	7.65	7.80	7.30
17	7.63	7.88	7.77	7.65	7.95	8.04	7.80	7,94	7.76	7,74	7,70	7.05
18	7.87	7.47	7.60	7.56	7,80	8.05	7.73	7.68	7.57	7.75	7.58	7.00
19	7.59	7,63	7.65	7.41	7.73	7.79	7.49	7.55	7.55	7.68	7.70	7.00
20	7.45	7.65	7.64	7.67	7.70	7.71	7.57	7.62	7.66	7.48	7.75	7.03
21	7.50	7,38	7.86	7.40	7,91	8.11	8.12	7.85	7.62	7.72	7.74	7.70
22	7.63	7.55	7.86	7.46	7.58	7.93	7.54	7.75	7.65	7.69	7.71	7.04
23	7.33	7.85	7.82	7.39	7.89	7.90	7.87	7.97	7.55	7.72	7./1	7.09
24	7.67	7.54	7.87	7.70	8.05	8.11	7.86	7.75	7.62	7.80	7.80	7.05
25	7.41	7 59	7.40	7.37	7.95	7.93	7.92	7.84	7.62	7.70	7.07	7.02
26	7.84	7.62	7.72	7.67	7.70	7.85	7.91	7.84	7.68	7.71	7.70	7.70
27	7.51	7.52	7.87	7.60	7.61	7.82	7.93	7.81	7.63	7.59	7.73	7.05
28	7.65	7.50	7.40	7.31	7.74	7.85	7.70	7.71	2.61	7.68	7,60	7.71
29	7.24	7.46	7.86	7.57	7.70	7.85	7.71	7.81	7.72	7.75	7.74	7.74
30	7.54	7.40	7.32	7.24	7.84	7.57	7.84	7.68	1.12	7.04	7.07	7.00
31	7.74	7.78	7.89	7.72	7.75	7.83	7.77	7.69	7.67	7.70	7.09	7.70
32	7.25	7.71	7.74	7.77	7.52	7.58	7.75	7.61	7.49	1.52	7.50	7.50
Magnesium (Normal Range 0.7 - 1.1 mmol/l)

				ivi	lagnesium (i	vormai r	hange u.		moni		+ indicate	es outlier
		PRE				POST				FINAL		
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	0.83	0.74	0,60	0.92	0.69	0.66	0.66	0.73	0.57	0.55	0.63	0.73
2	0.88	0.94	0.99	0.91	0.67	0.71	0.65	0.71	0.65	0,76	0.70	0,70
ŝ	0.87	0.63	0.89	0.92	0.60	0.66	0.66	0.72	0.83	0.64	0.63	0.71
4	1.03	0.51	0.67	0.67	0.63	0.67	0.65	0.71	0.58	0.58	0.67	0.73
5	0.89	0.64	0.91	0.60	0.70	0.61	0.70	0.76	0.67	0.47	0.67	0.74
6	0.83	0.78	0.85	0.56	0.64	0.62	0.71	0.73	0.63	0.41	0.68	0.70
7	0.84	0.74	0.68	1.00	0.67	0.67	0.63	0.72	0.41	0.44	0.68	0.69
Ŕ	0.27	0.71	0.69	0.59	0.64	0.75	0.60	0.64	0.68	0.64	0.49	0.60
ğ	0.86	0.51	0.83	0.88	0.67	0.66	0.68	0.65	0.59	0.57	0.62	0.64
10	0.92	0.73	1.11	0.85	0.69	0.81	0.77	0.80	0.82	0.71	0.58	0.96
11	0.58	0.72	0.90	0.81	0.58	0.63	0.67	0.67	0.65	0.48	0.58	0.63
12	0.91	0.59	0.86	0.55	0.72	0.67	0.66	0.76	0.58	0.58	0.62	0.77
13	0.88	0.70	0.85	1.05	0.67	0.61	0.65	0.76	0.66	0.57	0.52	0.78
14	0.50	0.69	0.89	0.62	0.71	0.72	0.69	0.71	0.67	0.55	0.57	0,74
16	0.97	0.82	1.00	0.68	0.81	0.75	0.71	0.70	0.74	0.61	0.60	0.22 *
16	0.90	0.87	0.89	0.91	0.61	0.72	0.65	0.72	0.47	0.63	0.65	0.67
17	0.87	0.72	0.52	0.89	0.60	0.71	0.58	0.71	0.56	0.61	0.54	0.67
18	0.89	0.82	0.87	1.00	0.76	0.80	0.63	0.78	0.66	0.68	0.35	0.85
19	0.91	0.79	0.83	0.76	0.68	0.71	0.69	0.72	0.66	0.60	0.71	0.55
20	0.88	0.76	0.83	0.55	0.67	0.74	0.64	0.67	0.70	0.39 *	0.58	0.65
21	0.98	0.87	0.59	0.78	0.70	0.74	0.68	0.68	0.64	0.58	0.57	0.08
22	0.94	0.94	0.86	0.72	0.76	0.90	0.63	0.70	0.72	0.76	0.68	0.72
23	0.85	0.76	0.90	0.88	0.51	0.63	0.71	0.68	0.51	0.71	0.73	0.67
24	0.90	0.87	0,72	0.75	0.77	0.75	0.66	0.74	0.67	0.62	0.64	0.00
25	0.95	0.58	0.66	0.76	0.66	0.65	0.64	0.63	0.56	0.53	0.64	0.55
26	0.58	0.61	0.80	0.82	0.56	0.77	0.53	0.74	0.54	0.62	0.55	0.81
27	0.86	0.83	0.95	0.87	0.61	0.71	0.73	0.72	0.50	0.51	0.33 *	0.82
28	0.80	0.86	0.97	0.80	0.64	0.63	0.67	0.63	0.55	0.60	0.59	0.70
29	0.98	0.83	0.50	0.91	0.76	0.64	0.69	0.67	0.58	0.55	0.65	0.65
30	0.93	0.72	0.97	0.69	0.64	0.68	0.70	0.73	0.65	0.56	0.69	0.76
31	0.73	0.62	0.56	0.71	0.70	0.75	0.67	0.70	0.59	0.66	0.68	0.68
32	0.83	0.93	0.59	0.66	0.63	0.60	0.65	0.71	0.61	0.63	0.92	0,43

Total Protein (Normal Range 64 - 88 g/l)

PRE			POST				FINAL					
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	73.0	55.0	50.0	61.0	58.0	57,0	59.0	57.0	58.0	55.0	54.0	54.0
2	710	74.0	76.0	72.0	57.0	58.0	62.0	56.0	55.0	70.0	66.0	59.0
3	71.0	48.0	70.0	71.0	61.0	58.0	60.0	60.0	86.0	46.0	65.0	57.0
4	76.0	31.0	57.0	55.0	60.0	55.0	58.0	58.0	59.0	52.0	62.0	60.0
5	66.0	47.0	73.0	41.0	62.0	58.0	65.0	63.0	65.0	42.0	74.0	62.0
6	71.0	59.0	73.0	46.0	59.0	58.0	57.0	57.0	68.0	33.0	55.0	57.0
7	74.0	53.0	50.0	70.0	58.0	62.0	53.0	59.0	37.0	50.0	58.0	50.0
8	56.0	69.0	54.0	45.0	54.0	54.0	54.0	58.0	55.0	50.0	51.0	50.0
9	63.0	30.0	65.0	79.0	49.0	52.0	54.0	66.0	50.0	48.0	51.0	61.0
10	64.0	56.0	70.0	74.0	54.0	62.0	55.0	70.0	67.0	57.0	42.0	74.0
11	46.0	60.0	65.0	70.0	53.0	60.0	56.0	53.0	54.0	54.0	53.0	62.U 62.0
12	65.0	38.0	72.0	51.0	56.0	60.0	59.0	62.0	46.0	55.0	59.0	02.U EE A
13	68.0	47.0	73.0	74.0	69.0	57.0	56.0	57.0	59.0	54.0	45.0	720
14	42.0	54.0	73.0	53.0	64.0	58.0	55.0	60.0	69.0	49.0	52.0	a n +
15	74.0	75.0	76.0	55.0	61.0	55.0	66.0	59.0	64.0	51.0	00.0 EE 0	5.0
16	70.0	69.0	73.0	71.0	53.0	57.0	60.0	57.0	55.0	52.0	55.0	57.0
17	76.0	51.0	52.0	66.0	56.0	50.0	66.0	54.0	53.0	52.0	26.0	60.0
18	70.0	70.0	68.0	71.0	58.0	63.0	53.0	60.0	67.0	57.0	570	44 0
19	70.0	68.0	74.0	56.0	59.0	60.0	61.0	61.0	03.U	30.0	57.0	68.0
20	71.0	66.0	72.0	42.0	58.0	64.0	57.0	64.0	05.U	44.U 50.0	10 0	62.0
21	66.0	69.0	47.0	73.0	53.0	57.0	51.0	61.0	52.U	50.0 66.0	65.0	68.0
22	68.0	77.0	71.0	65.0	55.0	59.0	56.0	60.0	58.0	50.0 66 0	61.0	60.0
23	70.0	71.0	70.0	74.0	55.0	61.0	55.0	0.10	58.0	60.0 64 O	61.0	47.0
24	73.0	61.0	50.0	53.0	62.0	59.0	57.0	59.0	50.0	34.0	01.0 69.0	58.0
25	79.0	39.0	51.0	63.0	59.0	58.0	59.0	58.0	54.0	47.0 E4.0	64.0	57.0
26	46.0	50.0	73.0	70.0	55.0	57.0	58.0	51.0	50.0	54.0 41 D	20.0	71 0
27	69.0	72.0	74.0	74.0	52.0	58.0	55.0	60.0 F 2 0	48.0	56 O	51 O	58.0
28	70.0	75.0	69.0	62.0	60 0	57.0	54.0	53.U 50.0	51.0	50.00 68.0	56 0	60.0
29	69.0	69.0	38.0	75.0	57.0	55.0	57.0	58.U	59.0	70.0	50.0 56.0	57.0
30	70.0	63.0	71.0	59.0	60.0	63.0	55.0	00.0	50.0	56.0	50.0 58.0	51.0
31	7 0.0	44.0	40.0	66.0	63.0	59.0	56.0	57.0	59.0 60.0	50.0 65.0	76.0	39.0
32	67.0	74.0	49.0	51.0	60.0	65.0	54.0	50.0	00.0	00.0	,0.0	00.0

Albumin (Normal Range 30 - 55 g/l)

PRE			POST					FINAL				
NO	RUN 1	RUN 2	RUN 3	RUN 4	BUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
	46.0	25 A	33.0	40.0	37.0	32.0	36.0	33.0	39.0	32.0	36.0	33.0
2	40.0	43.0	50.0	45.0	33.0	32.0	38.0	35.0	31.0	38.0	40.0	35.0
4	43.0	20.0	41.0	45.0	37.0	34.0	35.0	37.0	49.0	28.0	36.0	35.0
3	42.0	19.0	36.0	32.0	36.0	34.0	38.0	32.0	3 5.0	3 3.0	37.0	32.0
-44 E	28.0	28.0	43.0	28.0	33.0	34.0	36.0	39.0	34.0	24.0	37.0	36.0
6	12 0	37.0	46.0	31.0	33.0	33.0	34.0	34.0	31.0	18.0 *	33.0	32.0
7	46.0	34.0	28.0	41.0	37.0	33.0	36.0	34.0	21.0	27.0	36.0	31.0
6	36.0	37.0	33.0	24.0	32.0	33.0	32.0	28.0	33.0	33.0	30.0	27.0
o G	42.0	21.0	37.0	43.0	32.0	30.0	30.0	34.0	31.0	29.0	29.0	32.0
10	41 0	36.0	45.0	48.0	31.0	38.0	34.0	35.0	40.0	36.0	24.0	42.0
11	29.0	35.0	40.0	43.0	30.0	33.0	32.0	31.0	32.0	31.0	30.0	31.0
12	39.0	27.0	41.0	29.0	34.0	36.0	38.0	36.0	27.0	34.0	38.0	35.0
17	44.0	31.0	45.0	47.0	36.0	35.0	36.0	38.0	36.0	33.0	29.0	34.0
14	27.0	32.0	44.0	33.0	38.0	35.0	35.0	35.0	39.0	30.0	33.0	43.0
15	46.0	48.0	46.0	33.0	37.0	34.0	36.0	35.0	37.0	30.0	30.0	0.U "
16	44.0	44.0	47.0	46.0	34.0	34.0	36.0	36.0	33.0	32.0	33.0	30.0
17	49.0	34.0	33.0	39.0	34.0	32.0	33.0	32.0	33.0	33.0	33.0	33.0
18	39.0	44.0	44.0	46.0	35.0	35.0	32.0	35.0	34.0	35.0	15.0 *	37.0
19	45.0	42.0	46.0	36.0	38.0	35.0	35.0	35.0	36.0	33.0	33.0	20.0
20	42.0	41.0	45.0	27.0	32.0	34.0	35.0	34.0	35.0	23.0	30.0	35.0
21	43.0	42.0	30.0	45.0	34.0	33.0	32.0	36.0	33.0	30.0	31.0	34.0
22	45.0	41.0	37.0	39.0	35.0	33.0	27.0	33.0	34.0	34.0	32.0	37.0
23	41.0	44.0	46.0	44.0	31.0	38.0	35.0	33.0	34.0	40.0	38.0	31.0
24	47.0	36.0	37.0	30.0	35.0	37.0	35.0	35.0	32.0	34.0	30.0	29.0
25	49.0	24.0	34.0	35.0	35.0	34.0	32.0	33.0	33.0	29.0	32.0	32.0
26	28.0	29.0	45.0	40.0	34.0	31.0	33.0	33.0	29.0	30.0	30.0	37.0
27	47.0	44.0	44.0	46.0	33.0	36.0	34.0	37.0	27.0	26.0	18.0	43.0
28	46.0	43.0	44 0	37.0	37.0	35.0	35.0	34.0	33.0	33.0	32.0	33.0
29	44.0	43.0	24.0	45.0	33.0	35.0	35.0	34.0	34.0	34.0	33.0	32.U
30	43.0	36.0	43.0	34.0	34.0	36.0	33.0	33.0	30.0	37.0	33.0	30.0
31	44.0	25.0	26.0	41.0	37.0	33.0	32.0	36.0	31.0	30.0	32.0	22.0
32	45.0	45.0	30.0	33.0	35.0	38.0	31.0	35.0	36.0	38.0	44.V	20.0

Calcium (Normal Range 2.3 - 2.7 mmol/l)

PRE			POST					FINAL				
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
	2 4 0	1.80	1 73	2 26	2.05	1.40	2.12	1.42	2,16	1.43	2.10	1.48
2	2,43	2 3 2	2 43	2.30	2.06	1.92	2.16	1.42	2.00	2.13	2.24	1.50
2	2.00	1 72	2 29	2.44	1.42	1.33	1.44	1.46	1.86	1.31	1.53	1.59
2	2.47	1 18	1.85	1.93	1,44	1.32	1.45	1.40	1.44	1.35	1.49	1.47
5	2.47	1 51	2.45	1.47	1.36	1.32	1.51	1.42	1.39	1.19	1.52	1.48
0 6	2.32	1.96	2.30	1.59	1.37	1.38	1.35	1.34	1.44	1.08	1.29	1.45
7	2,02	1 92	1 52	2 20	1.37	1.38	1.35	1.34	0.93 *	1.21	1.42	1.39
<u> </u>	105	2 09	1.85	1.52	1.27	1.32	1.34	1.34	1.31	1.32	1.29	1.37
a	2 27	1 10	2.19	2.52	1.41	1.33	2.00	1.43	1.41	1.30	1.99	1.47
10	2.27	1.86	2.39	2.41	1.31	1,48	1.36	1.40	1.62	1.46	1.03	1.71
10	1 80	1.93	2.29	2.42	1.37	1.38	1.87	1.44	1.46	1.36	1.80	1.52
12	2 2 1	1.52	2.39	1.10	1.46	1,41	2.19	1.51	1.21	1.39	2.22	1.61
13	2.46	1.65	2.40	2.45	2.22	1,35	2.00	1.48	2.20	1.35	1.74	1.51
14	1 40	1.66	2.39	1.70	1.39	1.34	1.32	1.35	1.44	1.22	1.29	1.55
15	2.38	2.30	2.32	1.94	1.42	1.24	1.35	1.41	1.47	1.19	1.21	0.60
16	2.30	2.30	2.41	2.29	2.06	1.40	2.03	1.47	2.06	1.40	1.93	1.55
17	2 50	1.81	1.64	2.12	2.02	1,39	1.98	1.36	1.96	1.44	1.97	1.45
19	2.38	2.45	2.33	2.48	2.21	1.47	1.98	1.47	2.22	1.50	1.11	1.57
19	2.38	2.23	2.39	1.88	1.45	1.37	1.37	1.29	1.48	1.38	1,35	1.18
20	2.34	1.98	2.31	1.53	1.31	1.31	1.33	1.41	1.41	1.01	1.24	1.51
20	2.04	2.31	1.62	2.24	2.14	1,45	1.95	1.41	2.09	1.38	1.83	1.43
22	2.34	2.43	2.41	2.18	2.09	1.49	1.70	1.34	2.11	1.51	1.90	1.55
23	2.04	2.24	2.39	2.40	1.34	1,48	2.34	1.47	1.51	1.67	2.62	1.50
24	2 50	1.90	2.01	1.79	1.36	1,40	1.40	1.37	1.31	1.36	1.46	1.28
25	2.00	1.4.3	1.88	2.02	1.39	1,42	2.00	1.41	1.33	1.30	2.02	1.44
20	1 68	1 72	2.35	2.32	2.04	1.41	1.98	1.39	1.89	1.37	2.20	1.62
20	2.00	2 4 8	2 44	2.55	2.03	1.45	2.00	1.44	1.11	1.20	1.10	1.73
20	2.30	2 33	2.47	1.84	1.41	1.30	1.36	1.31	2.01	1.35	1.31	1.49
20	2 3 6	2.00	1 29	2.40	1.98	1.95	2.05	1.36	1.35	1.91	2.03	1.45
20	2,40	1.93	2.35	2.02	1.33	1,40	1.33	1.28	1.86	1.47	1.39	1.40
30	2.23	1 4 5	1.46	2.16	1.37	1,38	1.39	1.36	1.30	1.37	1.47	1.44
32	2.46	2.46	1.82	1.75	1.36	1,44	1.30	1,40	1.42	1.54	1.75	1.03

PRE			POST				FINAL					
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	12.0	13.0	11.0	10.0	17.0	10.0	8.0	22.0	16.0	9.0	11.0	19.0
2	7.0	28.0	9.0	4.0	15.0	32.0	6.0	6.0	13.0	22.0	10.0	6.0
3	10.0	16.0	5.0	11.0	20.0	10.0	4.0	12.0	31.0	15.0	5.0	14.0
4	9.0	0.0 *	21.0	6.0	12.0	-3.0 *	10.0	9.0	7.0	0.0	11.0	7.0
5	17.0	9.0	6.0	8.0	12.0	11.0	11.0	12.0	14.0	5.0	13.0	8.0
6	9.0	7.0	15.0	6.0	9.0	7.0	11.0	9.0	8.0	4.0	11.0	9.0
7	21.0	27.0	18.0	12.0	7.0	10.0	10.0	11.0	3.0	7.0	8.0	11.0
8	11.0	18.0	8.0	10.0	10.0	9.0	9.0	26.0	9.0	8.0	11.0	19.0
9	Б.О	3.0	7.0	6.0	17.0	6.0	9.0	5.0	14.0	5.0	10.0	7.0
10	10.0	Б.О	10.0	48.0	12.0	18.0	8.0	9.0	17.0	21.0	8.0	10.0
11	5.0	8.0	16.0	37.0	12.0	16.0	3.0	15.0	14.0	16.0	11.0	12.0
12	10.0	10.0	18.0	14.0	19.0	18.0	7.0	26.0	14.0	18.0	8.0	10.0
13	14.0	18.0	17.0	9.0	13.0	15.0	18.0	26.0	11.0	14.0	14.0	19.0
14	8.0	6.0	13.0	9.0	17.0	10.0	24.0	57.0	16.0	7.0	19.0	10
15	12.0	5.0	12.0	6.0	15.0	11.0	26.0	10.0	15.0	9.0	18.0	2.0
16	9.0	13.0	8.0	21.0	12.0	9.0	8.0	27.0	10.0	11.0	12.0	11 0
17	6.0	33.0	11.0	10.0	10.0	11.0	8.0	11.0	10.0	74.0	13.0	12.0
18	7.0	11.0	14.0	10.0	11.0	73.0	24.0	12.0	10.0	74.0	12.0	7 0
19	6.0	24.0	8.0	7.0	9.0	5.0	19.0	10.0	9.0	7.0	13.0	11.0
20	53.0 *	9.0	15.0	11.0	42.0	13.0	7.0	12.0	41.0	10.0	22.0	22.0
21	19.0	12.0	18.0	20.0	112.0 *	23.0	38.0	26.0	100.0 *	19.0	33.0	23.0
22	9.0	8.0	6.0	18.0	14.0	4.0	7.0	27.0	10.0	15.0	12.0	20.0
23	6.0	15.0	9.0	34.0	8.0	18.0	11.0	31.0	0.0	20.0	24.0	7.0
24	25.0	26.0	15.0	10.0	8.0	28.0	24.0	0.0	12.0	20.0	17.0	17.0
25	25.0	7.0	5.0	13.0	17.0	11.0	16.0	22.0	13.0	9.0	15.0	7.0
26	7.0	70	12.0	7.0	11.0	10.0	9.0	8.0	10.0	10.0	10.0	39.0
27	24.0	21.0	12.0	22.0	26.0	15.0	21.0	38.0	19.0	70.0	0.0	12.0
28	20.0	8.0	9.0	20.0	12.0	5.0	8.0	12.0	23.0	21.0	10 0	12.0
29	8.0	18.0	8.0	14.0	20.0	25.0	15.0	14.0	14.0	120	0.61	9.0
30	20.0	24.0	23.0	7.0	49.0	16.0	25.0	8.0	14.0	11 0	19.0	12.0
31	14.0	6.0	12.0	21.0	21.0	14.0	18.0	13.0	45.0	220	0.0	9.0
32	10.0	25.0	10.0	11.0	12.0	32.0	3.0	14.0	10.0	J∠.U	5.0	5.0

Sodium (Normal Range 136 - 144 mmol/I)

PRE			POST				FINAL					
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	142.0	116.0	113.0	138.0	166.0	157.0	161.0	163.0	171.0	154.0	153.0	164.0
2	141.0	140.0	141.0	142.0	167.0	157.0	162.0	160.0	159.0	156.0	167.0	161.0
3	142.0	106.0	140.0	140.0	172.0	167.0	164.0	166.0	223.0 *	160.0	171.0	177.0
4	140.0	88.0	118.0	119.0	167.0	162.0	170.0	165.0	158.0	159.0	169.0	165.0
5	141.0	102.0	139.0	96.0	171.0	172.0	166.0	167.0	165.0	146.0	163.0	165.0
6	139.0	113.0	135.0	101.0	167.0	169.0	169.0	164.0	166.0	139.0	169.0	166.0
7	137.0	123.0	102.0	132.0	171.0	164.0	166.0	162.0	110.0	134.0	167.0	162.0
8	124.0	126.0	115.0	105.0	174.0	167.0	160.0	164.0	166.0	166.0	155.0	163.0
9	133.0	82.0	140.0	143.0	167.0	167.0	156.0	163.0	160.0	156.0	154.0	169.0
10	135.0	109.0	138.0	140.0	173.0	162.0	168.0	169.0	197.0 *	154.0	127.0	204.0
11	104.0	125.0	140.0	135.0	158.0	159.0	165.0	164.0	160.0	156.0	156.0	167.0
12	135.0	107.0	140.0	182.0	170.0	167.0	165.0	165.0	136.0	156.0	165.0	170.0
13	143.0	114.0	140.0	142.0	167.0	169.0	159.0	165.0	160.0	161.0	144.0	100.0
14	99.0	118.0	142.0	101.0	168.0	171.0	170.0	164.0	163.0	151.0	163.0	175.0
15	138.0	137.0	141.0	115.0	175.0	173.0	170.0	164.0	175.0	162.0	149.0	41.0
16	140.0	143.0	139.0	139.0	169.0	166.0	159.0	166.0	163.0	158.0	148.0	168.0
17	142.0	119.0	108.0	131.0	161.0	165.0	161.0	165.0	151.0	166.0	153.0	174.0
18	140.0	140.0	138.0	142.0	169.0	168.0	167.0	169.0	167.0	165.0	102.0	150.0
19	138.0	136.0	138.0	121.0	167.0	168.0	164.0	168.0	160.0	163.0	158.0	120.0
20	137.0	118.0	138.0	107.0	174,0	175.0	159.0	167.0	1/1.0	128.0	140.0	150.0
21	140.0	141.0	110.0	135.0	168.0	166.0	162.0	165.0	161.0	150.0	153.0	100.0
22	141.0	141.0	140.0	138.0	166.0	166.0	160.0	171.0	159.0	108.0	174.0	167.0
23	136.0	133.0	141.0	139.0	149.0	165.0	163.0	164.0	165.0	180.0	179.0	160.0
<u>2</u> 4	142.0	120.0	121.0	110.0	170.0	169.0	167.0	165.0	159.0	159.0	104.0	162.0
25	138.0	102.0	117.0	119.0	162.0	165.0	156.0	163.0	152.0	151.0	103.0	102.0
26	113.0	115.0	138.0	138.0	169.0	163.0	163.0	166.0	154.0	154.0	183.0	192.0
27	144.0	140.0	140.0	141.0	157.0	169.0	164.0	163.0	129.0	134.0	89.0	170.0
28	138.0	140.0	140.0	126.0	173.0	171.0	170.0	166.0	155.0	169.0	167.0	173.0
29	138.0	142.0	95.0	140.0	165.0	165.0	162.0	167.0	158.0	152.0	103.0	167.0
30	141.0	125.0	137.0	127.0	167.0	164.0	167.0	166.0	148.0	102.0	170.0	170.0
31	136.0	100.0	107.0	130.0	174 0	168.0	170.0	168.0	154.0	150.0	1/8.0	112.0
32	140.0	138.0	111.0	109.0	169.0	165.0	169.0	167.0	162.0	173.0	227.0 -	112.0

Potassium (Normal Range 3.2 - 4.8 mmol/l)

PRE		POST					FINAL					
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	4.5	3.3	3.6	4.2	3.3	3.2	3.5	3.5	3.3	3.3	3.3	3.5
2	3.7	3.6	3.9	4.1	3.2	3.0	3.3	3.2	3.0	3.0	3.4	3.2
3	3.5	5.2	3.8	4.6	3.6	3.7	3.2	3.4	4.7	3.6	3.3	3.6
4	5.0	4.2	3.6	5.6	5.1	4.2	4.2	4.3	4.8	4.2	4.2	4.3
5	4.1	4.9	4.8	14.5 *	4.6	4.9	5.4	4.7	4.5	4.1	5.3	4.6
6	3.8	7.6	9.1	5.6	3.2	3.4	3.2	3.0	3.2	2.8	3.2	3.0
7	6.2	3.4	9.3	4.1	3.4	2.9	3.3	3.1	2.2	2.4	3.3	3.1
8	4.0	6.6	3.9	3.4	3.2	3.1	3.3	3.1	3.1	3.2	3.2	3.1
9	8.5	4.2	3.9	5.4	4.9	5.0	3.9	4.1	4.6	4.7	3.9	4.0
10	3.5	6.2	8.0	4.2	3.9	3.6	3.9	4.1	4.4	3.4	2.9	4.8
11	3.3	3.9	4.0	3.9	3.0	3.0	3.1	3.2	3.0	3.0	2.9	3.3
12	4.3	3.3	4.1	2.9	3.9	3.5	3.8	3.7	3.1	3.2	3.8	3.8
13	4.3	3.0	4.0	4.3	4.5	5.4	4.2	4.7	4.4	5.1	3.9	4.0
14	2.8	3.3	4.9	17.0 *	3.6	3.1	3.5	3.2	3.6	2.8	3.3	5.5 • • • •
15	4.1	6.7	3.9	7.1	4.0	3.9	3.5	3.2	4.0	3.7	3.1	0.8
16	4.2	3.9	4.4	3.5	4.2	4.5	4.3	4.9	4.0	4.3	4.1	5.0
17	Б.О	6.0	5.7	5.5	3.5	3.4	3.4	3.7	3.3	3.5	3.2	3.7
18	4.6	4.1	3.9	4.3	4.3	3.5	3.9	4.1	4.2	3.5	2.5	4.2
19	4.3	5.8	4.1	3.6	4.2	5.1	4.5	5.0	4.0	4.9	4.3	4.0
20	4.0	E .0	4.4	2.7	3.9	3.5	3.8	3.9	3.9	2.6	3.5	4.0
21	4.2	3.9	3.1	3.8	4.3	4.7	4.1	4.3	4.1	4.4	3.5	4.1
22	4.2	4.3	5.0	3.8	4.2	3.7	3.4	3.9	4.0	<u>ر</u> . /	3.7	4.2
23	3.5	3.9	4.1	4.4	3.2	3.2	3.6	3.1	.15	3.5	4.0	3.1
24	3.9	13.8 *	4.2	7.3	4.8	4.8	4.9	4.3	4,5	4.0	4.9	4.0
25	4.3	5.6	5.3	12.6 *	3.4	3.2	3.2	3.2	3.2	2.9	3.4 3 E	3.2
26	3.4	5.0	3.8	3.7	3.2	3.0	3.1	3.9	3.0	2.9	0.0	4.0
27	4.0	5.1	4.6	4.8	3.9	3.7	4.5	3.7	3.1	3.0	2.4	4,4 2 /
28	3.7	3.7	4.1	6.3	3.2	3.0	2.8	3.2	3.8	3.0	2.0	3.4
29	3.9	3.7	6,3	4.8	3.3	3.1	3.0	3.3	3.0	2.8	3.0 3.5	
30	4.0	3.5	7.6	4.0	3.0	3.2	3.4	3.5	2.9	<u>ა.</u> 1	3.0	3.5
31	6.5	3.4	3.5	3.6	4.3	3.9	3.8	3.6	2.8	3.6	4.0	<u>ა.</u> წ
32	3.8	4.5	3.5	7.4	3.4	3.4	3.6	3.4	3.3	3.6	4,8	2.2

Chloride (Normal Range 99 -106 mmol/l)

PRE			POST					FINAL				
NO	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4	RUN 1	RUN 2	RUN 3	RUN 4
1	105.0	96.0	82.0	105.0	74.0	71.0	73.0	74.0	73.0	67.0	60.0	69,0
2	109.0	109.0	103.0	106.0	80.0	73.0	70.0	78.0	73.0	70.0	68.0	73.0
2	106.0	80.0	108.0	107.0	76.0	75.0	77.0	79.0	106.0	71.0	76.0	83.0
3	105.0	62.0	92.0	92.0	79.0	71.0	76.0	78.0	66.0	71.0	68.0	73.0
-7	110.0	73.0	110.0	77.0	84.0	73.0	83.0	80.0	73.0	55.0	7 7.0	74.0
6	104.0	80.0	105.0	72.0	77.0	68.0	77.0	74.0	73.0	54.0	72.0	70.0
7	105.0	91.0	81.0	99.0	78.0	78.0	77.0	71.0	28.0	52.0	72.0	71.0
, p	92.0	97.0	85.0	79.0	74.0	71.0	79.0	85.0	65.0	68.0	69.0	78.0
a	101.0	54.0	106.0	107.0	74.0	77.0	76.0	81.0	65.0	67.0	69.0	73.0
10	99.0	83.0	106.0	106.0	81.0	76.0	76.0	82.0	86.0	67.0	42.0 *	92.0
11	78.0	92.0	109.0	98.0	75.0	73.0	71.0	72.0	75.0	68.0	61.0	68.0
12	102.0	76.0	107.0	54.0	72.0	71.0	77.0	78.0	39.0 *	61.0	70.0	76.0
13	107.0	85.0	109.0	106.0	76.0	67.0	70.0	72.0	67.0	60.0	56.0	68.0
14	72 0	88.0	106.0	83.0	83.0	75.0	74.0	70.0	71.0	57.0	65.0	66.0
15	100.0	106.0	109.0	88.0	80.0	74.0	78.0	77.0	73.0	69.0	55.0	1.0 *
16	106.0	109.0	105.0	103.0	79.0	79.0	82.0	71.0	71.0	71.0	70.0	66.0
17	104.0	89.0	80.0	99.0	80.0	78.0	74.0	75.0	67.0	78.0	62.0	72.0
18	106.0	106.0	107.0	104.0	80.0	71.0	75.0	73.0	74.0	68.0	29.0 *	/1.0
10	106.0	107.0	105.0	94.0	80.0	78.0	79 .0	76.0	72.0	68.0	70.0	68.0
20	103.0	89.0	105.0	77.0	76.0	79.0	68.0	77.0	70.0	38.0	56.0	74.0
21	105.0	106.0	81.0	101.0	74.0	77.0	73.0	77.0	63.0	66.0	65.0	66.0
22	113.0	103.0	108.0	103.0	74.0	78.0	74.0	74.0	69.0	77.0	81.0	77.0
27	101.0	103.0	106.0	103.0	6 6.0	77.0	74.0	74.0	71.0	89.0	83.0	69.0
20	105.0	96.0	90.0	86.0	81.0	74.0	76.0	72.0	71.0	65.0	70.0	59.0
24	103.0	50.0	89.0	94.0	67.0	77.0	77.0	73.0	57.0	69.0	73.0	66.0
26	85 O	85.0	103.0	106.0	77.0	79.0	72.0	80.0	65.0	70.0	81.0	92.0
20	105.0	103.0	101.0	105.0	68.0	74.0	79.0	75.0	36.0	48.0	13.0	36.0
20	108.0	107.0	102.0	99.0	78.0	76.0	73.0	7 7.0	60.0	72.0	69.0	80.0
20	105.0	111.0	72.0	103.0	78.0	77.0	76.0	70.0	63.0	67.0	69.0	68.0
20	100.0	99.0	107.0	99.0	77.0	78.0	75.0	74.0	65.0	75.0	74.0	70.0
30	104.0	71 0	79.0	99.0	75.0	76.0	74.0	76.0	66.0	67.0	73.0	82.0
32	104.0	103.0	81.0	81.0	76.0	78.0	74.0	78.0	72.0	79.0	106.0	29.0

FACTOR VI	11 :	POST PR	E STA	ENDIX III TISTICAL DATA			
General L Dependent	inear Mode Variable	rla Procedure : Y			* den	otes signif	icance
Source Model Error Corrected	Total.	DFSum of244.5041034.9021279.407	of Squares 142500 266250 708750	Mean Squ 0.187684 0.047598	lare 37 867	F Value 3.94	Pr > F 0.0001
		R-Square 0.478833	C.V. 327.7689	Root MSE 0.218173	E Y Me 18 0.00	ean 6656250	
Source	DF	Type III S	SS	Mean Square	F Value	Pr >	·F
R.	3	0.43823125	5	0.14607708	3.07	0.03	12
V1	1	0.00945312	2	0.00945312	0.20	0.65	68
V2	1	0.01125000)	0.01125000	0.24	0.62	:79
V1 * V2	1	0.00165312	2	0.00165312	0.03	0.85	525
V3	1	0.03001250)	0.03001250	0.63	0.42	90
V1 * V3	1	0.00025312	2	0.00025312	0.01	0.94	20
V2 * V3	1	0.21125000)	0.21125000	4.44	0.03	76 *
V4	1	0.82882812	2	0.82882812	17.41	0.00	01 *
V1 * V4	1	0.30031250)	0.30031250	6.31	0.01	.36 *
V2 * V4	1	0.06752812	2	0.06752812	1.42	0.23	64
V3 * V4	1	0.00227812	2	0.00227812	0.05	0.82	73
V5	1	0.93061250)	0.93061250	40.56	0.00	01 *
V1 * V5	1.	0.01757813	3	0.01757813	0.37	0.54	47
V2 * V5	1.	0.00720000)	0.00720000	0.15	0.69	81
V3 * V5	Э.	0.01531250)	0.01531250	0.32	0.57	18
V4 * V5	1.	0.00165312	2	0.00165312	0.03	0.85	525
V6	1	0.29645000)	0.29645000	6.23	0.01	.42 *
V1 * V6	1	0.03712812	2	0.03712812	0.78	0.37	92
V2 * V6	1	0.03125000)	0.03125000	0.66	0.41	.97
V3 * V6	1	0.09901250)	0.09901250	2.08	0.15	523
V4 * V6	1	0.03712813	3	0.03712813	0.78	0.37	92
V5 * V6	1	0.13005000)	0.13005000	2.73	0.10	14

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		0.05796875 0.07515625	0.02727140 0.02727140	0.0359 0.0069
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. -1		0.05718750 0.07593750	0.02727140 0.02727140	0.0384 0.0064
V1	V 2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0.04500000	0.03856758	0.2460
].	- 1	0.07093750	0.03856758	0.0688
~ 1	1	0.06937500	0.03856758	0.0750
-].	-]	0.08093750	0.03856758	0.0383
V 3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		0.08187500	0.02727140	0.0034
- 1		0.05125000	0.02727140	0.0630

V1	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0.07187500	0.03856758	0.0652
1	- 1	0.04406250	0.03856758	0.2559
-1	1	0.09187500	0,03856758	0.0190
].	-1	0.05843750	0.03856758	0.1328
V2	V3	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: $LSMEAN = 0$
1	1	0.11312500	0.03856758	0.0041
1	- 1	0.00125000	0.03856758	0.9742
- 1	1.	0.05062500	0.03856758	0.1922
- 1	~1	0.10125000	0.03856758	0.0100
V4		Y	Std Err	Pr > ۲۳۲
		LSMEAN	LSMEAN	HO: $LSMEAN = 0$
1		0.14703125	0.02727140	0.0001
-1		-0.01390625	0.02727140	0.6112
V1	V4	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.09000000	0.03856758	0.0216
1	- 1	0.02593750	0.03856758	0,5028
<u>]</u>	1	0.20406250	0.03856758	0.0001
-1	- 1	-0.05375000	0.03856758	0,1664

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1] - 1 - 1 - 1	0.11468750 -0.00031250 0.17937500 -0.02750000	0.03856758 0.03856758 0.03856758 0.03856758	0.0037 0.9936 0.0001 0.4774
¥3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	0.16656250 0.00281250 0.12750000 -0.02500000	0.03856758 0.03856758 0.03856758 0.03856758	0.0001 0.9420 0.0013 0.5183
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		0.18937500 -0.05625000	0.02727140 0.02727140	0.0001 0.0417
Vl	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.16906250 -0.05312500 0.20968750 -0.05937500	0.03856758 0.03856758 0.03856758 0.03856758 0.03856758	0.0001 0.1714 0.0001 0.1267

V2	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	0.18750000 -0.07312500 0.19125000 -0.03937500	0.03856758 0.03856758 0.03856758 0.03856758 0.03856758	0.0037 0.0608 0.0001 0.3097
£V	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1]. - 1	0.21562500 -0.05187500 0.16312500 -0.06062500	0.03856758 0.03856758 0.03856758 0.03856758	0.0001 0.1816 0.0001 0.1190
V4	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.27343750 0.02062500 0.10531250 -0.13312500	0.03856758 0.03856758 0.03856758 0.03856758	0.0001 0.5940 0.0074 0.0008
V 6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
]. -]		0.01843750 0.11468750	0.02727140 0.02727140	0.5005 0.0001

V1	V6	Ŷ	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: $LSMEAN = 0$
1	1	0.02687500	0.03856758	0.4875
1	- 1	0.08906250	0.03856758	0.0229
- 1	1	0.01000000	0.03856758	0.7959
- 1	- 1	0.14031250	0.03856758	0.0004
v 2	٧6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	l	0.02468750	0.03856758	0.5235
1	- 1	0.08968750	0.03856758	0.0220
1	1	0.01218750	0.03856758	0.7526
- 1.	- 1	0,13968750	0.03856758	0.0005
V3	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: $LSMEAN = 0$
1	1	0.00593750	0.03856758	0.8779
1	- 1	0.15781250	0.03856758	0.0001
-]	1	0.03093750	0.03856758	0.4243
- 1	- 1.	0.07156250	0.03856758	0.0664
V4	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.08187500	0.03856758	0.0362
1	- 1	0.21218750	0.03856758	0.0001
-1	1	~0.04500000	0.03856758	0.2460
-1	-1	0.01718750	0.03856758	0.6568

Lul : POST - PRE

V5	V6	Y	Std Err	Pr > ITI	
		LSMEAN	LSMEAN	HO: LSMEAN =	0
1	1	0.17312500	0.03856758	0,0001	
1	~ 1	0.20562500	0.03856758	0.0001	
~ 1	1	-0.13625000	0.03856758	0.0006	
~].	~ 1	0.02375000	0.03856758	0.5394	

FACTOR VIII ; PFODUCTION

General Lin Dependent V	ear Mod ariable	els Procedu ; Y	re			*	denotes	significance
Source Model Error Corrected Te	otal	DF 24 103 127	Sum of Squ 2908.7589 7530.0417 10438.8007	lares 98125 79922 78047	Mean 1 121.11 73.10	Square 9829089 9720193	F Value 1.66	Pr > F 0.0431
		R-Square 0.278649		C.V. 75.03275	Root 1 8.550;	MSE 27496	Y M 11.	lean 39539062
Source	DF	Туре	III SS	Mean Squ	lare	F Va	lue	Pr > F
R	3	217.	79180859	72,5972	6953	0.9	9	0.3992
V7	1	94.	78923828	94.7892	3828	1.3	0	0.2575
V8	1	13.	44859453	13.4485	9453	0.1	.8	0,6689
V9	1	403.	74163203	403.7416	3203	5.5	2	0.0207 *
V10	1	254	.50500078	254.5050	0078	3.4	.8	0.0649
V1.1	1	6 .	.04215703	6.0421	.5703	0.0	8	0.7743
V7 * V11	1	36.	.36978828	36.3697	8828	0.5	59	0.4822
V8 * V11	1	106	.01500078	106.0150	0078	1.4	5	0,2313
V9 * V11	1	81.	.32906953	81.3290	6953	1.1	.1	0.2940
V10 * V11	1	32.	.37106953	32.3710	6953	0.4	4	0.5073
V12	1	6.	.82189453	6.8218	9453	0.0)9	0.7606
V11 * V12].	4	.12203828	4.1220	3828	0.0	6	0.8128
V13	1	15.	71501953	15.7150)1953	0.2	21	0.6439
V7 * V13	1	45.	47003203	45.4700	3203	0.6	2	0.4321
V8 * V13	1	0 .	.74572578	0.7457	2578	0.0	1.	0.9197
V9 * V13	1	24	.36892578	24.3689	92578	0.3	13	0.5650
V10 * V13	1	8.	64760078	8.6476	50078	0.1	.2	0.7316
V11 * V13	1	25.	82109453	25.8210	9453	0.3	5	0.5536
V12 * V13	1	1283.	66111328	1283.6611	1328	17.5	6	0.0001 *
V14	1	149.	62337578	149.6233	7578	2.0	15	0.1556
V11 * V14	1	65.	10831328	65.1083	1328	0.8	9	0.3475
V13 * V14	1	32.	25048828	65.2504	8828	0.4	4	0.5081

FACTOR VIII : PRODUCTION

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	12.2559375	1.0687844	0.0001
- 1	10.5348437	1.0687844	0.0001
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	11.7195312	1.0687844	0.0001
1	11.0712500	1.0687844	0.0001
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	13.1714062	1.0687844	0.0001
- 1	9.6193750	1.0687844	0.0001
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN ≈ 0
1	12.8054687	1.0687844	0.0001
- 1	9.9853125	1.0687844	0,0001

FACTOR VIII : PRODUCTION

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		11.6126562 11.1781250	1.0687844 1.0687844	0.0001 0.0001
V7	Vll	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 ~1	13.0062500 11.5056250 10.2190625 10.8506250	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001
V8	V1 1	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	11.8468750 11.5921875 10.3784375 11.7640625	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001
V9	V] 1	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 - 1	1 - 1 1 - 1	12.5915625 13.7512500 10.6337500 8.6050000	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001

FACTOR VIII : PRODUCTION

V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1] -]. -]. -].	13.5256250 12.0853125 9.6996875 10.2709375	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - <u>1</u>		11.6262500 11.1645312	1.0687844 1.0687844	0.0001 0.0001
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	11.6640625 11.5612500 11.5884375 10.7678125	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001
V 13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		11.7457812 11.0450000	1.0687844 1.0687844	0.0001 0.0001

FACTOR VILL : PRODUCTION

V7	V13	Y	Std Err	Pr > IT1
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	12.0103125	1.5114894	0.0001
Э.	- 1	12.5015625	1.5114894	0.0001
- 1	1.	11.4812500	1,5114894	0.0001
-]].	9.5884375	1.5114894	0.0001
V8	V 13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	12.1462500	1.5114894	0.0001
1	- 1	11.2928125	1.5114894	0.0001
1	1	11.3453125	1.5114894	0.0001
- 1	- 1	10.7971875	1.5114894	0.0001
V9	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	.1	13.9581250	1.5114894	0.0001
1	1	12.3846875	1.5114894	0.0001
- 1	1	9.5334375	1.5114894	0.0001
- 1	- 1	9.7053125	1.5114894	0.0001
V10	V13	Y	Std Err	Pr > IT1
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	12.8959375	1.5114894	0.0001
1	- 1	12.7150000	1.5114894	0.0001
- 1	1	10.5956250	1.5114894	0.0001
- 1	- 1	9.3750000	1.5114894	0.0001

FACTOR VILL : PRODUCTION

V11	V1.3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = C)
1. 1 - 1 - 1	1 - 1 - 1 - 1	12.4121875 10.8131250 11.0793750 11.2768750	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001	
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0)
1 - 1 - 1	1 - 1 1 - 1	15.1434375 8.1090625 8.3481250 13.9809375	1.5114894 1.5114894 1.5114894 1.5114894 1.5114894	0.0001 0.0001 0.0001 0.0001	
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = ()
1 - 1		12.4765625 10.3142187	1.0687844 1.0687844	0.0001 0.0001	
V11	V14	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = ()
1 1 - 1 - 1	1 -1 1 -1	11.9806250 11.2446875 12.9725000 9.3837500	1,5114894 1,5114894 1,5114894 1,5114894	0.0001 0.0001 0.0001 0.0001	

. PRODUCTION

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	3.	32.3250000	1.5114894	0.0001
3	- 1	11.1665625	1.5114894	0.0001
-1	1.	12.6281250	1.5114894	0.0001
- 1	- 1	9.4618750	1.5114894	0.0001

General Linear Mo	dels Procedi	Пе	*	denotes signi:	ticance
Source Model Error Corrected Total	DF 24 103 127	Sum of Squares 5.92653125 16.52995625 22.45648750	Mean Square 0.24693880 0.16048501	F Value 1.54	Pr > F 0.0717
	R-Square 0.263912	C.V. -327.2926	Root MSE 0.40060581	Y M ean -0.10343'	750
Source	DF	Type III SS	Mean Square	F Value	Pr > F
R	3	0.85211875	0.28403958	1.77	0.1576
V1.	1	0.10237812	0.10237812	0.64	0.4263
V2	1	0,23805000	0.23805000	1.48	0.2260
V1. * V2	1	0.05362812	0.05362812	0.33	0.5645
V3	1	0.16102813	0.16102813	1.00	0.3188
V1 * V3	1	0.03380000	0.03380000	0.21	0.6473
V2 * V3	1	0.00090312	0.00090312	0.01	0.9403
V4	1	0.03001250	0.03001250	0.19	0.6663
V1. * V4	1	0.58050312	0,58050312	3.63	0.0600
V2 * V4	1	0.06480000	0.06480000	0.40	0.5266
V3 * V4	1	0.00812813	0.00812813	0.05	0.8224
V 5	1	0.01162813	0.01162813	0.07	0.7883
V1 * V5	1	0.02420000	0.02420000	0.15	0.6986
V2 * V5	1	0.20320313	0.20320313	1.27	0.2631
V3 * V5	1	0.15961250	0.15961250	0.99	0.3210
V4 * V5	1	1.88665312	1.88655312	11.76	0.0009 *
ν6	1	0.69325312	0.69325312	4.32	0.0402 *
V1 * V6	1	0.40051250	0.40051250	2.50	0.1172
V2 * V6	1	0.22612813	0.22612813	1.41	0.2379
V3 * V6	1	0.14851250	0.14851250	0.93	0.3383
V4 * V6	1	0.04727812	0.04727812	0.29	0.5885
V5 * V6	1	0.00020000	0.00020000	0.00	0.9719

POST - PRE

FIBRINOGEN

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V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.07515625 -0.13171875	0.05007573 0.05007573	0.1365 0.0098
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
]]		-0.06031250 -0.14656250	0.05007573 0.05007573	0.2312 0.0042
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1.	1	~0.05250000	0.07081777	0.4602
1	- 1	-0.09781250	0.07081777	0.1702
- 1	1	-0.06812500	0.07081777	0.3383
1	- 1.	-0.19531250	0.07081777	0.0069
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.06796875	0.05007573	0.1776
- 1		-0.13890625	0.05007573	0.0066

Vl	V 3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1. - 1. 1. - 1.	-0.05593750 -0.09437500 -0.08000000 -0.18343750	0.07081777 0.07081777 0.07081777 0.07081777	0.4314 0.1856 0.2612 0.0110
V2	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1. - 1 - 1	1 - 1 1 - 1	-0.02750000 -0.09312500 -0.10843750 -0.18468750	0.07081777 0.07081777 0.07081777 0.07081777	0.6986 0.1914 0.1288 0.0105
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.11875000 -0.08812500	0.05007573 0.05007573	0.0001 0.0814
Vı	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	ב 1 1 1	-0.15781250 0.00750000 -0.07968750 -0.18375000	0.07081777 0.07081777 0.07081777 0.07081777	0.6986 0.9159 0.2631 0.0108

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 -1 1 -1	-0.09812500 -0.02250000 -0.13937500 -0.15375000	0.07081777 0.07081777 0.07081777 0.07081777	0.1689 0.7513 0.0517 0.0322
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1] -] 1 · 1	-0.09125000 -0.04468750 -0.14625000 -0.13156250	0.07081777 0.07081777 0.07081777 0.07081777	0.2005 0.5294 0.0414 0.0661
V 5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.09390625 -0.11296875	0.05007573 0.05007573	0.0636 0.0262
V1	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.07937500 -0.07093750 -0.10843750 -0.15500000	0.07081777 0.07081777 0.07081777 0.07081777	0.2650 0.3188 0.1288 0.0309

V2	V5	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.09062500	0.07081777	0.2035
1	- 1	-0.03000000	0.07081777	0.6727
- 1	1	-0.09718750	0.07081777	0.1729
- 1	-1	-0.19593750	0.07081777	0.0067
V 3	V 5	Ŷ	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	-0.02312500	0.07081777	0,7447
1	- 1	-0,11281250	0.07081777	0,1142
- 1	1	-0,16468750	0.07081777	0.0220
- 1	- 1	0,11312500	0.07081777	0.1132
V4	V5	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0,01218750	0.07081777	0.8637
1	- 1	-0.24968750	0.07081777	0.0006
- 1	1	0.2000000	0.07081777	0.0057
-]	- 1	0.02375000	0.07081777	0.7380
V 6		Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1		0.17703125	0.05007573	0.0006
-1		-0.02984375	0.05007573	0.5525

General Linear Models Procedure Least Square Means

V1	V6	y lsmean	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	-0.09281250 -0.05750000 -0.26125000 -0.00218750	0.07081777 0.07081777 0.07081777 0.07081777	0.1929 0.4187 0.0004 0.9754
V2	V 6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1.] - 1 - 1.	1 - 1 1 - 1	-0.09187500 -0.02875000 -0.26218750 -0.03093750	0.07081777 0.07081777 0.07081777 0.07081777 0.07081777	0.1974 0.6856 0.0003 0.6631
V3	A8	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 - 1	-0.10750000 -0.02843750 -0.24656250 -0.03125000	0.07081777 0.07081777 0.07081777 0.07081777	0.1321 0.6888 0.0007 0.6599
V4	V 6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1. 1. 1.] -] 1 -]	-0,17312500 -0.06437500 -0.18093750 0.00468750	0.07081777 0.07081777 0.07081777 0.07081777 0.07081777	0.0162 0.3655 0.0121 0.9474

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- POST - PRE

V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1.	-0.16625000	0.07081777	0.0208
1	- 1	-0.02156250	0.07081777	0.7614
-1	1	-0,18781250	0.07081777	0.0093
-1	- 1	-0.03812500	0.07081777	0.5915

General Linear Mod Dependent Variable	els Procedu : Y	ire	 * denotes significance 			
Source Model Error Corrected Total	DF 24 103 127	Sum of Squares 1065.46106250 1955.06312500 3020 524187507	Mean Square 44.39421094 18.98119539	F Value 2.34	Pr > F 0.0017	
	R-Square 0.352740	C.V. 50.79082	Root MSE 4.35674137	Y Mean 8.577812	50	
Source	DF	Type III SS	Mean Square	F Value	Pr > F	
R V7 V8	3 1 1	13.90491250 104.04031250 37.41125000	4.63497083 104.04031250 37.41125000	0.24 5.48 1.97	0.8653 0.0211 * 0.1634	
V9 V1.0 V1.1	1 1 1	181.59415313 166.75945313 31.00781250	181.59415313 166.75945313 31.00781250	9.57 8.79 1.63	0.0025 * 0.0038 * 0.2041	
V7 * V11 V8 * V11	1 1	12.12781250 18.12020000 22.93337812	12.12781250 18.12020000 22.93337812	0.64 0.95	0.4259	
V10 * V11 V12	1 1	20.36815313 25.40062813	22.93337812 20.36815313 25.40062813	1.07 1.34	0.3027	
V11 * V12 V13 V7 * V13	1 1 1	6.41715312 5.49461250 1.33661250	6.41715312 5.49461250 1.33661250	0.34 0.29 0.07	0.5622 0.5917 0.7913	
V8 * V13 V9 * V13	1 1 1	0.36551250 188.51965312	0.36551250 188.51965312 8.03002812	0.02 9.93 0.42	0.8899 0.0021 * 0.5169	
V10 * V13 V11 * V13 V12 * V13	1 1 1	41.90701250 0.71102812	41.90701250 0.71102812	2.21	0.1404 0.8469	
V14 V11 * V14 V13 * V14	1 1 1	97.47570313 49.67552812 31.86015312	97.47570313 49.67552812 31.86015312	5.14 2.62 1.68	0.0255 * 0.1088 0.1980	

V7	Y	Std Err	Pr > 1TI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
]	9.47937500	0.54459267	0.0001
- 1	7.67625000	0.54459267	0.0001
V 8	y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	9.11843750	0.54459267	0.0001
- 1	8.03718750	0.54459267	0.0001
V 9	y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
*	9,76890625	0.54459267	0.0001
	7,38671875	0.54459267	0.0001
V 10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1-1	9.71921875	0.54459267	0.0001
	7.43640625	0.54459267	0.0001
ננע	Y	Std Err	Pr > 1T1
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1-1	9.07000000	0.54459267	0.0001
	8.08562500	0.54459267	0.0001

General Linear Models Procedure Least Square Means

V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	9.66375000	0.77017034	0.0001
1	- 1	9.29500000	0.77017034	0.0001
- 1	- 1	8.47625000	0.77017034	0.0001
- 1	- 1	6.87625000	0.77017034	0.0001
V 8	V1 1	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1].	9.23437500	0.77017034	0.0001
1	-]	9.00250000	0.77017034	0.0001
- 1	-]	8.90562500	0.77017034	0.0001
- 1	-]	7.16875000	0.77017034	0.0001
V 9	V1.1	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	9.83781250	0.77017034	0.0001
1	- 1	9.70000000	0.77017034	0.0001
-1	1	8.30218750	0.77017034	0.0001
-1	- 1	6.47125000	0.77017034	0.0001

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V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1]. - 1 1 - 1	10.6103125 8.8281250 7.5296875 7.3431250	0.77017034 0.77017034 0.77017034 0.77017034	0.0001 0.0001 0.0001 0.0001
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		9.02328125 8.13234375	0.54459267 0.54459267	0.0001 0.0001
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	9.29156250 8.84843750 8.75500000 7.41625000	0.77017034 0.77017034 0.77017034 0.77017034	0.0001 0.0001 0.0001 0.0001
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		8.37062500 8.78500000	0.54459267 0.54459267	0.0001

General Linear Models Procedure Least Square Means

V7	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	9.17000000	0.77017034	0.0001
1	- 1	9.78875000	0.77017034	0.0001
···].	1	7.57125000	0.77017034	0.0001
-1	-1	7.78125000	0.77017034	0.0001
V8	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	.].	8,85781250	0.77017034	0.0001
1	- 1	9.37906250	0.77017034	0.0001
-1	1	7,88343750	0.77017034	0.0001
-1	1.	8.19093750	0.77017034	0.0001
V9	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
l	1	8.34812500	0.77017034	0.0001
1	- 1	11.18968750	0.77017034	0.0001
- 1	1.	8,39312500	0.77017034	0.0001
- 1	-1	6.38031250	0.77017034	0.0001
V1 0	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	9.2615625	0.77017034	0.0001
1	~ 1	10.1768750	0.77017034	0.0001
- 1.	1	7.4796875	0.77017034	0.0001
- 1	-1	7.3931250	0.77017034	0,0001

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V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	9.43500000	0.77017034	0.0001
1	~ 1	8.70500000	0.77017034	0.0001
-1	1	7.30625000	0.77017034	0.0001
-1	~ 1	8.86500000	0.77017034	0.0001
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	8.74156250	0.77017034	0.0001
1	- 1	9.30500000	0.77017034	0.0001
- 1	1	7.99968750	0.77017034	0.0001
- 1	- 1	8.26500000	0.77017034	0.0001
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		9.45046875	0.54459267	0.0001
-1		7.70515625	0.54459267	0.0001
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	9.31968750	0.77017034	0.0001
1	-1	8.82031250	0.77017034	0.0001
-1	1	9.58125000	0.77017034	0.0001
-1	-1	6.59000000	0.77017034	0.0001

: PRODUCTION

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0		
1	3.	8.74437500	0.77017034	0.0001		
1	-1	7.99687500	0.77017034	0.0001		
- 1	1	10.15656250	0.77017034	0.0001		
-1	-].	7.41343750	0.77017034	0.0001		
General I	rinear Mode	His Procedu	1.6.	A denotes significance		
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Dependent	Variable	: У				
Source		DF	Sum of Squares	Mean Square	F Value	Pr > F
Model		24	150292.93750000	6262.20572917	3.80	0.0001
Error		103	169731.01367188	1647.87391914		
Corrected	Total	127	320023.95117188			
		R-Square	С.V.	Root MSE	Y Mean	
		0.469630	-1465.736	40.59401334	-2.76953	125
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F
R	3	103759,83	398437	34586.11322812	20.99	0.0001
V1	1.	82.08	007813	82.08007814	0.05	0.2838
V2	1	627,90	820313	627.90820313	0.38	0.5384
V1 * V2	1	3714.14	257813	3714,14257813	0.25	0.1363
V3	1	4614,00	195313	4614.00195313	2.80	0.0973
V1 * V3	1	4307.08	007813	4307.08007813	2.61	0.1090
V2 * V3	1	714.89	257813	714.89257813	0.43	0.5116
V4	1	22.36	132813	22.36132813	0.01	0.9075
VI * V4	1	3408.28	320313	3408,28320313	2.07	0.1534
V2 * V4	1	8.76	757813	8,76757813	0.01	0.9420
V3 * V4	1	25,83	007813	25,83007813	0.02	0.9006
V5	1	948.84	570313	948,84570313	0.58	0.4497
V1 * V5	1	1692.89	257813	1692,89257813	1.03	0.3132
V2 * V5	1	5336,73	632813	5336,73632813	3.24	0.0749
V3 * V5	1	8232.04	882813	8232,04882813	5.00	0.0276 *
V4 * V5	1	2902.26	757813	2902.26757813	1.76	0.1874
V6	1	43.36	132813	43,36132813	0.03	0.8715
V1 * V6	1	7177.51	757813	7177,51757813	4,36	0.0394 *
V2 * V6	1	422.31	445313	422,31445313	0.26	0.6138
V3 * V6	1	987.34	570313	987.34570313	0.60	0.4407
V4 * V6	1	998,48	632813	998.48632813	0.61	0.4381
V5 * V6	1	265.939	945313	265,93945313	0.16	0.6887

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		-1,96875000 -3,57031250	5.07425167 5.07425167	0.6988 0.4833
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
] - 1		-4.98437500 -0.55468750	5.07425167 5.07425167	0.3283 0.9132
V1	V 2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	1,2031250	7.17607558	0.8672
1	1	-5,1406250	7,17607558	0.4754
- 1	1	11,1718750	7.17607558	0.1226
- 1	1	4.0312500	7.17607558	0.5755
V.3		Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1		3.23437500	5.07425167	0.5253
1		-8.77343750	5.07425167	0.0868

V1.	V3	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1	1 ~ 1	-1.7656250 2.1718750	7.1760755 7.1760755	0.8061 0.7628
~ 1.	1	8.2343750	7.1760755	0.2538
- 7	·· .	~15,3750000	7.1760755	0,0345
V2	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	~1,34375000	7.1760755	0.8518
1	1	-8.62500000	7.1760755	0.2322
-]	.1	7,81250000	7.1760755	0,2788
· 1	·]	-8.91218750	7.1760755	0.2166
V4		Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1		-2.35156250	5.07425167	0,6440
- 1		~3.18750000	5.07425167	0.5313
V1	V4	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	3.60937500	7.1760755	0.6161
1	- 1	7,54687500	7.1760755	0.2954
- 1	1	-8.31250000	7.1760755	0.2494
~ 1	1	1,17187500	7.1760755	0.8706

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 - 1	1 -] 1 1	4.82812500 -5.14062500 0.12500000 1.23437500	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.5026 0.4754 0.9861 0.8638
٧3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1. - 1 1 - 1	3.20312500 3.26562500 ~7.90625000 ~9.64062500	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.6563 0.6500 0.2731 0.1821
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		0.04687500 5.49218750	5.07425167 5.07425167	0.9926 0.2816
٤V	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -] -] -]	4.39062500 -8.32812500 -4.48437500 -2.65625000	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.5420 0.2485 0.5334 0.7120

V 2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1.]	-8.71875000	7.1760755	0.2272
1	- 1	-1.25000000	7.1760755	0.8621
].	3	8.62500000	7.1760755	0.2322
- 1	- 1	-9.73437500	7.1760755	0.1779
V3	VS	Y	Std Err	Pr > ITT
• • •	• •	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	-2,0625000	7.1760755	0,7744
1	- 1	8.5312500	7.1760755	0.2372
- 1	1	1.9687500	7.1760755	0,7844
- 1	- 1	19.5156250	7.1760755	0.0077
V4	V5	v	Std Err	Pr > ITT
	• 3	LSMEAN	ISMEAN	HO: $LSMEAN = 0$
l	1.	-4.3906250	7.1760755	0.5420
1	~ 1	-0.3125000	7.1760755	0,9653
- 1	1	4,2968750	7.1760755	0.5506
- 1	- 1	-10.6718750	7.1760755	0.1400
V6		Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1		-3.35156250	5.07425167	0.5104
- 1		-2.18750000	5.07425167	0.6673

V1	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITL HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	4.9375000 -8.8750000 -11.6406250 4.5000000	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.4930 0.2190 0.1078 0.5320
V2	٧6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1]. - 1] - 1	-3.75000000 -6.21875000 -2.95312500 1.84375000	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.6024 0.3882 0.6815 0.7977
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1 - 1	-0.1250000 6.5937500 -6.5781250 -10.9687500	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.9861 0.3603 0.3615 0.1294
V4	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.14062500 -4.56250000 -6.56250000 0.18750000	7.1760755 7.1760755 7.1760755 7.1760755 7.1760755	0.9844 0.5263 0.3626 0.9792

____BRAND FACTOR : POST - PRE

V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1.	0.81250000	7.1760755	0,9101
1	1	0.90625000	7,1760755	0.8998
·]	1	-7.51562500	7.1760755	0.2974
- 1	- 1	-3.46875000	7.1760755	0,6299

General Linear Models Procedure Dependent Variable : Y

denotes significance

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Sour Mode Errc	.ce sl vi.	5		DF 24 103	Sum of Squar 164085.03437 193626.78117	es 500 187	Mean Square 6836.87643229 1879.87166186	F Value 3.64	Pr > F 0.0001
Corr	ec:	cted	Total	127 B. Soularo	357711,81554	688		V. Moom	
				0.458707	- 1.	.v. 77.0879	43.35748680	-24.4835	9375
Sour	ce	3		DF	Type III SS	Mean Square	F Value	Pr > F	
R			3	9071	9,55148437	30239.85049479	16.09	0.0001	
ν.			1	128	84.61132812	1284.61132812	0.68	0.4103	
V8			1	<u>n</u>	4.47070312	54.47070312	2 0.03	0.8652	
V9			1	2157	7.43445312	21577.43445312	11.48	0.0010 *	
V10			1	1538	9.15820312	15389.15820312	8.19	0.0051 *	
V11			1	847	4.39257812	8474.39257812	2 4.51	0.0361 *	
V7	*	V11	1	64	3.95632812	643.95632812	2 0.34	0.5596	
V8	*	V11	1	90	8.97820312	908.97820312	0.48	0.4884	
V9	×	V11	1.	7	7.34570312	77.34570312	2 0.04	0.8397	
V10	×	V11	1	154	6.37507813	1546.37507813	3 0.82	0,3665	
V12			1	192	21.22507812	1921.22507812	2 1.02	0.3144	
V11	*	V12	1	249	8.36132812	2498,36132812	2 1.33	0.2517	
V13			1	Ę.	64.47070313	54,47070313	0.03	0.8652	
V7	*	V13	1	26	57.09382812	267,09382812	2. 0.14	0.7070	
A8	*	V13	1.	116	9.46570312	1169,46570312	2 0.62	0.4321	
V9	*	V13	1	114	9.00195313	1149.00195313	0.61	0.4361	
V10	*	V13	1.		5.65320312	5.65320312	2 0.00	0.5964	
V11	*	V13	1	204	7.20007813	2047,20007813	3 1.09	0.2991	
V12	*	V13	1	1003	7.67382813	10037.67382813	5,34	0.0228*	
V14			1	397	7.20507812	3977.20507812	2 2,12	0.1488	
V11	*	V14	1	15	9.53445313	159.53445313	0.08	0.7714	
V13	*	V14	1	12	1.87507812	121,87507812	0,06	0.7995	

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-21.3156250	5.4196859	0.0002
	-27.65156257	5.1496859	0.0001
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
۲	-23.8312500	5.4196859	0.0001
۳	-25.1359375	5.1496859	0.0001
V 9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-11.5000000	5.4196859	0.0362
~ 1	-37.4671875	5.1496859	0.0001
V10	Y	Std Err	Pr > ITI
	LIS MEAN	LSMEAN	HO: LSMEAN = 0
1	13.5187500	5.4196859	0.0142
- 1	-35.4484375	5.1496859	0.0001

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-16.3468750 -32.6203125	5.4196859 5.1496859	0.0032 0.0001
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 1	1 - 1. - 1 - 1	-15,4218750 -27.2093750 -17.2718750 -38.0312500	7.6645932 7.6645932 7.6645932 7.6645932 7.6645932	0.0468 0.0006 0.0263 0.0001
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 	1 - 1 - 1 - 1	18.3593750 29.3031250 14.3343750 35.9375000	7.6645932 7.6645932 7.6645932 7.6645932	0.0184 0.0002 0.0463 0.0001
Λð	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1]]]	1 - 1 - 1	-4.1406250 -18.8593750 -28.5531250 -46.3812500	7.6645932 7.6645932 7.6645932 7.6645932	0.5902 0.0155 0.0003 0.0001

V10	V1.1.	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 ~ 1 - 1	-1,9062500 -25,1312500 -30,7875000 -40,1093750	7.6645932 7.6645932 7.6645932 7.6645932 7.6645932	0.8041 0.0014 0.0001 0.0001
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-20.6093750 -28.3578125	5.4196859 5.1496859	0.0002 0.0001
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	-16.8906250 -15.8031250 -24.3281250 -40.9125000	7.6645932 7.6645932 7.6645932 7.6645932 7.6645932	0.0298 0.0417 0.0020 0.0001
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-25.1359375 -28.8312500	5.4196859 5.1496859	0.0142 0.0001

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1		-23.4125000 -19.2187500 -26.8593750 -28.4437500	7.6645932 7.6645932 7.6645932 7.6645932 7.6645932	0.0029 0.0137 0.0007 0.0003
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1 - 1	-27.5062500 -20.1562500 -22.7656250 -27.5062500	7,6645932 7.6645932 7.6645932 7.6645932	0.0005 0.0099 0.0037 0.0005
V9	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	-9.1562500 -13.8437500 -41.1156250 -33.8187500	7.6645932 7.6645932 7.6645932 7.6645932	0.2350 0.0738 0.0001 0.0001
V10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-14.3812500 -12.6562500 -35.8906250 -35.0062500	7.6645932 7.6645932 7.6645932 7.6645932	0.0634 0.1017 0.0001 0.0001

V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 · 1] ~ 1	-13.0000000 -19.6937500 -37.2718750 -27.9687500	7.6645932 7.6645932 7.6645932 7.6645932 7.6645932	0.0929 0.0116 0.0001 0.0004
V12	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1 - 1	1 - 1 - 1 - 1	12.4062500 -28.8125000 -37.8656250 -18.8500000	7.6645932 7.6645932 7.6645932 7.6645932	0.1068 0.0003 0.0001 0.0156
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-18,9093750 -30,0578125	5.4196859 5.1496859	0.0007 0.0001
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 1	1 - 1 - 1	9.6562500 23.0375000 28.1625000 37.0781250	7.6645932 7.6645932 7.6645932 7.6645932	0.2106 0.0033 0.0004 0.0001

V13	V14	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	-20.5375000	7.6645932	0.0086
1	- 1	-29.7343750	7.6645932	0.0002
~ 1	1	-17.2812500	7,6645932	0.0263
- 1.	-1	-30,3812500	7.6645932	0.0001

pH : POST - PRE

General L	inear Mode	els Procedure			t den	the cimificance
Dependent	Variable	: Y			Gen	stes significance
Source		DF Sum o	f Squares	Mean Square	F Value	Pr > F
Model		24 1.853	93125	0.07724714	1 73	0 0311
Error		103 4.596	61875	0.04462737	4.75	0.0011
Corrected	Total	127 6.450	55000	0.01.01/01		
		R-Square	C.V.	Root MSE	V Mean	
		0.287407	132.5502	0.21125190	0.1593750	0
Source	DF	Type III S	S	Mean Square	F Value	Pr > F
R	3	0.85446250		0.85446250	6.38	0 0005
V1	1	0.07125312		0.07125312	1,60	0.2092
V2	1.	0.03850313		0.03850313	0.86	0.3551
V1 * V2	1	0.01051250		0.01051250	0.24	0.6285
V3	1	0.00211250		0,00211250	0.05	0.8282
V1 * V3	1	0.04425312		0.04425312	0.99	0.3217
V2 * V3	1.	0.01487812		0.01487812	0.33	0.5649
V4	1	0.12005000		0.12005000	2.69	0.1040
V1 * V4	1	0.01487812		0.01487812	0.33	0.5649
V2 * V4	1	0.05865313		0.05865313	1.31	0.2543
V3 * V4	1	0.04651250		0.04651250	1.04	0.3097
V5	1	0.04500000		0.04500000	1.01	0.3177
V1 * V5	1	0.00052812		0.00052812	0.01	0.9136
V2 * V5	1	0.00002813		0.00002813	0.00	0.9800
V3 * V5	1	0.01280000		0.01280000	0.29	0.5934
V4 * V5	1	0.01531250		0.01531250	0.34	0.5593
V6	1	0.31205000		0.31205000	6.99	0.0095 *
V1 * V6	1	0.15540313		0.15540313	3.48	0.0649
V2 * V6	1	0.0000313		0.00000313	0.00	0.9933
V3 * V6	1	0.03511250		0.03511250	0.79	0.3771
V4 * V6	1	0.00101250		0.00101250	0.02	0.8806
V5 * V6	1	0.00061250		0.00061250	0.01	0.9070

PH : POST PRE

1 V		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
.] -]		0.13578125 0.18296875	0.02640649 0.02640649	0.0001 0.0001
V2		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -		0.17671875 0.14203125	0.02640649 0.02640649	0.0001 0.0001
V1	V 2	y Iismean	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0.14406250	0.03734441	0.0002
. 1	· .1	0.12750000	0.03734441	0.0009
]]	0.15656250	0.03734441 0.03734441	0.0001 0.0001
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN ≈ 0
1		0.15531250	0.02640649	0.0001
.4		0.10341750	0.02640649	0.0001

PH : POST - PRE

٤V	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 _1 -] - 1	1 1 1 - 1	0.15031250 0.12125000 0.16031250 0.2-562500	0.03734441 0.03734441 0.03734441 0.03734441	0.0001 0.0016 0.0001 0.0001
V2	Δ3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	0.16187500 0.19156250 0.14875000 0.13531250	0.03734441 0.03734441 0.03734441 0.03734441	0.0001 0.0001 0.0001 0.0005
V4		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		0.15531250 0.16343750	0.02640649 0.02640649	0.0001 0.0001
V1	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 2 - 1 - 1	1 1 1 1	0.11593750 0.15562500 0.14156250 0.22437500	0.03734441 0.03734441 0.03734441 0.03734441	0.0025 0.0001 0.0003 0.0001

PH : POST - PRE

Λ5	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 1	1 1 1 - 1	0.12468750 0.22875000 0.13281250 0.15125000	0.03734441 0.03734441 0.03734441 0.03734441 0.03734441	0.0012 0.0001 0.0006 0.0001
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	0.14375000 0.16687500 0.11375000 0.21312500	0.03734441 0.03734441 0.03734441 0.03734441	0.0002 0.0001 0.0029 0.0001
V5		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		0.17812500 0.14062500	0.02640649 0.02640649	0.0001 0.0001
V.1	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	0.15656250 0.11500000 0.19968750 0.16625000	0.03734441 0.03734441 0.03734441 0.03734441	0.0001 0.0027 0.0001 0.0001

PH : POST - PRE

V2	V5	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.19500000 0.15843750 0.16125000 0.12281250	0.03734441 0.03734441 0.03734441 0.03734441	0.0001 0.0001 0.0001 0.0014
V3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 .1 .1 - 1	1 - 1 - 1	0.18406250 0.12656250 0.17218750 0.15468750	0.03734441 0.03734441 0.03734441 0.03734441	0.0001 0.0010 0.0001 0.0001
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.13656250 0.12093750 0.21968750 0.16031250	0.03734441 0.03734441 0.03734441 0.03734441	0.0004 0.0016 0.0001 0.0001
۷6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		0.20875000 0.11000000	0.02640649 0.02640649	0.0001 0.0001

pH : POST - PRE

V1	٧6	Y	Std Err	Pr > ITI
		LISMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.15031250	0.03734441	0.0001
1	- 1	0.12125000	0.03734441	0.0016
- 1	1	0.26718750	0.03734441	0.0001
- 1	- 1	0.09875000	0.03734441	0.0095
V2	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.22593750	0.03734441	0.0001
1	- 1	0.12750000	0.03734441	0.0009
- 1	1	0.19156250	0.03734441	0.0001
· 1	- 1	0.09250000	0.03734441	0.0149
٧3	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.22125000	0.03734441	0.0001
1	- 1	0.08937500	0.03734441	0.0185
- 1	1	0.19625000	0.03734441	0.0001
- 1	- 1	0.13062500	0.03734441	0.0007
V4	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	0.17531250	0.03734441	0.0001
]	1	0.08218750	0.03734441	0.0300
- 1	1	0.24218750	0.03734441	0.0001
- 1	- 1	0.13781250	0.03734441	0.0004

pH : POST - PRE

V5	VĞ	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0,22531250	0.03734441	0,0001
1	- 1.	0,13093750	0.03734441	0.0007
- 1	1	0,19218750	0.03734441	0.0001
· 1	- 1	0.08906250	0.03734441	0.0189

1

1

1

0.07507813

0.02000000

0.00661250

V14

V11 * V14

V13 * V14

General Linear Models Procedure denotes significance * Dependent Variable : Y Source \mathbf{DF} Sum of Squares Mean Square F Value Pr > FModel 24 1.24002188 0.05166758 2.80 0.0002 Error 103 1,89785000 0.01842573 Corrected Total 127 3.13787187 **R-Square** C.V. Root MSE Y Mean 0.395179 -133.0390 0.13574140 -0.10203125Source DF Type III SS Mean Square F Value Pr > FR 3 0.15230313 0.05076771 2.76 0.0462 V7 1 0.09570313 0.09570313 5.19 0.0247 * V8 1 0.16820000 0.16820000 9.13 0.0032 * V9 1 0.00052812 0.00052812 0,03 0.8659 V10 1 0.08201250 0.08201250 4.45 0.0373 * V11 1 0.03001250 0.03001250 1.63 0.2047 V7 * V11 1. 0.02205000 0.02205000 1.20 0.2765 * V11 0.00015313 V8 1 0.00015313 0.01 0.9275 V9 * V11 1 0.00080000 0.00080000 0.04 0.8354 V10 * V11 1 0.05200312 0.05200312 2.82 0.0960 V12 1 0.00125000 0.00125000 0.07 0.7950 V11 * V12 1 0.04277813 0.04277813 2.32 0.1306 V13 1 0.01201250 0.01201250 0.65 0.4213 V7 * V13 1 0.00211250 0.00211250 0.11 0.7356 V8 * V13 1 0.01320312 0.01320313 0.72 0.3992 V9 * V13 1 0.13520000 0.13520000 7,34 0.0079 * V10 * V13 1 0.00300313 0.00300313 0.16 0,6873 V11 * V13 1 0.06037812 3.28 0.06037812 0.0732 V12 * V13 1 0.26462813 0.26462813 14.36 0.0003 *

250

0.07507813

0.02000000

0.00661250

4.07

1.09

0.36

0.0461 *

0.2999

0.5504

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	~0.07468750	0.01696768	0.0001
- 1	~0.12937500	0.01696768	0.0001
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-0.06578125	0.01696768	0.0001
- 1.	-0.13828125	0.01696768	0.0001
٧9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	0,10009000	0.01696768	0.0001
- 1	0,10406250	0.01696768	0.0001
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-0.07671875	0.01696768	0.3001
- 1	-0.12734375	0.01696768	0.0001

V.1.4		Y LSME'AN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
ן ב		-0.08671875 -0.11734375	0.01696768 0.01696768	0.0001 0.0001
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.07250000 -0.07687500 -0.10093750 -0.15781250	0.02399592 0.02399592 0.02399592 0.02399592	0.0032 0.0018 0.0001 0.0001
ν8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.04937500 -0.08218750 -0.12406250 -0.15250000	0.02399592 0.02399592 0.02399592 0.02399592	0.0422 0.0009 0.0001 0.0001
Λð	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 1	1 - 1] - 1	-0.08718750 -0.11281250 -0.08625000 -0.12+87500	0.02399592 0.02399592 0.02399592 0.02399592	0.0004 0.0001 0.0005 0.0001

V10	V11	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.08156250 -0.07187500 -0.09187500 -0.16281250	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0010 0.0034 0.0002 0.0001
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.09890625 -0.10515625	0.01696768 0.01696768	0.0001 0.0001
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.06531250 -0.10812500 -0.13250000 -0.10218750	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0076 0.0001 0.0001 0.0001
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.09234375 -0.11171875	0.01696768 0.01696768	0.0001 0.0001

General Linear Models Procedure Least Square Means

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-0.06093750 -0.08843750 -0.12375000 -0.13500000	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0126 0.0004 0.0001 0.0001
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.06625000 -0.06531250 -0.11843750 -0.15812500	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0068 0.0076 0.0001 0.0001
V9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~1 ~1 ~1] -] -] -]	-0.12281250 -0.07718750 -0.06187500 -0.14625000	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0001 0.0017 0.0113 0.0001
V10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1. - 1	-0.06218750 -0.09125000 -0.12250000 -0.13218750	0.02399592 0.02399592 0.02399592 0.02399592 0.02399592	0.0109 0.0002 0.0001 0.0001

V11.	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 1 1	-0.09875000 -0.07468750 -0.08593750 -0.14875000	0.02399592 0.02399592 0.02399592 0.02399592	0.0001 0.0024 0.0005 0.0001
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.04375000 -0.15406250 -0.14093750 -0.06937500	0.02399592 0.02399592 0.02399592 0.02399592	0.0712 0.0001 0.0001 0.0047
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.12625000 -0.07781250	0.01696768 0.01696768	0.0001 0.0001
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO. LSMEAN = 0
1 1 - 1 1	1 - 1 1 - 1	0,09843750 0,07500000 0,15406250 0,08062500	0.02399592 0.02399592 0.02399592 0.02399592	0.0001 0.0023 0.0001 0.0011

General Linear Models Procedure Least Square Means

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V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0)
1. 1 - 1] - 1 1	-0.12375000 -0.06093750 -0.12875000	0.02399592 0.02399592 0.02399592	0.0001 0.0126 0.0001 0.0001	

General L Dependent	inear Mode Variable	ls Procedu. : Y	Ľe		* deno	otes significance
Source Model Error Corrected	Total	DF 24 103 127	Sum of Squares 0.84258125 1.59489297 2.43747422	Mean Square 0.03510755 0.01548440	F Value 2.27	Pr > F 0.0025
		R-Square 0.345678	C.V. -111.7744	Root MSE 0.12443632	Y Mean -0.111328	312
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F
R	3	0.401	60859	0 13396053	0 65	
V1	1	0.043	314453	0.04214452	8,65	0.0001
V2	1	0.021	78828	0.04314453	2.79	0.0981
V1 * V2	1	0.068	391328	0.02178828	1.41	0.2383
V3	1	0 029	970703	0.00091328	4.45	0.0373 *
V1 * V3	- 1	0 029	503203	0.02970703	1.92	0.1690
V2 * V3	1	0 001	253828	0.02503203	1.62	0.2064
V4	1	0.059	994453	0.00253828	0.16	0.6864
V1 * V4	1	0 000	106328	0.05994453	3.87	0.0518 *
V2 * V4	1	0.000	103828	0.00006328	0.00	0.9492
V3 * V4	1	0.00	219452	0.00003828	0.00	0.9604
V5	1	0.001		0.03219453	2.08	0.1524
V1 * V5	1	0.002	419405 106053	0.00219453	0.14	0.7073
$V_2 * V_5$	+ 1	0.00.	-004E2	0.00106953	0.07	0.7932
V3 * V5		0.01:	1009455 1000E2	0.01509453	0.97	0.3258
V4 * V5	1	0.00	/90953	0.00796953	0.51	0.4747
VG VG	۲. ۱	0.01.		0.01106328	0.71	0.3999
VO 171 * 176	1 r	0.020	075703	0.02075703	1.34	0.2496
	1	0.000	57038	0.00657038	0.04	0.8372
	1	0.005	91328	0.00591328	0.38	0.5380
V.5 * V6	1	0.007	/35078	0.00735078	0,47	0.4924
V4 * V6	1	0.009	97578	0.00997578	0,64	0.4240
VP * Ne	1	0.075	56328	0.07556328	4.88	0.0294 *

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.09296875	0.01555454	0.0001
- 1		-0.12968750	0.01555454	0.0001
V2		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.09828125	0.01555454	0.0001
- 1		-0.12437500	0.01555454	0.0001
V1	V 2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0.10312500	0.02199744	0.0001
1	- 1	0.08281250	0.02199744	0.0003
- 1	1	0.09343750	0.02199744	0.0001
- 1	- 1	0.16593750	0.02199744	0.0001
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1.		-0. 12656 250	0.01555454	0.0001
- 1		-0.09609375	0.01555454	0.0001

V1	ν3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.12218750	0.02199744	0.0001
1	- 1	-0.06375000	0.02199744	0.0046
- 1	1	-0.13093750	0.02199744	0.0001
- 1	- 1	-0.12843750	0.02199744	0.0001
V2	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.10906250	0.02199744	0.0001
1	- 1	-0.08750000	0.02199744	0.0001
-1	1	-0.14406250	0.02199744	0.0001
-1	- 1	-0.10468750	0.02199744	0.0001
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.08968750	0.01555454	0.0001
- 1		-0.13296875	0.01555454	0.0001
V1	٧4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.07062500	0.02199744	0.0018
1	- 1	-0.11531250	0.02199744	0.0001
- 1	1	-0.10875000	0.02199744	0.0001
- 1	- 1	-0.15062500	0.02199744	0.0001

General Linear Models Procedure Least Square Means

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.07718750 -0.11937500 -0.10218750 -0.14656250	0.02199744 0.02199744 0.02199744 0.02199744	0.0007 0.0001 0.0001 0.0001
ν3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-0.08906250 -0.16406250 -0.09031250 -0.10187500	0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0001 0.0001 0.0001
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1		-0.11546875 -0.10718750	0.01555454 0.01555454	0.0001 0.0001
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-0.1000000 -0.08593750 -0.13093750 -0.12843750	0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0002 0.0001 0.0001

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V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1. - 1 - 1 - 1	-0.09156250 -0.10500000 -0.13937500 -0.10937500	0.02199744 0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0001 0.0001 0.0001
Δ3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-0.12281250 -0.13031250 0.10812500 -0.08406250	0.02199744 0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0001 0.0001 0.0002
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 -1 -1	-0.10312500 -0.07625000 -0.12781250 -0.13812500	0.02199744 0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0008 0.0001 0.0001
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.09859375 -0.12406250	0.01555454 0.01555454	0.0001 0.0001

V1	V 6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.08250000 -0.10343750 -0.11468750 -0.14468750	0.02199744 0.02199744 0.02199744 0.02199744 0.02199744	0.0003 0.0001 0.0001 0.0001
V2	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1	1 - 1 - 1.	-0.07875000 -0.11781250 -0.11843750 -0.13031250	0.02199744 0.02199744 0.02199744 0.02199744	0.0005 0.0001 0.0001 0.0001
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1				
1 - 1 - 1	1 - 1 1 - 1	-0.10625000 -0.14687500 -0.09093750 -0.10125000	0.02199744 0.02199744 0.02199744 0.02199744	0.0001 0.0001 0.0001 0.0001
1 - 1 - 1 V4	1 - 1 - 1 - 1 V6	-0.10625000 -0.14687500 -0.09093750 -0.10125000 Y LSMEAN	0.02199744 0.02199744 0.02199744 0.02199744 Std Err LSMEAN	0.0001 0.0001 0.0001 0.0001 Pr > ITI HO: LSMEAN = 0

V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.07843750	0.02199744	0.0006
1	- 1	-0.15250000	0.02199744	0.0001
- 1	1	-0.11875000	0.02199744	0.0001
- 1	- 1	~0.09562500	0.02199744	0.0001

MAGNESIUM : PRODUCTION

General Linear Models Procedure Dependent Variable : Y

denotes significance

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Source Model Error Corrected	Total	DF 24 103 127	Sum of Squa 0.28127500 1.07177422 1.35304922	res Mean Squa 0.0117197 0.0104055	re F Value 9 1.13 7	€ Pr > F 0.3298	
		R-Square 0.207882		C.V. -177.6461	Root MSE 0.10200772	Y Mean -0.05742187	
Source	DF	Туре	III SS	Mean Squa	re F	Value Pr > 1	F
R V7	3	0.1	13507109	0.045023	70 4	0.006	5
V8	1	0.0	0056953	0.000569	53 (0.815	5
vo		0.0	JUZI3423	0.002194	53 (0.647	0
V10		0.0	00004403	0.005644	53 (0.463	1
V11	1	0.0	000000000	0.023382	03	2.25 0.136	9
V7 * V11	1	0.0	00003020	0.000038	28 (0.951	8
V8 * V11	- 1	0.0	00050000	0.022313	38	2.14 0.146	1
V9 + V11	1	0.0	00203020	0.002538	28 (0.622	4
V10 + V11	1	0.1	00013203	0.000132	(03)	0.01 0.910	5
V12	1	0.0	01301333	0.013819	53	0.251	8
V11 * V12	1	0.0	00790393	0.007965	93 (0.383	5
V13	1	0,1	00271993	0.002719	153 (ED	0.26 0.610	3
V7 * V13	1	0.1	000034300	0.000344	-53 (-79 (0.856	0
V8 * V13	1	0	01381953	0.001100	120 (150 1	0.736	1.
V9 + V13	1	0.0	00172578	0.013013	נכי סר סר	0.251	8
V10 + V13	1	0.0	03611328	0.001720	10 (20 -		7
V11 * V13	1	0,0	00011020	0.000000	20 2	0.065	3
V12 * V13	1	0.0	00020020	0.000200	20 (ED (0.374	2
V14	1	0.0	00253203	0.000019	03 (22 (Б
V11 * V14	1	0,0	00106953	0.002002	() () () () () () () () () () () () () (1.40 0.659	5
V13 * V14	1	<u>0.</u>	00028203	0.000282	03 (0.749	∠ 6
V7	Y	Std Err	Pr > ITI				
-----	-------------	------------	----------------				
	LSMEAN	LSMEAN	HO: LSMEAN = 0				
1	-0.05531250	0.01275096	0.0001				
- 1	-0.05953125	0.01275096	0.0001				
V8	Y	Std Err	Pr > ITI				
	LSMEAN	LSMEAN	HO: LSMEAN = 0				
1.	-0.05328125	0.01275096	0.0001				
1	-0.06156250	0.01275096	0.0001				
V9	Y	Std Err	Pr > ITI				
	ISMEAN	LSMEAN	HO: LSMEAN = 0				
1	-0.06406250	0.01275096	0.0001				
- 1	-0.05078125	0.01275096	0.0001				
V10	Y	Std Err	Pr > ITI				
	LSMEAN	LSMEAN	HO: LSMEAN = 0				
1	-0.07093750	0.01275096	0.0001				
- 1	-0.0439-625	0.01275096	0.0008				

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.05796875 -0.05687500	0.01275096 0.01275096	0.0001 0.0008
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~1 -1	1 -1 -1 -1	-0.06906250 -0.04156250 -0.04687500 -0.07218750	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0002 0.0232 0.0107 0.0001
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 1 - 1	-0.04937500 0.05718750 -0.06656250 -0.05656250	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0073 0.0020 0.0004 0.0022
V9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.06562500 -0.06250000 -0.05031250 -0.05125000	0.01803259 0.01803259 0.01803259 0.01803259	0.0004 0.0008 0.0063 0.0054

V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1.	1 - 1 1 - 1	-0.08187500 -0.06000000 -0.03406250 -0.05375000	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0001 0.0012 0.0617 0.0036
V12		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1.		-0.04953125 -0.06531250	0.01275096 0.01275096	0.0002 0.0001
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.05468750 -0.06125000 -0.04437500 -0.06937500	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0031 0.0010 0.0155 0.0002
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.05578125 -0.05906250	0.01275096 0.01275096	0.0001 0.0001

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 1 - 1	-0.05062500 -0.06000000 -0.06093750 -0.05812500	0.01803259 0.01803259 0.01803259 0.01803259	0.0060 0.0012 0.0010 0.0017
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1 - 1	-0.04125000 -0.06531250 -0.07031250 -0.05281280	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0242 0.0005 0.0002 0.0042
۷9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 ~ 1 1 - 1	-0.05875000 -0.06937500 -0.05281250 -0.04875000	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0015 0.0002 0.0042 0.0080
V 10	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 · 1 · 1 · 1	-0.05250000 -0.08937500 -0.05906250 -0.02875000	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.00 44 0.0001 0.0014 0.1139

V11	V13	Y IJSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.06437500 -0.05156250 -0.04718750 -0.06656250	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0005 0.0051 0.0102 0.0004
V12	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-0.04750000 -0.05156250 -0.06406250 -0.06656250	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0097 0.0051 0.0006 0.0004
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.06140625 -0.05343750	0.01275096 0.01275096	0.0001 0.0001
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.05906250 -0.05687500 -0.06375000 -0.05000000	0.01803259 0.01803259 0.01803259 0.01803259 0.01803259	0.0014 0.0021 0.0006 0.0066

'13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN =	0
1	1	-0,06125000	0.01803259	0.0010	
1	- 1	-0.05031250	0.01803259	0.0063	
1	1	0,06156250	0,01803259	0.0009	
• 1	· 1	0.05656250	0.01803259	0.0022	
1 1 1 1	1 -1 1 -1	-0.06125000 -0.05031250 -0.06156250 -0.05656250	0.01803259 0.01803259 0.01803259 0.01803259	0.0010 0.0063 0.0009 0.0022	

TOTAL PRO)TEAN ;	POST PRE			
General L Dependent	dnear Mode Variable	els Procedure : Y	*	denotes signi	ficance
Source		DF Sum of Squares	Mean Square	F Value	Pr > F
Frror		24 5044.43750000) 210.18489583	1.87	0.0164
Corrected	Total	103 11569.67968750	112.32698726		
	10141	$P_{\rm s}$ Square $Q_{\rm W}$			
		0.303624 0.001	ROOT MSE	Y Mean	
		0.505024 ~204.0001	10.598844268	-5.19531	250
Source	DF	Type III SS	Mean Square	F Value	Pr > F
R	3	1584.77343750	528,25781250	4 70	0 0041
V1	1	508.00781250	508.00781250	4 50	
V2	1	187.69531250	187.69531250	1 67	0.0338 *
V1 * V2	1	328.32031250	328.32031250	2.92	0.1990
V.3	1	17.25781250	17.25781250	0.15	0.6959
V1 * V3	1	134.07031250	134.07031250	1 19	0.0000
V2 * V3	1	11.88281250	11.88281250	0.11	0.2772
V4	1	835.38281250	835.38281250	7.44	0 0075 *
V1 * V4	1	5.69531250	5.69531250	0.05	0.8223
V2 * V4	1.	2.25781250	2.25781250	0.02	0.8875
V3 * V4	1	244.75781250	244.75781250	2.18	0.1430
V5	1	0.38281250	0.38281250	0.00	0.9536
V1 = V5	1.	267.38281250	267.38281250	2.38	0.1259
V2 * V5	1	89.44531250	89.44531250	0.80	0.3743
V3 * V5	1	29.07031250	29.07031250	0.26	0.6120
V4 * V5	Ţ	173.44531250	173.44531250	1.54	0.2168
V0	1	409.69531250	409.69531250	3.65	0.0589 *
VI * Vb	1	14.44531250	14.44531250	3.13	0.7206
V2 * V6	1	13,13281250	13.13281250	0.12	0.7331
V.5 * V6	1	126.00781250	126.00781250	1.12	0.2920
VH * V6	1	4.88281250	4.88281250	0.04	0.8353
VD 7 V6	1	56.44531250	56.44531250	0.50	0.4800

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1,		-3.20312500 -7.18750000	1.32480534 1.32480534	0.0174 0.0001
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-3.98437500 -6.40625000	1.32480534 1.32480534	0.0033 0.0001
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1	-3.5937500 -2.8125000 -4.3750000 -10.0000000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.0579 0.1364 0.0215 0.0001
٧3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5,56250000 -4,82812500	1.32480534 1.32480534	0.0001 0.0004

V1	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-4.59375000 -1.81250000 -6.53125000 -7.84375000	1.87355767 1.87355767 1.87355767 1.87355767	0.0159 0.3356 0.0007 0.0001
V2	V3	Y LISMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1 -1 -1	1 - 1 - 1 - 1	-4.65625000 -3.31250000 -6.46875000 -6.34375000	1.87355767 1.87355767 1.87355767 1.87355767	0.0146 0.0800 0.0008 0.0010
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-2.64062500 -7.75000000	1.32480534 1.32480534	0.0489 0.0001
V1	٧4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 1 1	-0.43750000 -5.96875000 -4.84375000 -9.53125000	1.87355767 1.87355767 1.87355767 1.87355767	0.8158 0.0019 0.0111 0.0001

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-1.56250000 -6.40625000 -3.71875000 -9.09375000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.4062 0.0009 0.0498 0.0001
٤V	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 1 -1 -1	-1.62500000 -9.50000000 -3.65625000 -6.00000000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.3878 0.0001 0.0537 0.0018
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5.14062500 -5.25000000	1.32480534 1.32480534	0.0002 0.0001
Vl	ν5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1 - 1 - 1	1 - 1 - 1	-4.59375000 -1.81250000 -5.68750000 -8.68750000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.0159 0.3356 0.0030 0.0001

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1 - 1	-3.09375000 -4.87500000 -7.18750000 -5.62500000	1.87355767 1.87355767 1.87355767 1.87355767	0.1017 0.0106 0.0002 0.0034
٧3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-5.03125000 -6.09375000 -5.25000000 -4.40625000	1.87355767 1.87355767 1.87355767 1.87355767	0.0084 0.0015 0.0061 0.0206
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-3,75000000 -1,53125000 -6,53125000 -8,96875000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.0480 0.4156 0.0007 0.0001
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-3.40625000 -6.98437500	1.32480534 1.32480534	0.0116 0.0001

V1	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-1.75000000 -4.65625000 -5.06250000 -9.31250000	1.87355767 1.87355767 1.87355767 1.87355767	0.3525 0.0146 0.0081 0.0001
V2	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.87500000 -6.09375000 -4.93750000 -7.8750000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.3193 0.0015 0.0097 0.0001
V3	VG	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-2.78125000 -8.34375000 -4.03125000 -5.62500000	1.87355767 1.87355767 1.87355767 1.87355767	0.1407 0.0001 0.0338 0.0034
V4	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1] - 1	-0.65625000 4.62500000 -6.15625000 -9.34375000	1.87355767 1.87355767 1.87355767 1.87355767 1.87355767	0.7269 0.0152 0.0014 0.0001

V 5	V6	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-2.68750000	1.87355767	0.1545
1	- 1	-7.59375000	1.87355767	0.0001
- 1	1	-4.12500000	1.87355767	0.0299
-1	- 1	-6,37500000	1,87355767	0.0010

General Linear Models Procedure Dependent Variable : Y

* denotes significance

Source Model Error Corrected	Total	DF Sum of 24 1512 103 8970 127 10482 R-Square 0.144297	Squares 2.65625000 0.31250000 2.96875000 C.V. -417.6660	Меа 63. 87.	an Square .02734375 .09041262 Root MSE 9.33222442	F Value 0.72 Y Ma 2	Pr > F 0.8169 ean 3437500
Source	DF	Type III SS	S Mean	Square	F Value	Pr	> F
R	3	467 90629	5000 15	5 96875000	1 70	0 1	576
V7	1	72.0000		2 00000000	T 7 2	1.0	550
V8	1	52.53125	5000 5	2.00000000	0.03	0.3	201
V9	1	4.5000	0000	4 50000000	0.00	0.4	206
V10	1	210.12500	0000 21	0 12500000	2 41	0.0	200
V11	1	0.78125	5000	0.78125000	0 01	0,1	234 247
V7 * V11	1	36.12500	0000 3	12500000	0.41	0.5	210
V8 * V11	1	34.03125	5000 3	34.03125000	0 39	0,5	222
V9 * V11	1	6.12500	0000	6.12500000	0.07	0.5	914
V10 * V11	1	66.12500	2000 e	6.12500000	0.76	0.3	856
V12	1	195.03125	5000 19	5.03125000	2.24	0.1	376
V11 * V12	1	0.78125	5000	0.78125000	0.01	0.9	247
V13	1	0.28125	5000	0.28125000	0.00	0.9	548
V7 * V13	1	3.12500	0000	3.12500000	0.04	0.8	501
V8 * V13	1	30,03125	5000 3	10.03125000	0.34	0.5	583
V9 * V13	1	1,12500	000	1.12500000	0.01	0.9	097
V10 * V13	1	276.12500	000 27	6.12500000	3.17	0.0	779
V11 * V13	1	7.03129	5000	7.03125000	0.08	0.7	769
V12 * V13	Ţ	38.28125	5000 3	8.28125000	0.44	0.5	088
V14	1	5,28125	5000	5.28125000	0.06	0.8	060
V11 * V14	1	3.78125	5000	3.78125000	0.04	0.8	354
V13 * V14	1	1.53125	5000	1.53125000	0.02	0.8	948

General Linear Models Procedure Least Square Means

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.48437500	1.6652805	0.2061
- 1	-2.98437500	1.6652805	0.0120
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1,59375000	1.6652805	0.1748
- 1	-2.87500000	1.6652805	0.0154
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-2.04687500	1.6652805	0.0823
- 1	-2.42187500	1.6652805	0.0404
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-3.51562500	1.6652805	0.0032
- 1	-0.95312500	1.6652805	0.4158

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V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-2.15625000 -2.31250000	1.6652805 1.6652805	0.0674 0.0501
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.93750000 -1.03125000 -2.37500000 -3.59375000	1.64971979 1.64971979 1.64971979 1.64971979 1.64971979	0.2429 0.5333 0.1530 0.0317
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.00000000 -2.18750000 -3.31250000 -2.43750000	1.64971979 1.64971979 1.64971979 1.64971979 1.64971979	0.5457 0.1878 0.0473 0.1426
V 9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-2.18750000 -1.90625000 -2.12500000 -2.71875000	1.64971979 1.64971979 1.64971979 1.64971979	0.1878 0.2506 0.2006 0.1024

V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 -1	1 - 1 - 1	-4.15625000 -2.87500000 -0.15625000 -1.75000000	1.64971979 1.64971979 1.64971979 1.64971979	0.0133 0.0844 0.9247 0.2913
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		~1.00000000 -3.46875000	1.6652805 1.6652805	0.3933 0.0037
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.00000000 -3.31250000 -1.00000000 -3.62500000	1.64971979 1.64971979 1.64971979 1.64971979	0.5457 0.0473 0.5457 0.0302
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-2.18750000 -2.28125000	1.6652805 1.6652805	0.0636 0.0532

V'7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN - O
1	1	-1.28125000	1.64971979	0.4391
1	- 1	-1.68750000	1.64971979	0.3088
- 1	1	-3.09375000	1.64971979	0.0636
- 1	- 1	-2.87500000	1.64971979	0.0844
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-1.06250000	1.64971979	0.5210
1	- 1	-2.12500000	1.64971979	0.2006
- 1	1	-3,31250000	1.64971979	0.0473
- 1	- 1	-2.43750000	1.64971979	0.1426
V 9	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: $LSMEAN = 0$
1	1	-1.90625000	1.64971979	0.2506
1	- 1	-2.18750000	1.64971979	0.1878
- 1	1	-2.46875000	1.64971979	0.1376
- 1	-1	-2.37500000	1.64971979	0.1530
V1 0	V13	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	-2.00000000	1.64971979	0.2282
1	- 1	-5.03125000	1.64971979	0.0029
- 1	1	-2.37500000	1.64971979	0.1530
~ 1	- 1	-0.46875000	1.64971979	0.7769

V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	~2.34375000 -1.96875000 -2.03125000 -2.59375000	1.64971979 1.64971979 1.64971979 1.64971979 1.64971979	0.1584 0.2355 0.2210 0.1190
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1 - 1	1 - 1 1 - 1	-1.50000000 -0.50000000 -2.87500000 -4.06250000	1.64971979 1.64971979 1.64971979 1.64971979	0.3653 0.7624 0.0844 0.0155
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-2.03125000 -2.43750000	1,6652805 1,6652805	0.0846 0.0391
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-1.78125000 -2.53125000 -2.28125000 -2.34375000	1.64971979 1.64971979 1.64971979 1.64971979	0.2828 0.1280 0.1697 0.1584

V13	V14	Y	Std Err	Pr > ITI HO, ISMEAN - 0
		LIDMERIA	номени	$\mathbf{n}\mathbf{O}: \mathbf{DSMEAN} = \mathbf{O}$
1	1	-2.09375000	1.64971979	0.2072
1	-1	-2.28125000	1,64971979	0.1697
- 1	1	-1.96875000	1.64971979	0.2355
- 1.	- 1	-2,59375000	1.64971979	0.1190

General L:	inear Mode	els Procedure		*	denotes sign	ificance
Dependent	Variable	: Y			denotes sign	TTTCance
Source		DF Sum	of Squares	Mean Square	F Value	Pr < F
Model		24 18	58.43750000	77.43489583	2 03	0 0078
Error		103 39	29.06250000	38.14623786	2,05	0.0070
Corrected	Total	127 57	87.5000000			
		R-Square	C.V.	Root MSE	Y Mean	
		0.321112	-131.7603	6.17626407	-4.6875	0000
Source	DF	Type III	SS	Mean Square	F Value	Pr > F
R	3	616.812500	00	205.60416667	5.39	0 0017
V1	1	225.781250	00	225.78125000	5.92	0 0167 *
V2	1	75.031250	00	75.03125000	1.97	0 1638
V1 * V2	1	60.500000	00	60.5000000	1.59	0.2107
V3	1	38.281250	00	38,28125000	1.00	0.3188
V1 * V3	1	60.500000	00	60.5000000	1,59	0.2107
V2 * V3	1	4.50000	00	4.5000000	0.12	0.7319
V4	1	242.00000	00	242.00000000	6.34	0.0133 *
V1 * V4	1	2.531250	00	2.53125000	0.07	0.7972
V2 * V4	1	3.781250	00	3.78125000	0.10	0.7535
V3 * V4	1	87.781250	00	87.78125000	2.30	0.1323
V5	1	5.281250	00	5.28125000	0.14	0,7106
V1 * V5	1	91.125000	00	91.12500000	2.39	0.1253
V2 * V5	1	6.125000	00	6.12500000	0.16	0.6895
V3 * V5	1	24.500000	00	24.5000000	0.64	0.4247
V4 * V5	1	7.031250	00	7.03125000	0.18	0.6686
V6	1	128.000000	00	128.0000000	3.36	0.0699 *
V1 * V6	1	9.031250	00	9.03125000	0.24	0.6276
V2 * V6	1	22.781250	00	22.78125000	0.60	0.4414
V3 * V6	1	132.031250	00	132.03125000	3.46	0.0657 *
V4 * V6	1	12.500000	00	12.5000000	0.33	0.5683
V5 * V6	1	2.531250	00	2.53125000	0.07	0.7972

Vl		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-3.35937500 -6.01562500	0.77203301 0.77203301	0.0001 0.0001
V 2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		-3.92187500 -5.45312500	0.77203301 0.77203301	0.0001 0.0001
Vı	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 · 1 · 1	1 - 1 - 1 - 1	-3.28125000 -3.43750000 -4.56250000 -7.46875000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0033 0.0021 0.0001 0.0001
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5.23437500 -4.14062500	0.77203301 0.77203301	0.0001 0.0001

Vl	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-4.59375000 -2.12500000 -5.87500000 -6.15625000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0001 0.0543 0.0001 0.0001
V2	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1	1 -1 1 -1	-4.65625000 -3.18750000 -5.81250000 -5.09375000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0001 0.0043 0.0001 0.0001
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1		-3.31250000 -6.06250000	0.77203301 0.77203301	0.0001 0.0001
V1	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.84375000 -4.87500000 -4.78125000 -7.25000000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0943 0.0001 0.0001 0.0001

V 2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-2.71875000 -5.12500000 -3.90625000 -7.00000000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0144 0.0001 0.0005 0.0001
٧3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-3.03125000 -7.43750000 -3.59375000 -4.68750000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0065 0.0001 0.0014 0.0001
V5		Y LISMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-4.48437500 -4.89062500	0.77203301 0.77203301	0.0001 0.0001
LΛ	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 ~ 1	1 ~ 1 1 - 1	~4.00000000 ~2.71875000 ~4.96875000 ~7.06250000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0004 0.0144 0.0001 0.0001

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 1 - 1	-3.50000000 -4.34375000 -5.46875000 -5.43750000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0018 0.0001 0.0001 0.0001
V3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-4.59375000 -5.87500000 -4.37500000 -3.09625000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0001 0.0001 0.0001 0.0005
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1 - 1	-3.34375000 -3.28125000 -5.62500000 -6.50000000	1.09181955 1.09181955 1.09181955 1.09181955	0.0028 0.0033 0.0001 0.0001
٧G		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1		-3.68750000 -5.68750000	0.77203301 0.77203301	0.0001 0.0001

General Linear Models Procedure Least Square Means

V1	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1 <u>1</u> 1	1 - 1 - 1	-2.62500000 -4.09375000 -4.75000000 -7.28125000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0180 0.0003 0.0001 0.0001
Λ5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-2.50005000 -5.34375000 -4.87500000 -6.03125000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0241 0.0001 0.0001 0.0001
٧3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	-3.21875000 -7.25000000 -4.15625000 -4.12500000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0040 0.0001 0.0002 0.0003
V4	V 6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 · 1 · 1	1 1 1 1 - 1	-2.00000000 -4.62500000 -5.37500000 -6.75000000	1.09181955 1.09181955 1.09181955 1.09181955 1.09181955	0.0699 0.0001 0.0001 0.0001

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V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-3.34375000	1.09181955	0.0028
1	- 1	-5.62500000	1.09181955	0.0001
· 1	1	-4.03125000	1,09181955	0.0004
- 1	- 1	-5.75000000	1.09181955	0.0001

General Lin Dependent V	ear Mod ariable	els Procedure : Y	* dei	notes signif	ificance		
Source Model Error Corrected T	otal	DF Sum 24 5 103 29 127 35	of Square 583.3750000 943.742187 527.117187	s Meai 00 24.1 50 28.9	n Square 30729167 58002124	F Value 0.85	Pr > F 0.6655
		R-Square 0.165397	C. -31	V. 5.3418	Root MSE 5.34602855	Y Mean -1.695312	250
Source	DF	Type 111	SS	Mean Square	F Value	Pr >	> F
R	3	55,77	343750	18.5911458	3 0.65	0.58	344
V7	1	11.883	281.250	11.88281250	0 0.42	0.52	205
V8	1	9.57	031250	9.5703125	0 0.33	0.56	541
V9	1	0.94	531250	0.94531250	0.03	0.85	560
V10	1	103.32	031250	103.3203125	0 3.62	0.06	501 *
V11.	1	20.32	031250	20.3203125	0 0.71	0.40)11
V7 * V11	1	21.94	531250	21,9453125	0 0.77	0.38	329
V8 * V11	1	7.50	781250	7.5078125	0 0.26	0.60)94
V9 * V11	1	4.13	281250	4.1328125	0 0.14	0.70)45
V10 * V11	1	14.44	531250	14.4453125	0 0.51	0.47	787
V12	1	106.94	531250	106.9453125	0 3.74	0.05	558 *
V11 * V12	1	1.75	781250	1.7578125	0 0.06	0.80	046
V13	1	0.94	531250	0.9453125	0.03	0.85	560
V7 * V13].	1.75	781250	1.7578125	0 0.06	0.80	046
V8 * V13	1	5.69	531250	5.6953125	0.20	0.65	562
V9 * V13	1	10.69	531250	10.6953125	0 0.37	0.54	121
V10 * V13	1.	138.19	531250	138.1953125	0 4.84	0.03	301 *
V11 * V13	1	15.820	031250	15.8203125	0 0.55	0.45	586
V12 * V13	1	43.94	531250	43.9453125	0 1.54	0.21	178
V14	1	2.25	781250	2.2578125	0.08	0.77	792
V11 * V14	1.	0.63	281250	0.6328125	0 0.02	0.88	320
V13 * V14	1	4.882	281250	4.88281250	0.17	0.68	302

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.39062500	0.66825357	0.0399
1	-2.98437500	0.66825357	0.0035
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.42187500	0.66825357	0.0357
- 1	-1.96875000	0.66825357	0.0040
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1.	-1.78125000	0.66825357	0.0089
- 1	-1.60937500	0.66825357	0.0178
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-2,59375000	0.66825357	0.0002
- 1	-0,79687500	0.66825357	0.2358

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-1.29687500 -2.09375000	0.66825357 0.66825357	0.0550 0.0023
V 7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-1.40625000 -1.37500000 -1.18750000 -2.81250000	0.94505326 0.94505326 0.94505326 0.94505326 0.94505326	0.1398 0.1487 0.2118 0.0036
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 ~ 1 1 - 1	-0,78125000 -2,06250000 -1,81250000 -2,12500000	0.94505326 0.94505326 0.94505326 0.94505326 0.94505326	0.4103 0.0314 0.0579 0.0267
V9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.56250000 -2.00000000 -1.03125000 -2.18750000	0.94505326 0.94505326 0.94505326 0.94505326	0.1013 0.0367 0.2777 0.0226

General Linear Models Procedure Least Square Means

V10	V11	Y LSMEAN	SLd Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 - 1 - 1	~2.53125000 -2.65625000 -0.06250000 -1.53125000	0.94505326 0.94505326 0.94505326 0.94505326	0.0086 0.0059 0.9474 0.1082
V1.2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.78125000 -2.60937500	0.66825357 0.66825357	0.2451 0.0002
V11	V12	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.5000)000 -2.09375000 -1.06250000 -3.12500000	0.94505326 0.94505326 0.94505326 0.94505326	0.5979 0.0289 0.2635 0.0013
V13		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-1.60937500 -1.78125000	0.66825357 0.66825357	0.0178 0.0089

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V7	V1.3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-1.18750000 -1.59375000 -2.03125000 -1.96875000	0.94505326 0.94505326 0.94505326 0.94505326 0.94505326	0.2118 0.0947 0.0339 0.0397
٧8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	-1.12500000 -1.71875000 -2.09375000 -1.84375000	0.94505326 0.94505326 0.94505326 0.94505326 0.94505326	0.2366 0.0719 0.0289 0.0538
V9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-1.40625000 -2.15625000 -1.81250000 -1.40625000	0.94505326 0.94505326 0.94505326 0.94505326 0.94505326	0.1398 0.0246 0.0579 0.1398
V 10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.46875000 -3.18750000 -1.75000000 0.15625000	0.94505326 0.94505326 0.94505326 0.94505326	0.1232 0.0002 0.0669 0.8690

V11.	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1.	-1.56250000	0.94505326	0.1013
1	-1	-1.03125000	0.94505326	0.2777
-1	1	-1.65625000	0.94505326	0.0827
-1	-1	-2.53125000	0.94505326	0.0086
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1).	-1.28125000	0.94505326	0.1781
1	- 1	-0.28125000	0.94505326	0.7666
- 1	1	-1.93750000	0.94505326	0.0429
- 1	- 1	-3.28125000	0.94505326	0.0008
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-1.56250000	0.66825357	0.0213
- 1		1.82812500	0.66825357	0.0073
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	~1.09375000	0.94505326	0.2498
- 1	-1	~1.50000000	0.94505326	0.1155
- 1	1	-2.03125000	0.94505326	0.0339
1	-1	-2.15625000	0.94505326	0.0246

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-1.28125000	0.94505326	0.1781
1	~1	-1.93750000	0.94505326	0.0429
- 1	1	-1,84375000	0.94505326	0.0538
- 1	~ 1	-1.71875000	0.94505326	0.0719

General Lin Dependent V	lear Mod Mariable	els Procedur : Y	re	*	denotes significance	
Source Model Error Corrected 1	`otal	DF 24 103 127	Sum of Squares 4.89423750 15.51191797 21.40615547	Mean Square 0.203926563 0.16030988	F Value 1.27	Pr > F 0.2027
		R-Square 0.228637	C.V. -70.04176	Root MSE 0.40038717	Y Mean -0.5716	4062
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F
R	3	1.147	38359	0.38246120	2.39	0.0734
V1	1	0.452	43828	0.45243828	2.82	0.0960
V2	1	0.047	766328	0.04766328	0.30	0.5867
V1 * V2	1	0.012	260078	0.01260078	0.08	0.7798
V3	1	0.160)31953	0.16031953	1.00	0.3196
V1 * V3	1.	0.161	.73828	0.16173828	1.01	0.3175
V2 * V3	1.	0.090)84453	0.09084453	0.57	0.4533
V4	1	1.564	123828	1.56423828	9.76	0.0023 *
V1 * V4	1	0,057	737578	0.05737578	0.36	0.5510
V2 * V4	1	0.017	734453	0.01734453	0.11	0.7429
V3 * V4	1	0.123	313203	0.12313203	0.77	0.3828
V5	1	0.062	256953	0.06256953	0.39	0.5335
V1 * V5	1	0.112	21953	0.11221953	0,70	0.4047
V2 * V5	1	0.007	735078	0.00735078	0.05	0.8309
V3 * V5	1	0.015	509453	0.01509453	0.09	0.7596
V4 * V5	1	0.119	943828	0.11943828	0.75	0.3901
V6	1	0.483	88203	0.48388203	3.02	0.0853
V1 * V6	1	0.025	03203	0.02503203	0.16	0.6935
V2 * V6	1	0.145	12578	0.14512578	0.91	0.3436
V3 * V6	1	0,037	46953	0.03746953	0.23	0.6298
V4 * V6	1	0.000	17578	0.00017578	0.00	0.9736
V5 * V6	1	0.050	80078	0.05080078	0.32	0.5747

CALCIUM : POST - PRE

V1.		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-0.51218750 -0.63109375	0.05004840 0.05004840	0.0001 0.0001
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.55234375 0.59093750	0.05004840 0.05004840	0.0001 0.0001
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.50281250 -0.52156250 0.60187500 -0.66031250	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
¥3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		0,60703125 -0,53625000	0.05004 840 0.05004840	0.0001 0.0001
General Linear Models Procedure Least Square Means

V1	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-0.58312500 -0.44125000 -0.63093750 -0.63125000	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V2	Δ3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.61437500 -0.49031250 -0.59968750 -0.58218750	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V4		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.68218750 -0.46109375	0.05004840 0.05004840	0.0001 0.0001
V 1.	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.60156250 -0.42281250 -0.76281250 -0.49937500	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001 0.0001

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V2	٧4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1] - 1 1 - 1	-0.65125000 -0.45343750 -0.71312500 -0.46875000	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-0.68656250 -0.52750000 -0.67781250 -0.39468750	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-0.54953125 -0.59375000	0.05004840 0.05004840	0.0001 0.0001
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 1 1 - 1	-0.51968750 -0.50468750 -0.57937500 -0.68281250	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001

General Linear Models Procedure Least Square Means

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 -1 1 ~1	-0.53781250 -0.56687500 -0.56125000 -0.62062500	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
٧3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-0.57406250 -0.64000000 -0.52500000 -0.54750000	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.69062500 ~0.67375000 -0.40843750 -0.51375000	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.51015625 -0.63312500	0.05004840 0.05004840	0.0001 0.0001

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V1	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 	-0.46468750 -0.55968750 -0.55562500 -0.70656250	0.07077912 0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V2	V6	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.45718750 -0.64750000 -0.56312500 -0.61875000	0.07077912 0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-0.52843750 -0.68562500 -0.49187500 -0.58062500	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001
V4	٧6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.62187500 -0.74250000 -0.39843750 -0.52375000	0.07077912 0.07077912 0.07077912 0.07077912	0.0001 0.0001 0.0001 0.0001

V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.46812500	0.07077912	0,0001
1	- 1	-0,63093750	0.07077912	0.0001
- 1	1	-0,55218750	0.07077912	0,0001
- 1	- 1	-0,63531250	0.07077912	0.0001

General Li: Dependent	near Mod Variable	els Procedur : Y	e			* den	otes signif	ficance
Source Model Error Corrected '	Total	DF 24 103 127	Sum of Sc 1,207768 5,286686 6,4944554	quares 75 72 47	Mean 0.05 0.05	Square 032370 132706	F Value 0.98	Pr > F 0.4978
		R-Square 0.185969		C.V. -3411.648		Root MSE 0.22655475	Y Mean -0.00664(062
Source	DF	Туре	III SS	Mean Squ	uare	F Value	Pr :	> F
R	3	0	.17185859	0.05	5728620	1.12	0.34	461
V7	1	0	.00009453	0.00	0009453	0.00	0.96	559
V8	1	0	.01220703	0.03	1220703	0.24	0.62	268
V9	1	0	.00861328	0.00	0861328	0.17	0.68	829
V10	1	0	.16747578	0.10	6747578	3,26	0.0	738
V11	1	0	.08150703	0.0	8150703	1,59	0.23	105
V7 * V11	1	0	.04843828	0.04	4843828	0.94	0.33	336
V8 * V11	1	0	.00085078	0.0	0085078	0.02	0,89	978
V9 * V11	1	0	.00439453	0.00	0439453	0.09	0.7	704
V10 * V11	1	0	.09845703	0.0	9845703	1.92	0.16	690
V12	1	0	.19453203	0.19	9453203	3,79	0.0	543 *
V11 * V12	1	0	.01143828	0.03	1143828	0.22	0.63	379
V13	1	0	.01106328	0.0	1106328	0.22	0.64	434
V7 * V13	1	0	.04388203	0.04	4388203	0.85	0.3	573
V8 * V13	1	0	.03219453	0.03	3219453	0.63	0.43	302
V9 * V13	1	0	.03347578	0,03	3347578	0.65	0.42	212
V10 * V13	Ţ	0	.21043828	0.23	1043828	4.10	0.04	455 *
V11 * V13	Ĺ	0	.01033203	0.03	1033203	0.20	0.65	546
V12 * V13	1	0	.06345703	0.00	5345703	1.24	0.20	688
V14	1	0	.00017578	0.00	0017578	0.00	0.95	534
V11 * V14	1	0	.00203203	0.00	0203203	0.04	0.84	427
V13 * V14	1	0	.00085078	0.00	0085078	0.02	0.89	978

General Linear Models Procedure Least Square Means

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-0.00578125	0.02831934	0.8386
- 1.	-0.00750000	0.02831934	0.7917
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	0.00312500	0.02831934	0.9123
- 1	-0.01640625	0.02831934	0.5636
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	0.00156250	0.02831934	0.9561
- 1	-0.01484375	0.02831934	0.6013
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1 - 1	-0.04281250 0.02953125	0.66825357	0.1337

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		0.01859375 -0.03187500	0.02831934 0.02831934	0.5129 0.2630
V7	V1 1.	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. 1 - 1 - 1	1 - 1 1 1	-0.00000000 -0.01156250 0.03718750 -0.05118750	0.04004960 0.04004960 0.04004960 0.04004960 0.04004960	1.0000 0.7734 0.3553 0.1955
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.03093750 ~0.02468750 0.00625000 -0.03906250	0.04004960 0.04004960 0.04004960 0.04004960 0.04004960	0.4416 0.5390 0.8763 0.3317
V9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	0.02093750 -0.01781250 0.01625000 -0.04593750	0.04004960 0.04004960 0.04004960 0.04004960	0.6022 0.6574 0.6858 0.2540

V1.0	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.04531250	0.04004960	0.2605
1	- 1	-0.04031250	0.04004960	0.3165
-1	1	0.08250000	0.04004960	0.0419
-1	- 1	-0.02343750	0.04004960	0.5597
V 12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		0.03234375	0.02831934	0.2561
-1		-0.04562500	0.02831934	0.1102
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	0.04812500	0.04004960	0.2323
1	- 1	-0.01093750	0.04004960	0.7853
- 1	1	0.01656250	0.04004960	0.6801
- 1	- 1	-0.08031250	0.04004960	0.0476
V13		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.01593750	0.02831934	0.5748
- 1		0.00265625	0.02831934	0.9255

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.00343750 -0.01500000 -0.03531250 0.02031250	0.04004960 0.04004960 0.04004960 0.04004960	0.9318 0.7088 0.3800 0.6131
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	0.00968750 -0.00343750 -0.04156250 0.00875000	0.04004960 0.04004960 0.04004960 0.04004960	0.8093 0.9318 0.3018 0.8275
V9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	0.00843750 -0.00531250 -0.04031250 0.01062500	0.04004960 0.04004960 0.04004960 0.04004960 0.04004960	0.8336 0.8947 0.3165 0.7913
V 10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1 - 1	-0.01156250 -0.07406250 -0.02031250 0.07937500	0.04004960 0.04004960 0.04004960 0.04004960	0.7734 0.0673 0.6131 0.0502

V11.	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	0.00031250 0.03687500 -0.03218750 -0.03156250	0.04004960 0.04004960 0.04004960 0.04004960	0.9938 0.3593 0.4234 0.4325
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	0.04531250 0.01937500 -0.07718750 -0.01406250	0.04004960 0.04004960 0.04004960 0.04004960 0.04004960	0.2605 0.6296 0.0567 0.7262
V14		Y IISMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-0.00546875 -0.00781250	0.02831934 0.02831934	0.8473 0.7832
V11	V14	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	0.02375000 0.01343750 ~0.03468750 ~0.02906250	0.04004960 0.04004960 0.04004960 0.04004960	0.5545 0.7379 0.3884 0.4697

V13	V1.4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.01218750	0.04004960	0.7615
1	- 1	-0.01968750	0.04004960	0.6241
- 1	1	0.00125000	0.04004960	0.9752
- 1	- 1.	0.00406250	0.04004960	0.9194

General Linear Models Procedure Dependent Variable : Y				* denotes significance			
Source Model Error Corrected	Total	DF 24 103 127	Sum of Squares 5792.00000000 18144.21875000 23936 21875000	Mean Square 241.33333333 176.15746359	F Value 1.37	Pr > F 0.1411	
		R-Square 0.241976	C.V. 469.3015	Root MSE 13.27243247	Y Mean 2.82812	500	
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F	
R	3	326	.78125000	108,92708333	0.62	0 6047	
Vl	1	38	.28125000	38.28125000	0.22	0 6421	
V 2	1	0	.12500000	0.12500000	0.00	0.0421	
V1. * V2	1	420	.50000000	420.5000000	2.39	0.1254	
V3	1	26	.28125000	26.28125000	0.15	0.7001	
V1 * V3	1	712	.53125000	712.53125000	4.04	0 0469 *	
V2 * V3	1	45	.12500000	45,12500000	0.26	0.6139	
V4	1	657	.03125000	657.03125000	3.73	0.0562 *	
V1 * V4	1	47	.53125000	47.53125000	0.27	0.6046	
V2 * V4	1	10	.12500000	10.12500000	0.06	0.8110	
V3 * V4	1	94	.53125000	94.53125000	0.54	0.4655	
ν5	1	294	.03125000	294.03125000	1.67	0,1993	
Vl * V5	1	13	.78125000	13.78125000	0.08	0.7803	
V2 * V5	1	36	.12500000	36.12500000	0.21	0.6516	
V3 * V5	1	1023	.78125000	1023.78125000	5.81	0.0177 *	
V4 * V5	1	830	.28125000	830.28125000	4.71	0.0322 *	
V6	1	338	.0000000	338.0000000	1.92	0.1690	
V1 * V6	1	153	.12500000	153.12500000	0.87	0 3533	
V2 * V6	1	427	.78125000	427.78125000	2.43	0 1222	
V3 * V6	1	50	.0000000	50.0000000	0.28	0.5953	
V4 * V6	1	36	.12500000	36.12500000	0.21	0.6516	
V5 * V6	1	210	.12500000	210.12500000	1.19	0.2773	

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		2.28125000 3.37500000	1.65905406 1.65905406	0.1721 0.0445
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		2.79687500 2.85937500	1.65905406 1.65905406	0.0949 0.0878
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1] -1	0.43750000 4.12500000 5.15625000 1.59375000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.8524 0.0817 0.0302 0.4985
Δ3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		3.28125000 2.37500000	1.65905406 1.65905406	0.0506 0.1553

V1	¥3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 - 1	5.09375000 -0.53125000 1.46875000 5.28125000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.0322 0.8213 0.5327 0.0265
V 2	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	2.65625000 2.93750000 3.90625000 1.81250000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.2602 0.2134 0.0990 0.4416
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		0.56250000 5.09375000	1.65905406 1.65905406	0.7353 0.0027
V1	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.62500000 3.93750000 0.50000000 6.25000000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.7905 0.0963 0.8317 0.0090

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.81250000 4.78125000 0.31250000 5.40625000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.7298 0.0441 0.8943 0.0232
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	1.87500000 4.68750000 -0.75000000 5.50000000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.4260 0.0484 0.7499 0.0210
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1		1.31250000 4.3 4 375000	1.65905406 1.65905406	0.4307 0.0102
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	1.09375000 3.46875000 1.53125000 5.21875000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.6421 0.1423 0.5154 0.0283

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	0.75000000 4.84375000 1.87500000 3.84375000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.7499 0.0415 0.4260 0.1044
V3	V 5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	4.59375000 1.96875000 -1.96875000 6.71875000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.0529 0.4034 0.4034 0.0051
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	1.59375000 -0.46875000 1.03125000 9.15625000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.4985 0.8420 0.6612 0.0002
V 6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		4.45312500 1.20312500	1.65905406 1.65905406	0.0085 0.4700

V1.	V 6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 ~ 1 1 - 1	2.81250000 1.75000000 6.09375000 0.65625000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.2334 0.4574 0.0108 0.7803
V2	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	6.25000000 -0.65625000 2.65625000 3.06250000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.0090 0.7803 0.2602 0.1947
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1	1 - 1 1 - 1	4.28125000 2.28125000 4.62500000 0.12500000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.0709 0.3332 0.0514 0.9576
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	2.71875000 -1.59375000 6.18750000 4.00000000	2.34625675 2.34625675 2.34625675 2.34625675 2.34625675	0.2492 0.4985 0.0097 0.0921

V5	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	4.21875000	2.34625675	0.0751
1	- 1	-1.59375000	2.34625675	0.4985
- 1	1	4.68750000	2,34625675	0.0484
- 1	- 1	4.00000000	2.34625675	0.0912

General Linear Models Procedure Dependent Variable : Y

-1.27343750

*

Source Model Error Corrected Toral	DF 24 103 127	Sum of Squares 847.56250000 2915.86718750 3763.42968750	Mean Square 35.31510417 28.30939017	F Value 1.25	Pr > F 0.2211
	R-Square	C.V.	Root MSE	Y Mea	n
	0.225210	-417.8185	5,32065693	-1.273	43750

Sourd	ce	DF	Type III SS	Mean Square	F Value	Pr > F
R		3	60.27343750	20.09114583	0 71	0 5484
V7		1	1.32031250	1.32031250	0 05	0.2404
V8		1	7,50781250	7.50781250	0.27	0.6077
V9		1.	15.82031250	15.82031250	0 56	0.4564
V10		1	7.50781250	7.50781250	0.27	0.4004
V11		1	0.63281250	0.63281250	0.02	0.8814
י 77	* V11	1	5.69531250	5.69531250	0.20	0.6547
V8 -	* V11	1	48.75781250	48,75781250	1.72	0.1923
V9 -	* V11	1	53.82031250	53.82031250	1.90	0.1709
V10 -	* V11	1	2.82031250	2.82031250	0.10	0 7529
V12		1.	168.82031250	163.82031250	5,96	0.0163 *
V11 :	* V12	1.	6.57031250	6,57031250	0.23	0.6310
V13		1	17.25781250	17,25781250	0.61	0 4367
V7 1	* V13	1	11.88281250	11.88281250	0 42	0.5185
V8 :	* V13	1	146.63281250	146.63281250	5 18	0.0249 *
V9 3	* V13	1	73.50781250	73.50781250	2 60	0.0219
V10 v	* V13	1	8,50781250	8 50781250	0 30	0.5847
V11 v	* V13	1	27.19531250	27 19531250	0.96	0.2027
V12 +	* V13	1	37 19531250	37 19531250	1 31	0.3293
V14		- 1	118 19531250	118 19531250	1 1 9	0.2343
V11 /	* V14		25 38281250	110,120010EV	4,10	0,0430 *
V13 /	• V14	1	2.25781250	2.25781250	0.08	0.3459

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.37500000	0.66508212	0.0412
- 1	-1.17187500	0.66508212	0.0812
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.03125000	0.66508212	0.1241
- 1.	-1.51562500	0.66508212	0.0247
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.62500000	0.66508212	0.0163
- 1	-0.92187500	0.66508212	0.1687
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-1.51562500	0.66508212	0.0247
1	-1.03125000	0.66508212	0.1241

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-1.34375000 -1.20312500	0.66508212 0.66508212	0.0459 0.0734
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-1.65625000 -1.09375000 -1.03125000 -1.31250000	0.94056815 0.94056815 0.94056815 0.94056815	0.0812 0.2476 0.2755 0.1659
V8	V11	Y LSMEAN	Sud Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-1.71875000 -0.34375000 -0.96875000 -2.06250000	0.94056815 0.94056815 0.94056815 0.94056815 0.94056815	0.0705 0.7155 0.3054 0.0306
V 9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 1	1 - 1 - 1 - 1	-2.34375000 -0.90625000 -0.34375000 -1.50000000	0.94056815 0.94056815 0.94056815 0.94056815	0.0143 0.3375 0.7155 0.1138

V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	-1.43750000	0.94056815	0.1295
-1	-1.59375000	0.94056815	0.0932
1	-1.25000000	0.94056815	0,1868
- 1	-0.81250000	0.94056815	0.3897
	V11 -1 1 -1	V11 Y LSMEAN 1 -1.43750000 -1 -1.59375000 1 -1.25000000 -1 -0.81250000	V11 Y Std Err LSMEAN LSMEAN 1 -1.43750000 0.94056815 -1 -1.59375000 0.94056815 1 -1.25000000 0.94056815 -1 -0.81250000 0.94056815

V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.12500000 -2.42187500	0.6650 821 2 0.66508212	0.8513 0.0004
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	0.03125000 -2.71875000 -0.28125000 -2.12500000	0.94056815 0.94056815 0.94056815 0.94056815 0.94056815	0.9736 0.0047 0.7655 0.0260
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.90625000 -1.64062500	0.66508212 0.66508212	0.1760 0.0153

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 -1 1 -1	-1.31250000 -1.43750000 -0.50000000 -1.84375000	0.94056815 0.94056815 0.94056815 0.94056815 0.94056815	0.1659 0.1295 0.5962 0.0527
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	0.40625000 -2.46875000 -2.21875000 -0.81250000	0.94056815 0.94056815 0.94056815 0.94056815	0.6667 0.0100 0.0202 0.3897
V9	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 -1 1 -1	-0.50000000 -2.75000000 -1.31250000 -0.53125000	0.94056815 0.94056815 0.94056815 0.94056815	0.5962 0.0043 0.1659 0.5734
V 10	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.40625000 -1.62500000 -0.40625000 -1.65625000	0.94056815 0.94056815 0.94056815 0.94056815 0.94056815	0.1379 0.0870 0.6667 0.0812

V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 1 1	-1.43750000 -1.25000000 -0.37500000 -2.03125000	0.94056815 0.94056815 0.94056815 0.94056815	0.1295 0.1868 0.6909 0.0331
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1 - 1	0.78125000 -1.03125000 -2.59375000 -2.25000000	0.94056815 0.94056815 0.94056815 0.94056815	0.4081 0.2755 0.0069 0.0186
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-2.23 43750 0 -0.31250000	0.66508212 0.66508212	0.0011 0.6394
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
] 1 1 1	1. - 1 1. - 1.	-2.75000000 0.06250000 -1.71875000 -0.68750000	0.94056815 0.94056815 0.94056815 0.94056815	0.0043 0.9471 0.0705 0.4665

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-2.00000000	0.94056815	0.0359
1	- 1	0,18750000	0.94056815	0.8424
- 1	1	-2.46875000	0.94056815	0.0100
-1	- 1	-0.81250000	0.94056815	0.3897

General Lin Dependent V	ear Mod ariable	els Procedu : Y	re	*	denotes signi	ficance
Source Model Error Corrected T	otal	DF 24 103 127	Sum of Squares 12004.12500000 20812.24218750 32816 36718750	Mean Square 500.17187500 202.06060376	F Value 2.48	Pr > F 0.0009
		R-Square 0.365797	C.V. 38.49153	Root MSE 14.21480228	Y Mean 36.9296	8750
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F
R	3	2729	.52343750	909.84114583	4.50	0.0052
Vl	1	492	.19531250	492,19531250	2.44	0 1217
V2	1	207	.57031250	207.57031250	1 03	0 3132
V1 * V2	1	929	.88281250	929,88281250	4,60	0.0343 *
V3	1	223	.13281250	223.13281250	1.10	0.2958
V1 * V3	1	164	.25781250	164.25781250	0.81	0 3694
V2 * V3	1	43	.94531250	43.94531250	0.22	0.6419
V4	1	4266	.57031250	4266.57031250	21.12	0.0001 *
V1 * V4	1	103	.32031250	103.32031250	0.51	0.4762
V2 * V4	1	48	.75781250	48,75781250	0,24	0.6243
V3 * V4	1	168	.82031250	168.82031250	0.84	0.3628
V5	1	92	.82031250	92,82031250	0.46	0.4994
V1 * V5	1.	103	.32031250	103.32031250	0.51	0.4762
V2 * V5	1	381	.57031250	381,57031250	1.89	0.1724
V3 * V5	1	76	.57031250	76.57031250	0.38	0.5395
V4 * V5	1	347	.82031250	347,82031250	1.72	0.1924
V6	1	1040	.82031250	1040 82031250	5.15	0.0253 *
V1 * V6	1	56	.44531250	56.44531250	0.28	0 5983
V2 * V6	1	303	.19531250	303,19531250	1.50	0 2234
V3 * V6	1	51	.25781250	51,25781250	0.25	0.6156
V4 * V6	1	82	.88281250	82.88281250	0.41	0.5233
V5 * V6	1	89	.44531250	89.44531250	0.44	0.5073

V1.		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		38.8906250 34.9687500	1.7768503 1.7768503	0.0001 0.0001
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		38.2031250 34.9687500	1.7768503 1.7768503	0.0001 0.0001
V1.	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1	37.4687500 40.3125000 38.9375000 31.0000000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
٧3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 ~ 1		35.6093750 38.2500000	1.7768503 1.7768503	0.0001 0.0001

V1	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1 - 1	36.4375000 41.3437500 34.7812500 35.1562500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V2	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	37.4687500 38.9375000 33.7500000 37.5625000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		42.7031250 31.1562500	1.7768503 1.7768503	0.0001 0.0001
Vl	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	45.5625000 32.2187500 39.8437500 30.0937500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 1	1 - 1 1 - 1	44.5937500 31.8125000 40.8125000 30.5000000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1. 1 1	42.5312500 28.6875000 42.8750000 33.6250000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		37.7812500 36.0781250	1.7768503 1.7768503	0.0001 0.0001
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 1 - 1	38,8437500 38,9375000 36,7187500 33,2187500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001

General Linear Models Procedure Least Square Means

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 1 1	40.7812500 35.6250000 34.7812500 36.5312500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 - 1	1 - 1 1 - 1	35.6875000 35.5312500 39.8750000 36.6250000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1 - 1	41.9062500 43.5000000 33.6562500 28.6562500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		39. 7812 500 34. 078 1250	1.7768503 1.7768503	0.0001 0.0001

General Linear Models Procedure Least Square Means

V1	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 1 1 1	42.4062500 35.3750000 37.1562500 32.7812500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V2	٧6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	42.5937500 33.8125000 36.9687500 34.3437500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
ν3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1.	1 - 1 1 - 1	39.0937500 32.1250000 40.4687500 36.0312500	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001
V4	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1 - 1	44.7500000 40.6562500 34.8125000 27.5000000	2.51228458 2.51228458 2.51228458 2.51228458 2.51228458	0.0001 0.0001 0.0001 0.0001

General Linear Models Procedure Least Square Means

V5	V 6	¥ LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	41.4687500	2,51228458	0.0001
1	- 1	34.0937500	2.51228458	0,0001
1.	1	38,0937500	2,51228458	0.0001
- 1	- 1	34.0625000	2.51228458	0.0001

SODIUM : PRODUCTION

General Lir Dependent \	lear Mode Variable	els Procedure : Y			*	den	otes signi	ficance
Source Model Error Corrected '	Potal	DF Sum 24 804 103 4661 127 5465	of Squares 3.56250000 2.86718750 6.42968750		Mean Square 335.1484375 452.5521086	0 2	F Value 0.74	Pr > E 0.7986
		R-Square 0.147166	C.V. -368.46	80	Root M 21,273	SE 27217	¥ -5.	Mean 77343750
Source	DF	Туре	III SS	Mean	Square	FV	alue	Pr > F
R	3	1372.77	343750	457	59114583	1.0	1	0 3910
V7	1	39.38	281250	30	.38281250	0.0	÷ 9	0.7686
V8	1	217.88	281250	217	.88281250	0.4	8	0.4893
V9	1	250.32	031250	250	32031250	0.5	5	0.4587
V10	1	1134.07	031250	1134	.07031250	2.5	1	0.1165
V11	1	35.07	031250	35	.07031250	0.0	8	0.7813
V7 * V11	1	178,13	281250	178	,13281250	0.3	9	0.5318
V8 * V11	1	61.88	281250	61	.88281250	0.1	4	0.7123
V9 * V11	1	56.44	531250	56	.44531250	0.1	2	0.7247
V10 * V11	1	347.82	031250	347	.82031250	0.7	7	0.3827
V12	1	1603.19	531250	1603	.19531250	3.5	4	0.0626 *
V11 * V12	1	438,82	031250	438	.82031250	0.9	7	0.3271
V13	1	2.82	031250	2	.82031250	0.0	1	0.9372
V7 * V13	1	18.75	781250	18	75781250	0.0	4	0.8391
V8 * V13	1	532.19	531250	532	.19531250	1.1	8	0.2807
V9 * V13	1	96,25	781250	96	.25781250	0.2	1	0.6456
V10 * V13	1	1281,44	531250	1281	.44531250	2.8	3	0.0955
V11 * V13	1	168.82	031250	168	.82031250	0.3	7	0.5427
V12 * V13	1	192.57	031250	192	.57031250	0.4	3	0.5156
V14	1	2,82	031250	2	82031250	0.0	1	0.9372
V11 * V14	1	0.19	531250	0	.19531250	0.0	0	0.9835
V13 * V14	1	11.88	281250	11	.88281250	0.0	3	0.8716

SODIUM : PRODUCTION

General Linear Models Procedure Least Square Means

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-5.21875000	2.65915902	0.0524
- 1	-6.32812500	2.65915902	0.0192
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1.	-4.46875000	2.65915902	0.0959
1	-7.07812500	2.65915902	0.0090
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-7.17187500	2.65915902	0.0082
- 1	-4.37500000	2.65915902	0.1030
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-8,75000000	2.65915902	0.0014
- 1	-2,79687500	2.65915902	0.2954

SODIUM : PRODUCTION

General Linear Models Procedure Least Square Means

V11		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5.25000000 -6.29687500	2.65915902 2.65915902	0.0510 0.0198
V7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-5.87500000 -4.56250000 -4.62500000 -8.03125000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.1213 0.2278 0.2216 0.0351
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-3.25000000 -5.68750000 -7.25000000 -6.90625000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.3895 0.1335 0.0566 0.0692
V 9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 · 1 - 1	1 -1 1 -1	-7.31250000 -7.03125000 -3.18750000 -5.56250000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.0546 0.0644 0.3986 0.1422
V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
----------------------	--------------------	--	--	--------------------------------------
1 - 1 - 1	1 -1 1 -1	-9.87500000 -7.62500000 -0.62500000 -4.96975000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.0100 0.0452 0.8683 0.1893
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-2.23437500 -9.31250000	2.65915902 2.65915902	0.4027 0.0007
Vll	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-3.5625000 -6.9375000 -0.9062500 -11.6875000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.3457 0.0679 0.8100 0.0024
V1 3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5.62500000 -5.92187500	2.65915902 2.65915902	0.0368 0.0281

General Linear Models Procedure Least Square Means

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-4.68750000 -5.75000000 -6.56250000 -6.09375000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.2154 0.1293 0.0840 0.1082
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-2.28125000 -6.65625000 -8.96875000 -5.18750000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.5454 0.0797 0.0189 0.1708
V9	V13	y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-6.15625000 -8.18750000 -5.09375000 -3.65625000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.1047 0.0318 0.1785 0.3332
V1 0	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-5.4375000 -12.0625000 -5.8125000 0.2187500	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.1512 0.0018 0.1253 0.9537

V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-6.25000000 -4.25000000 -5.00000000 -7.59375000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.0996 0.2610 0.1866 0.0461
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-3.3125000 -1.1562500 -7.9375000 -10.6875000	3.76061875 3.76061875 3.76061875 3.76061875 3.76061875	0.3805 0.7591 0.0372 0.0054
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		-5. 62500 000 -5.92187500	2.65915902 2.65915902	0.0368 0.0281
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 ~ 1	1 - 1 1 - 1	-5.06250000 -5.43750000 -6.18750000 -6.40625000	3.76061 875 3.76061 875 3.76061 875 3.76061 875 3.76061 875	0.1812 0.1512 0.1029 0.0915

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-5.78125000	3,76061875	0.1273
1	- 1	-5.46875000	3.76061875	0.1489
- 1	1	-5,46875000	3.76061875	0.1489
- 1	- 1	-6.37500000	3.76061875	0.0931

General L:	inear Mode	els Procedur	e			* don.	oton odmode	
Dependent	Variable	: Y	-			~ den	otes signif	licance
Source Model Error Corrected	Total	DF 24 99 127	Sum of Sc 84.6607 163.24850 247.9092	quares 7332 0087 7419	Mean So 3.52753 1.64897	uare 222 476	F Value 2.14	Pr > F 0.0048
		R-Square		C.V.	Rc	ot MSE	Y Mean	
		0.341499		-160.0315	1.	28412412	-0.802419	35
Source	DF	Туре	III SS		Mean Square	F Value	Pr >	F
R	3	4.90)697477		1,63565826	0.99	0.30	999
Vl	1	0.19	249006		0.19249006	0.12	0.55	177
V2	1	0.53	3396202		0.53396202	0.32	0.57	706
V1 * V2	1.	0.44	1176415		0.44176415	0.27	0.57	59
V3	1	6.59	9583190		6.59583190	4.00	0.04	82 *
V1 * V3	1	4.83	3121733		4.83121733	2.93	0.09	01
V2 * V3	1	1.23	3717575		1.23717575	0.75	0.38	85
V4	1	7.52	2170621		7.52170621	4.56	0.03	152 *
V1 * V4	1	0,15	5722329		0.15722329	0.10	0.75	581
V2 * V4	1	1.17	7876265		1.17876265	0.71	0.39	99
V3 * V4	1	0.47	7808908		0.47808908	0.29	0.59	915
V5	1	32.62	2942012		32.62942012	19.79	0.00	01 *
V1 * V5	1	0,28	3113683		0.28113683	0.17	0.68	306
V2 * V5	1	0.08	3803141		0.08803141	0.05	0.81	78
V3 * V5	1	1.86	5417603		1.86417603	1.13	0.29	03
V4 * V5	1	0.19	9901383		0.19901380	0.12	0.72	90
V6	1	1.23	3951670		1.23951670	0.75	0.38	180
V1 * V6	1	0.56	5397458		0.56397458	0.34	0.56	500
V2 * V6	1	4.46	5733357		4.46733357	2.71	0.10	29
V3 * V6	1.	1.48	3171515		1.48171515	0,90	0.34	55
V4 * V6	1	2.01	L602177		2.01602177	1.22	0.27	15
V5 * V6	1	11.01	134347		11.01134347	6,68	0.01	.12 *

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.82970677 -0.75066977	0.16376500 0.16363869	0.0001 0.0001
V2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - <u>1</u>		-0.85602049 -0.72435605	0.16534957 0.16207046	0.0001 0.0001
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	.1	-0.83570144	0.23139024	0.0005
1	- 1	-0,82371210	0.23138038	0.0006
- 1	1.	-0,87633954	0.23575416	0.0003
- 1	-]	-0.62500000	0.22700322	0.0070
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-0.55850154	0.16707500	0.0012
- 1		-1.02187500	0.16051552	0.0001

V1	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1.	1 -1 1 -1	-0.40003855 -1.25937500 -0.71696454 -0.78437500	0.23610471 0.22700322 0.23575416 0.22700322	0.0933 0.0001 0.0030 0.0008
V2	٧3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
.1 1 - 1 - 1	1 - 1 1 - 1	-0.11312500 -0.00125000 -0.05062500 -0.10125000	0.24048174 0.22700322 0.23138038 0.22700322	0.0033 0.0001 0.0930 0.0001
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-1.03727049 -0.54310605	0.16534957 0.16207046	0.0001 0.0011
Vl	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-1.11253855 -0.54687500 -0.96200243 -0.53933710	0.23610471 0.22700322 0.23137038 0.23138038	0.0001 0.0178 0.0001 0.0218

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-1.20082888	0.23576709	0.0001
1	-1	-0.51121210	0.23138038	0.0295
-1	1	-0.87371210	0.23138038	0.0003
-1	-1	-0.57500000	0.22700322	0.0129
¥3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.74329098	0.24048174	0.0026
1	- 1.	-0.37371210	0.23138038	0.1095
- 1	1	-1.33125000	0.22700322	0.0001
- 1	- 1	-0.71250000	0.22700322	0.0022
V5		Y LSMEAN	Stð Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1		-1,30470677	0.16376500	0.0001
1		-0.27566977	0.16363869	0.0952
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-1.39195144	0.23139024	0.0001
1	-1	-0.26746210	0.23138038	0.2505
· 1	1	-1.21746210	0.23138038	0.0001
- 1	-1	-0.28387743	0.23137038	0.2228

V 2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1 - 1	1 1 1 1	-1,34378855 -0,36825243 -1,26562500 -0,18308710	0.23610471 0.23137038 0.22700322 0.23138038	0.0001 0.1147 0.0001 0.4307
V3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0,95003855 -0,16696454 -0,65937500 -0,38437500	0.23610471 0.23575416 0.22700322 0.22700322	0.0001 0.4805 0.0001 0.0936
V4	٧5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 - 1	-1.59195144 -0.48258954 -1.01746210 -0.06875000	0.23139024 0.23575416 0.23138038 0.22700322	0.0001 0.0433 0.0001 0.7626
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.68975154 -0.89062500	0. 1670 7500 0. 16051 552	0.0001 0.0001

V1.	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.79691355 -0.86250000 -0.58258954 -0.91875000	0.23610471 0.22700322 0.23575416 0.22700322	0.0011 0.0003 0.0152 0.0001
V2	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 - 1	-0.56516598 -1.14687500 -0.81433710 -0.63437500	0.24048174 0.22700322 0.23138038 0.22700322	0.0208 0.0001 0.0007 0.0062
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.34825308 -0.76875000 -1.03125000 -1.01250000	0.24520555 0.22700322 0.22700322 0.22700322	0.1587 0.0010 0.0001 0.0001
V4	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.80891598 -1.26562500 -0.57058710 -0.51562500	0.24048174 0.22700322 0.23138038 0.22700322	0.0011 0.0001 0.0154 0.0253

V5	V6	Y	Std Err	Pr > ITI
		LSMEAN	LSMEAN	HO: LSMEAN = 0
1	1	-1.50316355	0.23610471	0.0001
1	- 1	-1.10625000	0,22700322	0.0001
- 1	1	0.12366046	0.23575416	0.6011
-].	~ 1	-0.67500000	0.22700322	0.0037

General Li	inear Mode	ls Procedur	re			* deno	otes signif	licance
Dependent	Variable	: Y						
Source		DF	Sum of Se	quares	Mean Squ	are	F Value	Pr > F
Model		24	3.31687	500	0.138203	13	0.57	0.9400
Error		103	24.77429	687	0.240527	15		
Corrected	Total	127	28.09117	187				
		R-Square		С.V.	Roc	t MSE	Y Mean	
		0.118075		-375.9028	0.4	9043568	-0.130468	375
Source	DF	Туре	III SS		Mean Square	F Value	Pr	> F
R	3	0.50	273438		0.16757813	0.70	0.55	561
V7	1	0.00	0632813		0.00632813	0.03	0.81	715
V8	1	0.04	882812		0.04882812	0.20	0.65	533
V9	1	0.10)695313		0.10695313	0.44	0.50	064
V10	1	0.41	632813		0.41632813	1.73	0.19	912
V11	1	0.17	257812		0.17257812	0.72	0.39	989
V7 * V11	1	0,05	695312		0.05695312	0,24	0.62	276
V8 * V11	1	0.01	757813		0.01757813	0.07	0.78	374
V9 * V11	1	0.00	070312		0.00070312	0.00	0.95	570
V10 * V11	1	0.35	5070312		0.35070312	1.46	0.23	300
V12	1	0,73	507812		0.73507812	3.06	0.08	334
V11 * V12	1	0.10	695312		0.10695312	0.44	0.50)64
V13	1	0.00	382812		0.00382812	0.02	0.89	999
V7 * V13	1	0.00)195313		0.00195313	0.01	0.92	284
V8 * V1.3	1	0.07	507818		0.07507813	0.31	0.5	776
V9 * V13	1	0.02	257813		0.02257813	0.09	0.75	599
V10 * V13	1	0.61	.882813		0.61882813	2.57	0.13	L18
V11 * V13	1	0.00	070312		0.00070312	0.00	0.95	570
V12 * V13	1	0,02	257812		0.02257812	0.09	0.75	599
V14	1	0.00	007812		0.00007812	0,00	0.98	357
V11 * V14	1	0.04	882812		0.04882812	0.02	0.65	533
V13 * V14	1	0.00	070313		0.00070313	0.00	0.95	570

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: L SMEAN = 0
1	-0.13750000	0.06130446	0.0270
- 1	-0.12343750	0.06130446	0.0467
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-0.11093750	0.06130446	0.0733
- 1	-0.15000000	0.06130446	0.0161
V9	Y	Std Err	Pr > ITI
	LISMEAN	LSMEAN	HO: LSMEAN = 0
1	-0.15937500	0.06130446	0.0107
- 1	-0.10156250	0.06130446	0.1006
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1.	-0.18750000	0.06130446	0.0028
- 1	-0.07343750	0.06130446	0.2337

V11		Y I.SMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	=	0
1 - 1		-0.09375000 -0.16718750	0.06130446 0.06130446	0.1293 0.0075		
V 7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN		0
1 1 - 1 - 1	1 - 1 1 - 1	-0.12187500 -0.15312500 -0.06562500 -0.18125000	0.08669760 0.08669760 0.08669760 0.08669760	0.1628 0.0803 0.4508 0.0390		
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	=	0
1 1 -1 -1	1 - 1 - 1 - 1	-0.06250000 -0.15937500 -0.12500000 -0.17500000	0.08669760 0.08669760 0.08669760 0.08669760	0.4726 0.0689 0.1524 0.0461		
V 9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	Ħ	0
1 1 -1 -1	1 - 1 1 - 1	-0.12500000 -0.19375000 -0.06250000 -0.14062500	0.08669760 0.08669760 0.08669760 0.08669760	0.1524 0.0276 0.4726 0.1079		

V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1	1 - 1 - 1 - 1	-0.20312500 -0.17187500 -0.01562500 -0.16250000	0.08669760 0.08669760 0.08669760 0.08669760	0.0211 0.0501 0.8573 0.0637
V1.2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-0.05468750 -0.20625000	0.06130446 0.06130446	0.3744 0.0011
V11	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1. - 1	1 -1 1 -1	-0.04687500 -0.14062500 -0.06250000 -0.27187500	0.08669760 0.08669760 0.08669760 0.08669760	0.5899 0.1079 0.4726 0.0022
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1.		-0.12500000 -0.13593750	0.06130446 0.06130446	0.0440 0.0288

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-0.12812500 -0.14687500 -0.12187500 -0.12500000	0.08669760 0.08669760 0.08669760 0.08669760	0.1425 0.0933 0.1628 0.1524
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-0.08125000 -0.14062500 -0.16875000 -0.13125000	0.08669760 0.08669760 0.08669760 0.08669760 0.08669760	0.3509 0.1079 0.0543 0.1331
V9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 - 1	1 - 1 1 - 1	-0.14063500 -0.17812500 -0.10937500 -0.09375000	0.08669760 0.08669760 0.08669760 0.08669760	0.1079 0.0425 0.2100 0.2821
V10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-0.11250000 -0.26250000 -0.13750000 -0.00937500	0.08669760 0.08669760 0.08669760 0.08669760	0.1973 0.0031 0.1158 0.9141

V11	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	= (C
1 1 ~ 1 - 1	1 - 1 1 - 1	-0.09062500 -0.09687500 -0.15937500 -0.17500000	0.08669760 0.08669760 0.08669760 0.08669760	0.2983 0.2664 0.0689 0.0461		
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	=	0
1 1 -1 ~1	1 -1 1 -1	-0.06250000 -0.04687500 -0.18750000 -0.22500000	0.08669760 0.08669760 0.08669760 0.08669760	0.4726 0.5899 0.0329 0.0108		
V] 4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	=	0
1 1.		-0.12968750 -0.13125000	0.06130446 0.06130446	0.0368 0.0346		
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN	æ	0
1 1 - 1 - 1	1 -1 1 -1	-0.11250000 -0.07500000 -0.14687500 -0.18750000	0.08669760 0.08669760 0.08669760 0.08669760	0.1973 0.3890 0.0933 0.0329		

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-0.12187500	0.08669760	0.1628
1.	- 1	-0.12812500	0.08669760	0.1425
- 1	1	-0.13750000	0.08669760	0.1158
- 1	- 1	-0.13437500	0.08669760	0.1242

General Li Dependent	inear Mode Variable	ls Procedu: : Y	t e	*	denotes signi	ficance
Source		DF	Sum of Squares	Mean Square	F Value	Pr > F
Model		24	6782.62500000	282.60937500	1.78	0.0246
Error		103	16326.80468750	158,51266687		
Corrected	Total	127	23109.42968750			
		R-Square	С.V.	Root MSE	Y Mean	
		0.293500	-60.74418	12.59018137	-20.7265	6250
Source	DF	Туре	III SS	Mean Square	F Value	Pr > F
R	3	1736.33	593750	578.77864583	3.65	0.0150
V1	_L	524.07	031250	524.07031250	3.31	0.0719
V2	1	388.50	781250	388.50781250	2.45	0.1205
V1 * V2	1	341.25	781250	341.25781250	2.15	0.1454
V3	1	438.82	031250	438.82031250	2.77	0.0992
V1 * V3	1	548.63	281250	548,63281250	3.46	0.0657
V2 * V3	1	6.57	031250	6.57031250	0.04	0.8391
V4	1	775.19	531250	775.19531250	4.89	0.0292 *
V1 * V4	1	23.63	281250	23,63281250	0.15	0.7002
V2 * V4	1	14.44	531250	14.44531250	0.09	0.7634
V3 * V4	1	446.25	781250	446.25781250	2.82	0.0964
V5	1	46.32	031250	46.32031250	0.29	0.5900
V1 * V5	1	288.44	531250	288,44531250	1.44	0.2327
V2 * V5	1.	303,19	531250	303,19531250	1.91	0.1696
V3 * V5	1	51.25	781250	51.25781250	0.32	0.5708
V4 * V5	1	150.94	531250	150.94531250	0.95	0.3314
V6	1	500.07	031250	500.07031250	3.15	0.0787
V1 * V6	1	5.69	531250	5,69531250	0.04	0.8500
V2 * V6	1	15,82	031250	15.82031250	0.10	0.7527
V3 * V6	1	56.44	531250	56.44531250	0.36	0,5520
V4 * V6	1	11.88	281250	11.88281250	0.07	0.7848
V5 * V6	1	168.82	031250	168.82031250	1.07	0.3045

V1		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-18.7031250 -22.7500000	1.5737727 1.5737727	0.0001 0.0001
V 2		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1		-18.9843750 -22.4687500	1.5737727 1.5737727	0.0001 0.0001
V1	V2	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 - 1 - 1	-18.5937500 -18.8125000 -19.3750000 -26.1250000	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V3		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-22.5781250 -22.8750000	1.5737727 1.5737727	0.0001 0.0001

V1	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-22.6250000 -14.7812500 -22.5312500 -22.9687500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V2	V3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-21.0625000 -19.9062500 -24.0937500 -20.8437500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V4		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-18.2656250 -23.1875000	1.5737727 1.5737727	0.0001 0.0001
V1	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-15.8125000 -21.5937500 -20.7187500 -24.7812500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001

V2	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-16.1875000 -21.7812500 -20.3437500 -24.5937500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V3	V4	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 - 1 1 - 1	-18.2500000 -26.9062500 -18.2812500 -19.4687500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V5		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1		-20.1250000 -21.3281250	1.5737727 1.5737727	0.0001 0.0001
V1	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-19.4375000 -17.9687500 -20.8125000 -24.6875000	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001

V2	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 - 1 1 - 1	-16.8437500 -21.1250000 -23.4062500 -21.5312500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
٧3	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 -1 -1	1 -1 1 -1	-21.3437500 -23.8125000 -18.9062500 -18.8437500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V4	V5	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-18.7500000 -17.7812500 -21.5000000 -24.8750000	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V6		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-18.7500000 -22.7031250	1.5737727 1.5737727	0.0001 0.0001

V1	٧6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 1	-16,9375000 -20,4687500 -20,5625000 -24,9375000	2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V2	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1 - 1	1 -1 1 -1	-16.6562500 -21.3125000 -20.8437500 -24.0937500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V3	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-19.9375000 -25.2187500 -17.5625000 -20.1875000	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001
V4	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-16,5937500 -19,9375000 -20,9062500 -25,4687500	2.2256507 2.2256507 2.2256507 2.2256507 2.2256507	0.0001 0.0001 0.0001 0.0001

V5	V6	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-17.0000000	2.2256507	0.0001
1	*-]	-23.2500000	2.2256507	0.0001
1	1	-20.5000000	2.2256507	0.0001
-1	·· 1	-22.1562500	2,2256507	0.0001

General Line Dependent Va	ear Mode ariable	els Procedure : Y		* den	otes significance
Source Model Error Corrected Te	otal	DFSum of Sc244512.4310320882.7412725395.13	quares Me 3750000 18 4218750 20 7968750	ean Square 88.01822917 02.74506978	F Value Pr > F 0.93 0.5658
		R-Square 0.177689	C.V. -164.6408	Root MSE 14.23885774	Y Mean -8.6483750
Source	DF	Type III SS	Mean Square	F Value	Pr > F
R	3	61.02343750	20.3411458	3 0.10	0.9597
V'7	1	33,00781250) 33.0078125(0 0.16	0.6874
V8	1	402.57031250	402.57031250	D 1.99	0.1618
V9	1	0.19531250	0.19531250	0.00	0.9753
V10	1	255.94531250) 255,9453125(0 1.26	0.2638
V11	1	41.63281250	41.63281250	0.21	0.6514
V7 * V11	1	187.69531250) 187.69531250	0.93	0.3382
V8 * V11	1	4.13281250) 4.13281250	0.02	0.8867
V9 * V11	1	155.32031250) 155.3203125(0.77	0.3835
V10 * V11	1	395,50781250) 395.50781250) 1.95	0.1655
V12	1	995,69531250	995.69531250	0 4.91	0.0289 *
V11 * V12	1	402.57031250	402.57031250	0 1.99	0.1618
V13	1	13.13281250) 13.13281250	0.06	0.7996
V7 * V13	1	126.00781250) 126.00781250	0.62	0.4323
V8 * V13	1	424.13281250) 424.13281250	0 2.09	0.1511
V9 * V13	1	99.75781250) 99.7578125(0.49	0.4846
V10 * V13	1	825,19531250	825.19531250	0 4.07	0.0462 *
V11 * V13	1	18.75781250	18.75781250	0.09	0.7616
V12 * V13	1	6.57031250	6.57031250	0.03	0.8575
V14	1	46.32031250	46,32031250	0.23	0.6337
V11 * V14	1	17.25781250) 17.2578125(0.09	0.7711
V13 * V14	1	0,00781250	0.00781250	0.00	0.9951

V7	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-8.14062500	1.77985722	0.0001
- 1	-9.15625000	1.77985722	0.0001
V8	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1.	-6.8750000	1.77985722	0.0002
- 1	-10.4218750	1.77985722	0.0001
V9	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-8.68750000	1.77985722	0.0001
- 1	-8.60937500	1.77985722	0.0001
V10	Y	Std Err	Pr > ITI
	LSMEAN	LSMEAN	HO: LSMEAN = 0
1	-10.0625000	1.77985722	0.0001
- 1	-7.2343750	1.77985722	0.0001

V11		y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1. - 1		-8.07812500 -9.21875000	1.77985722 1.77985722	0.0001 0.0001
V 7	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-8.7812500 -7.5000000 -7.3750000 -10.9375000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0007 0.0036 0.0042 0.0001
V8	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 - 1 1 - 1	-6.1250000 -7.6259000 -10.0312500 ~10.8125000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0167 0.0031 0.0001 0.0001
V9	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 1 - - - 1	-9,2187500 -8,1562500 -6,9375000 -10,8125000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0004 0.0016 0.0069 0.0001

V10	V11	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 - 1	1 -1 1 -1	-11.2500000 -8.8750000 -4.9062500 -9.5625000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0001 0.0006 0.0540 0.0002
V12		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-5.8593750 -11.4375000	1.77985722 1.77985722	0.0014 0.0001
Vll	V12	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 1 -1	1 -1 1 -1	-7.0625000 -9.0937500 -4.6562500 -13.7812500	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0060 0.0005 0.0672 0.0001
V13		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1		-8.96875000 -8.32812500	1. 779857 22 1. 77985 722	0.0001 0.0001

V7	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-7.4687500 -8.8125000 -10.4687500 -7.8437500	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0037 0.0007 0.0001 0.0024
V8	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 -1 1 -1	-5.3750000 -8.3750000 -12.5625000 -8.2812500	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0351 0.0012 0.0001 0.0014
V9	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-8.12500000 -9.25000000 -9.81250000 -7.40625000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0017 0.0004 0.0002 0.0040
V10	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 - 1 - 1	1 -1 1 -1	-7.8437500 -12.2812500 -10.0937500 -4.3750000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0024 0.0001 0.0001 0.0852

V11	V1.3	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 ~ 1 - 1	1 -1 1 -1	-8.78125000 -7.37500000 -9.15625000 -9.28125000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0007 0.0042 0.0004 0.0004
V12	V13	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 1 -1 -1	1 - 1 1 - 1	-6.4062500 -5.3125000 -11.5312500 -11.3437500	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0124 0.0372 0.0001 0.0001
V14		Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1 - 1		-8.04687500 -9.25000000	1.77985722 1.77985722	0.0001 0.0001
V11	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
] 1 - 1 - 1	1 - 1 1 - 1	-7.8437500 -8.3125000 -8.2500000 10.1875000	2.5170982 2.5170982 2.5170982 2.5170982 2.5170982	0.0024 0.0013 0.0014 0.0001

V13	V14	Y LSMEAN	Std Err LSMEAN	Pr > ITI HO: LSMEAN = 0
1	1	-8.37500000	2.5170982	0.0012
1	- 1	-9.56250000	2.5170982	0.0002
-1	1	-7.71875000	2.5170982	0.0028
- 1	-1	~8.93750000	2.5170982	0.0006

OSTASIS ATHWAYS Appendix IV Intrinsic Extrinsic Coagulation Coagulation Pathway GINH Pathway Party and VII 332 ARRENTER REPRESENTATION OF THE OWNER OWN Tasse W Factor ly Charged ILMW Kininogr Día VE 0 ua Tase Cot Vila-II-Xa-LACI Inactive Common Coagulation Pathway 44 ingited. Ingthe I GBE Fibrinolytic Panapa Japad 瓜田 System Survey and and a state IN IS IS IS IS lipsi Protecter S Thrombo-medicin 62 Protein (LERE Protest C lauthe Graphi KEY Provense (me Precarsion (in) divigen it precarsion denoted by an numerals unter Diversionen Products lactor pro Enzymatic Complexes (mais true taux collactore), surfaces, non-etc. Activated Entyme Advances Mays Calabies Suscentrity of complexes or mul-tiple functions of a factor Indulation Name Bor B Rathers with two predering sciences

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