

DECOMPOSITION COORDINATING METHOD FOR THE SOLUTION OF A MULTI-AREA
POWER SYSTEM DYNAMIC OPTIMISATION PROBLEM INCORPORATING
DISTRIBUTED GENERATION SOURCES

by

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DECLARATION

I, Litha Mbangeni, declare that the contents of this dissertation/thesis represent my own unaided work, and that the dissertation/thesis has not previously been submitted for academic examination towards any qualification. Furthermore, it represents my own opinions and not necessarily those of the Cape Peninsula University of Technology.



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ABSTRACT

This research investigates the optimal coordination of wind and thermal power generation in single- and multi-area systems using advanced economic dispatch formulations and optimization methods. A comprehensive literature review was conducted to examine existing problem formulations, methodologies, and algorithms applied to hybrid power systems, including wind-thermal, wind-diesel, wind-PV, and hydrothermal configurations.

The study first develops a rigorous mathematical formulation for the wind-thermal economic emission dispatch (WEED) problem in a single-area power system, explicitly incorporating operational constraints and emission considerations. The formulation is then extended to a multi-area wind-thermal economic dispatch (WTED) problem, where inter-area power exchange and tie-line constraints are modelled to reflect realistic interconnected grid conditions.

Two optimization techniques are developed and implemented: the Lagrange multiplier method, representing a conventional analytical approach, and the Particle Swarm Optimization (PSO) method, representing a modern metaheuristic algorithm. Both methods are applied to the single-area and multi-area WTED problems. To facilitate computational analysis, MATLAB-based software is developed for each approach, including a decomposition-based framework for the multi-area case to enhance scalability and solution efficiency.

The developed methods are tested on standard IEEE benchmark systems, and the obtained results are compared with existing solutions reported in the literature. The comparative analysis demonstrates the accuracy, robustness, and computational efficiency of the proposed approaches. The findings provide valuable insights into optimizing hybrid wind-thermal power systems, advancing sustainable, economically efficient power generation strategies.

Keywords: Multi-region wind-conventional economic emission dispatch, decomposition approach, renewable energy, and optimization techniques.

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DEDICATION

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TABLE OF CONTENTS

ii

Declaration	
Abstract	iii
Acknowledgements	iv
Dedication	v
Table of contents	vi
List of figures	ix
List of tables	x
Glossary	xiv

CHAPTER 1: INTRODUCTION

1.1	Awareness of the research problem	1
1.2	Statement of the research problem	2
1.3	Design-based problems	3
1.4	Sub-problems of implementation	4
1.5	Research aim and objectives	4
1.5.1	Research Aim	4
1.5.2	Objectives	4
1.6	Hypothesis	5
1.7	Delimitation of the research	5
1.8	Motivation of the research	6
1.9	Assumption	7
1.10	The deliverables of the thesis	7
1.11	Chapter breakdown	8
1.12	Conclusion	9

CHAPTER TWO: LITERATURE REVIEW

2.1	Introduction	10
2.2	Wind-thermal economic dispatch	11
2.2.1	Wind-thermal economic emission formulation for a single area dispatch problem	12
2.2.1.1	Problem formulation for single-criterion economic dispatch	12
2.2.1.2	Multi-criterion economic dispatch.	31
2.2.2	Study of optimisation techniques employed in solving the single-area dynamic wind-thermal economic dispatch problem	33
2.2.2.1	Single criteria	33
2.2.2.2	Multi criteria	37
2.3	Economic dispatch for Hybrid Renewable Energy Systems (HRES)	60
2.3.1	Study the techniques applied in solving the single-area economic dispatch problem for Hybrid Renewable Energy Systems (HRES)	61
2.3.1.1	Single-criteria	61
2.3.1.2	Multi-criteria	64
2.4	Multi-area wind-thermal economic dispatch	75
2.4.1	Study on mathematical models and techniques applied to resolve the multi-area wind-thermal economic dispatch	78
2.4.1.1	Single-criteria	78
2.4.1.1	Multi-criteria	79

vii

2.4.2	Multi-area economic emission dispatch problem formulation	82
2.5	Outcomes from analysis of the literature	93
2.5.1	Examination of the problem formulation used to solve both single-area and multi-area economic dispatch problems with single- and multiple-criteria.	93
2.5.2	Analysis of methods and algorithms used to solve single- and multi-criteria single-area and multi-area economic dispatch problems.	93
2.6	Conclusion	94

CHAPTER THREE: WIND-THERMAL ECONOMIC EMISSION DISPATCH(WTEED) PROBLEM USING LAGRANGE’S ALGORITHM

3.1	Introduction	95
3.2	WTEED problem formulation	95
3.2.1	Wind-thermal economic emission formulation for a single area dispatch problem	95
3.2.1.1	Emission cost function formulation	96
3.2.1.2	Probability distribution function for wind power	98
3.3	Optimisation of a single area dispatch problem with multi-criteria	101
3.4	The algorithm applied in solving the single-area WTEED problem	101
3.5	Description of the Test Systems	106
3.5.1	Test System 1: IEEE30 bus system with 6 units	107
3.5.1.1	WTEED problem discussion and results for the six-unit system	108
3.5.2	Test System 2: IEEE30 bus system with 10-units.	110
3.5.2.1	WTEED problem results and discussion for Ten-Unit System	110
3.5.3	Test System 3: IEEE30 bus system with 40-units	113
3.5.3.1	WTEED problem results and discussions for the Forty-Unit System	119
4.	Conclusion	122

CHAPTER FOUR: WIND-THERMAL COMBINED ECONOMIC DISPATCH(WTEED) PROBLEM USING PARTICLE SWARM OPTIMIZATION(PSO)

4.1	Introduction	124
4.2	PSO algorithm	124
4.3	WTEED problem solution using the developed PSO algorithm	125
4.4	Application of PSO algorithm to solve the WTEED problem	132
4.4.1	Test system 1: IEEE 30 bus system with six generation units	132
4.4.1.1	The IEEE30 bus system with 6-unit results discussion	133
4.4.2	Test system 2: IEEE 30 bus system with 10 generation units	135
4.4.2.1	The IEEE 30 bus system with 10-units results discussion	136
4.4.3	Test System 3: IEEE 30 bus system with 40 generation units	138
4.4.3.1	The IEEE 30 bus system for 40-units results, and discussion	139
5.	Conclusion	142

CHAPTER FIVE: MULTI-AREA WIND-THERMAL ECONOMIC EMISSION DISPATCH(MAWTEED) PROBLEM USING LAGRANGE MULTIPLIER METHOD(LMM)

5.1	Introduction	144
5.2	Multi-area wind-thermal economic emission dispatch problem formulation	144
5.3	Solution of the MAWTEED problem using Lagrange’s decomposition coordinating method.	147

5.4	Algorithm of the Lagrange decomposition-coordinating method for calculation of the MAWTEED problem	150
5.5	Studies of the multi-area MAWTEED problem solutions	150
5.5.1	Test system I: IEEE30 bus system using 6-units	153
5.5.1.1	The MAWTEED problem results and discussion for the 6-Unit System	155
5.5.2	Test System 2: IEEE30 bus system using a 12-unit system	155
5.5.2.1	The MAWTEED problem results, and discussion for the 12-Unit System	158
5.5.3	Test System 3: IEEE30 bus system using 40 generating units	159
5.5.3.1	The MAWTEED problem results, and discussion for a 40-Unit System	164
6.	Conclusions	165

CHAPTER SIX: MULTI-AREA WIND-THERMAL ECONOMIC EMISSION DISPATCH(MAWTEED) PROBLEM USING PARTICLE SWARM OPTIMISATION (PSO)

6.1	Introduction	166
6.2	Introduction to the PSO algorithm	166
6.3	PSO algorithm developed for the solution of the MAWTEED problem	167
6.4	Case studies of the multi-area MAWTEED problem solutions	172
6.4.1	Test system I: IEEE 30 bus system with 6 generating units.	174
6.4.1.1	The MAWTEED problem results, and discussion for the 6-Unit System	176
6.4.2	Test System 2: IEEE30 bus system with 12 generating units.	176
6.4.2.1	Discussion of the MAWTEED Problem for the 12-Unit System	180
6.4.3	Test System 3: IEEE30 bus system with 40 generating units.	180
6.4.3.1	The MAWTEED problem results and discussion for the 40-Unit System	185
6.5	Conclusions	185

CHAPTER SEVEN: CONCLUSION AND FUTURE RECOMMENDATIONS

7.1	Introduction	187
7.2	Research aim and objectives	187
7.2.1	Research Aim	187
7.2.2	Objectives	187
7.3	The deliverables of the thesis	188
7.3.1	A comparative review of the current methodologies for addressing the single-area and multi-area economic emission dispatch problem.	188
7.3.2	Mathematical formulation of the economic dispatch problems	188
7.3.3	Optimisation methods developed to solve the economic emission dispatch problems	188
7.3.4	Software development and implementation for the solution to the economic emission dispatch problem for both single and multi-area systems	189
7.4	Implementation of the thesis findings	190
7.5	Future research	191
7.6	Publications	191

REFERENCES 193**LIST OF FIGURES**

Figure 1.1: Model of a multi-area power system with tie-line power transfer (Krishnamurthy & Tzoneva, 2016)	1
Figure 2.1: Organisation of optimisation techniques (Kothari & Dhillon, 2012)	10
Figure 2.2: Single-area and Multi-area power systems Dispatch Problem Organisation	11
Figure 2.3: Conventional cost curve with/without VPLE (A. Ghasemi et al., 2016)	13
Figure 2.4: Ramp rate limits of a generating unit (Kothari & Dhillon, 2012)	15
Figure 2.5: Effective cost attributes with restricted operational zones (Kothari & Dhillon, 2012)	16
Figure 2.6: A power curve for a general wind turbine(Masters, 2004)	17
Figure 2.7: Wind velocity Probability Density Function (PDF) (Masters, 2004)	19
Figure 2.8: Predicted model for WNN (Meyyappan & Pandu, 2015)	34
Figure 2.9: Quantity of papers for wind-thermal economic dispatch on yearly basis	43
Figure 2.10: Quantity of papers vs algorithm of wind-thermal economic dispatch	46
Figure 2.11: Power sources and storage for mixed renewable energy system (Ogunjuyigbe et al., 2016)	61
Figure 2.12: Quantity of papers for HRES economic dispatch on yearly basis	66
Figure 2.13: The quantity of papers pertaining to the HRES economic dispatch algorithms	67
Figure 2.14: Interconnected power system(Krishnamurthy & Tzoneva, 2016)	75
Figure 2.15: Quantity of papers for multi-area wind-thermal dispatch problem on yearly basis.	76
Figure 2.16: Quantity of papers for multi-area wind-thermal dispatch problem versus algorithm	78
Figure 2.17: Decomposition structure with two levels (Krishnamurthy & Tzoneva, 2016)	80
Figure 3.1: Conventional cost curve with or without valve-point loading effect.	96
Figure 3.2: Flow diagram of the bi-criteria dispatch problem algorithm solution.	105
Figure 3.3: Wind-thermal economic dispatch power system model with six generators.	107
Figure 3.4: Fuel cost and emissions for various algorithms using a 6-unit system	109
Figure 3.5: Comparison of the Fuel cost and emission analysis for different optimization algorithms applied to a 6-unit system.	109
Figure 3.6: Values of fuel cost and power demand for various algorithms employing a 10-unit system in comparison to the developed algorithm	112
Figure 3.7: Values of emission and power demand for various algorithms employing a 10-unit system in comparison to the developed	112

algorithm	
Figure 3.8: Values of fuel cost and power demand for various algorithms using a 40-unit system in relation to the developed method	121
Figure 3.9: Values of emission and power demand for various algorithms using a 40-unit system in relation to the developed algorithm.	122
Figure 4.1: PSO algorithm for the WTEED problem solution flowchart.	131
Figure 4.2: Values of fuel cost and power demand for various algorithms using a 6-unit system compared to the developed PSO	134
Figure 4.3: Emission and power demand values for different algorithms using a 6-unit system compared to the developed PSO	134
Figure 4.4: Values of fuel cost and power demand for various algorithms applied to a 10-unit system, and compared to the developed PSO algorithm.	137
Figure 4.5: Values of emission and power demand for various algorithms Applied to the 10-unit system and compared to the developed PSO algorithm	137
Figure 4.6: Values of CEED and power demand for various algorithms Applied to the 10-unit system in relation to the developed PSO algorithm	138
Figure 4.7: Values of fuel cost and power demand for the WTEED problem using PSO algorithm applied to a 40-unit system	141
Figure 4.8: Values of fuel cost and emission for the WTEED problem using PSO algorithm applied to a 40-unit system	142
Figure 5.1: Lagrange decomposition coordinating algorithm for the solution of MAWTEED problem in two level structure	149
Figure 5.2: Lagrange's decomposition-coordinating algorithm flowchart for solving the MAWTEED problem	152
Figure 5.3: Fuel cost versus power demand for different optimisation methods using the LM algorithm for a 6-unit system	154
Figure 5.4: Fuel cost versus power demand for different optimisation methods using the LM algorithm for a 12-unit system	157
Figure 5.5: Emission versus power demand for different optimisation methods using the LM algorithm for a 12-unit system	157
Figure 5.6: CEED versus power demand for different optimisation methods using the LM algorithm for a 12-unit system	158
Figure 5.7: Values of fuel cost, and power demand for MAWTEED problem using the LM algorithm for a 40-unit system	163
Figure 5.8: Values of emission, and power demand for the MAWTEED problem using the LM algorithm for a 40-unit system	164
Figure 6.1: The MAWTEED problem solution flowchart of applied to PSO algorithm	173
Figure 6.2: Fuel cost versus power demand for different optimisation methods using the PSO algorithm for a 6-unit system	175
Figure 6.3: Values of fuel cost, and power demand for various optimisation strategies applied to PSO algorithm for a 12-unit system	178
Figure 6.4: Emission versus power demand for different optimisation methods using the PSO algorithm for a 12-unit system	179
Figure 6.5: CEED versus power demand for different optimisation methods using the PSO algorithm for a 12-unit system	179
Figure 6.6: Values of fuel cost, and power demand for MAWTEED problem applied to PSO with a 40-unit system	184
Figure 6.7: Emission versus power demand for the bi-criteria dispatch problem using PSO for 40-unit system	185

LIST OF TABLES

Table 2.1: Quantity of papers for wind-thermal economic dispatch on a yearly basis	41
Table 2.2: Techniques and algorithms applied to solve the single-area wind-thermal economic dispatch problem	43
Table 2.3: Review of the papers on single and multi-criteria wind-thermal economic dispatch problem.	47
Table 2.4: Number of publications of HRES economic dispatch on yearly basis	65
Table 2.5: Techniques and algorithms applied to the HRES single-area economic dispatch problem.	66
Table 2.6: Study of literature for single and multi-criteria hybrid renewable energy systems.	68
Table 2.7: Quantity of papers for multi-area dispatch problem on yearly basis	75
Table 2.8: Techniques and algorithms applied to solve the multi-area wind-thermal economic dispatch problem	76
Table 2.9: Multi-area review papers for single and multi-criteria dispatch problem	84
Table 3.1: IEEE 30 Bus System data for 6 thermal system.	106
Table 3.2: Transmission line coefficients	106
Table 3.3: Wind-speed data	106
Table 3.4: The WTEED using LMM with different power demand for a 6-unit system	107
Table 3.5: : LMM-based WTEED in comparison to other optimisation techniques PD = 283.4 [MW]	108
Table 3.6: Various power demands applied to a 10-unit generators for LMM WTEED problem	110
Table 3.7: The WTEED problem with Lagrange compared with other optimization algorithms PD = 2000 [MW]	111
Table 3.8: Developed LMM compared with various algorithms for the ten-unit system (Secui et al., 2024a)	113
Table 3.9: IEEE 30 Bus System data for 40 thermal system	114
Table 3.10(a): The B-coefficients $B_{ij} \times 10^{-6}$, $B_{0i} \times 10^{-4}$, and B_{00} for 40-unit system	115
Table 3.10(b): The B-coefficients $B_{ij} \times 10^{-6}$, $B_{0i} \times 10^{-4}$, and B_{00} for 40-unit system	116
Table 3.11: Various power demands applied to a 40-unit generators for LMM WTEED problem	118
Table 3.12: The WTEED problem with Lagrange compared with other optimization algorithms for an IEEE 40-unit system for PD = 10,500 MW	119
Table 3.13: Developed LMM compared with various algorithms for the 40-unit system(Secui et al., 2024a)	121
Table 4.1: The wind-thermal economic emission dispatch problem using PSO method with various power demands	132
Table 4.2: : PSO, and LMM compared to other optimisation algorithms for WTEED problem, PD = 283.4 MW	133
Table 4.3: The wind-thermal economic emission dispatch problem using PSO with various power demands for 10-unit generators	135
Table 4.4: PSO compared to LM method and other optimization algorithms for WTEED problem applied to 10-unit system, PD = 2000[MW]	136
Table 4.5: Table 4.5: Various power demands applied to a 40-unit generators for PSO WTEED problem	139
Table 4.6: PSO compared to LM method and other optimization algorithms for WTEED problem applied to 40-unit system, PD = 10500[MW]	140
Table 5.1: The MAWTEED problem using the Lagrange multiplier method with various power demands	153

Table 5.2: The MAWTEED problem using the Lagrange multiplier method is compared with other optimisation algorithms using PD = 1263[MW]	154
Table 5.3: The MAWTEED problem using LM Method with several power demands for 12-unit generators.	155
Table 5.4: Lagrange multiplier method compared with other optimisation algorithms for MAWTEED problem, PD = 2090[MW]	156
Table 5.5: Wind-speed data	159
Table 5.6: IEEE 30 Bus System data for 40 thermal system	160
Table 5.7: The MAWTEED problem using Lagrange multiplier method with various power demands for 40-unit system	161
Table 5.8: Lagrange algorithm compared with other optimization algorithms for MAWTEED applied to IEEE 40-unit system for PD = 10500[MW]	162
Table 5.9: LMM Comparison with various algorithms(Ahmed et al., 2022)	163
Table 6.1: The MAWTEED problem applied to PSO algorithm with various power demands	174
Table 6.2: PSO and LM compared with other optimisation algorithms for MAWTEED problem using PD = 1263[MW]	175
Table 6.3: The MAWTEED problem using PSO with various power demands for 12-unit system.	177
Table 6.4: PSO compared with other optimisation algorithms for MAWTEED problem, PD = 2090[MW]	177
Table 6.5: Wind-speed data	180
Table 6.6: IEEE 30 Bus System data for 40 thermal system.	181
Table 6.7: The MAWTEED problem PSO method with various power demands for 40-unit system	182
Table 6.8: MAWTEED using PSO in relation with other optimization algorithms applied 40-unit system, PD = 10500[MW]	183
Table 6.9: Relation of PSO with various algorithms (Ahmed et al., 2022)	184
Table 7.1: Developed programs for the solution of a single area WTEED problem	189
Table 7.2: Developed programs for the solution of a multi-area WTEED problem	190
 APPENDICES	 209
 APPENDIX A: DEVELOPED MATLAB PROGRAM FOR A SINGLE AREA WTEED PROBLEM USING LAGRANGE’S ALGORITHM	 209
Appendix A1: MATLAB script file – WTEED_case6units.m	209
Appendix A2: MATLAB script file – WTEED_case10units.m	212
Appendix A3: MATLAB script file – WTEED_case40units.m	215
APPENDIX B: DEVELOPED MATLAB PROGRAM FOR A SINGLE AREA WTEED PROBLEM USING PSO ALGORITHM	221
Appendix B1: MATLAB script file – WTEED_casePSO6units.m	221
Appendix B2: MATLAB script file – WTEED_casePSO10units.m	223
Appendix B3: MATLAB script file – WTEED_casePSO40units.m	226
APPENDIX C: DEVELOPED MATLAB PROGRAM FOR A MULTI-AREA WTEED PROBLEM USING LAGRANGE’S ALGORITHM	232
Appendix C1: MATLAB script file – MAWTEED_case6units.m	232
Appendix C2: MATLAB script file – MAWTEED_case12units.m	235
Appendix C3: MATLAB script file – MAWTEED_case40units.m	249
APPENDIX D: DEVELOPED MATLAB PROGRAM FOR A MULTI-AREA WTEED PROBLEM USING PSO ALGORITHM	245
Appendix D1: MATLAB script file – MAWTEED_casePSO6units.m	243
Appendix D2: MATLAB script file – MAWTEED_casePSO12units.m	243

GLOSSARY

ABBREVIATIONS AND ACRONYMS

Acronyms/Abbreviations	Explanation
ABC	Artificial Bee Colony
AI	Artificial Intelligence
ANN	Artificial Neural Network
ANN/GA/PL	Artificial Neural Network with Genetic Algorithm and Priority List
CC	Cluster of Computers
CCP	Chance Constrained Programming
CDF	Cumulative Distribution Function
CE-NSGA-II	Controlled Elitist-Non-Dominated Sorting Genetic Algorithm II
CMA-ES	Covariant Matrix Adaptation Evolution Strategy
DED	Dynamic Economic Dispatch
DER	Distributed Energy Resources
DSR	Down Spinning Reserve
ED	Economic Dispatch
EED	Economic Emission Dispatch
EP	Evolutionary Programming
EV	Electric Vehicle
FF	Fuel Function
FFG	Fossil Fuel Fired Generator
GA	Genetic Algorithm
GT	Game Theory
H-MCSA-DE	Hybrid Modified Cuckoo Search Algorithm and Differential Algorithm
HRES	Hybrid Renewable Energy System
HS	Harmony Search
IO	Iterative Optimisation
IOT	Iterative Optimisation Technique
LR	Lagrangian Relaxation
MADED	Multi-Area Dynamic Economic Dispatch
MAED	Multi Area Economic Dispatch
MAEED	Multi Area Economic Emission Dispatch
MAWTEED	Multi Area Wind Thermal Economic Emission Dispatch
MATLAB	Matrix Laboratory
MDT	Minimum Down Time
MILP	Mixed Integer Linear Programming
MIP	Mixed Integer Programming
ML	Machine Learning
MLT	Mean Learning Technique
MOEA	Multi-Objective Evolutionary Algorithm
MUT	Minimum Up time
MW	Megawatt
NSGA-II	Non-Dominated Sorting Genetic Algorithm II
OCD	Optimal Conditional Decomposition
PDF	Probability Distribution Function
PDIP	Primal Dual Interior Point
PL	Priority List
PSO	Particle Swarm Optimisation
PV	Photovoltaic

QNM	Quasi-Newton Method
RES	Renewable Energy Source
RTDS	Real Time Digital Simulator
RVCA	Real-Valued Cultural Algorithm
SA	Simulated Annealing
SED	Static Economic Dispatch
SMCS	Sequential Monte Carlo Simulation
SMODE	Summation-based Multi-Objective Differential Evolution
USR	Up Spinning Reserves
WECS	Wind Energy Convention System
WDF	Weibull Distribution System
WPDF	Weibull Probability Distribution Function
WTEED	Wind Thermal Economic Emission Dispatch
P_w	Power delivered by a wind turbine [MW]
P_R	Rated power output of the wind turbine[MW]
v_{in}	Cut in wind speed[m/s]
v_r	Rated wind speed[m/s]
v_{out}	Cut out wind speed[m/s]
ρ	Air Density[kg/m ³]
A	Rotor swept area
C_p	Power coefficient of a wind turbine
$F(v)$	Wind probability distribution function
k, c	Weibull distribution shape and scale parameters
F_C	Total generation cost[\$/h]
C_i	Cost coefficient of a generator i
P_{Gi}	Output power of thermal generator I [MW]
P_{Di}	Power demand in area i [MW]
P_L	Transmission line losses [MW]
B_{ij}	Transmission loss coefficients
E_i	Emission of a generator i[kg]
a_i, b_i, c_i	Quadratic cost coefficient for generator I
$\alpha_i, \beta_i, \gamma_i$	Emission coefficients for CO_2, NO_x, SO_2
λ	Lagrange multiplier
N	Number of areas
R_u, R_d	Ramp up and ramp down limits[MW/min]
h	Price penalty factor

CHAPTER ONE INTRODUCTION

1.1 Awareness of the research problem.

Economic dispatch is essential to the operation of power systems, and its primary objective is to allocate power to consumers at minimum cost, subject to system constraints. (Wood & Wollenberg, 2012). This is Static Economic Dispatch (SED) if the dispatching time interval is a single time period, and Dynamic Economic Dispatch (DED) if the dispatching time interval spans multiple, continuous time periods. However, more research has shown that the use of ED in power can be more accurate and practical for monitoring system behaviour. (Cheng & Zhang, 2014).

Prior to the discovery of various alternative energy sources, the economic dispatch problem involved only conventional thermal energy generation. Due to a sudden rise in traditional energy sources, such as coal and oil, and atmospheric gases, several nations have supported research on renewable energy applications to diversify energy sources. Wind is one of the alternative energy sources among these projects. One MAWTEED study of interest is MADED (Multi-Area Dynamic Economic Dispatch). A publication (Soroudi & Rabiee, 2013) associated with this research is MADED: Multi-Area Dynamic Economic Dispatch. MADED considers wind power uncertainties, a power pool market, and hydrothermal generating units in each area, and utilizes Optimal Condition Decomposition (OCD) with parallel computing. It is implemented for two interrelated power resources. The successful implementation of a multi-area power system ensures continuous power availability. However, the frequency fluctuates slightly due to greater interconnected power system deviations and variations in power transmission to other sub-areas. This can be achieved by interconnecting tie-lines between the sub-areas, as shown in Figure 1.1. Also, the use of thermal units that can be used as reserves (Up-Spinning reserves (USR) and Down Spinning Reserve (DSR) to compensate for the wind uncertainties.

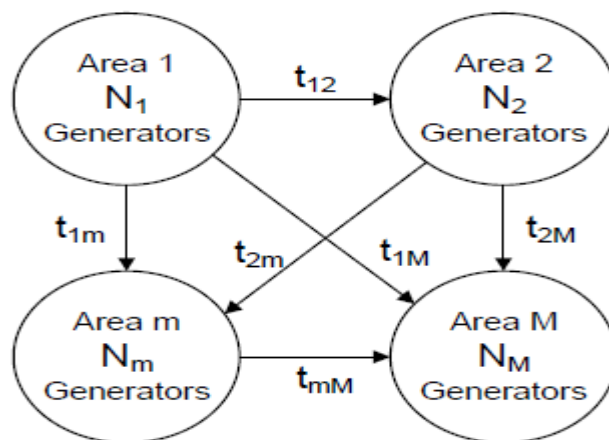


Figure 1.1: Model of a multi-area power system with tie-line power transfer

(Krishnamurthy & Tzoneva, 2016)

Where

N_m	The number of generators belonging to the area m
M	A number of interconnected areas
t_{1m}	Number of tie-lines from area 1 to area M
t_M	Number of tie-lines connecting areas

Environmental problems and fuel consumption can be reduced significantly with renewable energy sources. (Liang et al., 2015). However, the uncertainties in wind speed and its uncontrollability create uncertainty in wind power production. Wind power is fundamentally stochastic compared to other conventional energy sources, meaning its use must be evaluated at a larger, more aggregate scale within complex systems. In this regard, (Xia & Elaiw, 2010) Also offers a survey of mathematical optimization solutions that have addressed the problem involving distributed generation resources with effective results, such as the lambda iterative method, Lagrange relaxation, as well as Artificial Intelligence methods, which consist of artificial neural networks, Genetic Algorithm (GA), Simulated Annealing (SA), Evolutionary Programming (EP), Particle Swarm Optimization(PSO).

(Jeyakumar et al., 2006), done a comparison study of PSO with other optimization methods in different types of Economic dispatch (ED). It was observed that PSO convergence was better than that of Classical Evolutionary Programming (CEP) for MAED. It is simple and easy to converge to the global optimum. This algorithm can be used to determine the optimal power allocation of generating units in each area.

The MAWTEED problem has many variables, nonlinear equations, and high dimensions, making calculations very complex. The MAWTEED problem can be very complex; hence, it is necessary to formulate the problem and develop an algorithm and software to solve it using the Lagrange decomposition method.

The MAWTEED is solvable via the Lagrange decomposition coordinating approach, which is one of the optimal methods for parallelizing a solution. It takes a larger, overall problem and creates sub-problems whose solutions, when added together, equal the overall solution; thus, optimality is preserved.

Based on the above, this thesis investigated a solution to the problem for MAWTEED using the decomposition method

1.2 Statement of the research problem

Replacing thermal generating units with renewable energy sources (RES) reduces atmospheric gas emissions and fuel consumption(Wang & Singh, 2007). However, wind plants provide much more uncertain capacity than thermal generating units and

are much more nonlinear, making predictions for generation output less certain. Therefore, an electric power system largely depends on thermal generation for the time being. The integration of wind turbines with existing thermal generating units can pose challenges for power system balancing. If wind power is available, it can reduce the need for conventional generating capacity, freeing it for reserve purposes. On the other hand, if there is a sudden reduction in wind power, it directly affects the system frequency between generation and load. Wind energy can significantly shorten the lifespan of thermal generators, while these units play a vital role as reserves to compensate for wind uncertainties. Therefore, wind and thermal generation coordination constitutes a more complex optimization problem for creating a cost-effective dispatch schedule.

Power systems are interconnected because interconnected areas are more reliable and can be operated at a lower cost than isolated areas. A change in load demand in one area can be accommodated by interchanging power between the regions via tie lines. Suppose a generating unit is lost in one of the interconnected areas. In that case, the connected regions increase their power outputs to compensate for the lost plant until the reserve or standby generator is brought into service.

It is necessary to address the difficulties above using methods applicable to the conditions of deregulated power system operation and to reduce the complexity and data communication between interconnected systems.

The research problem can be divided into the following sub-problems.

- Design-based sub-problems
- Implementation sub-problems.

1.3 Design-based problems

1.3.1 Sub-problem 1: Literature review of the different problems relative to the single area and the MAWTEED problem.

1.3.2 Sub-problem 2: Mathematical formulation of the single area and MAWTEED problem relative to the quadratic fuel cost of thermal generators and the Weibull probability distribution function of wind generation.

1.3.3 Sub-problem 3: Mathematical formulation of the single area WTEED problem relative to Lagrange's method.

1.3.4 Sub-problem 4: Mathematical formulation of the PSO method relative to the single area WTEED Problem.

1.3.5 Sub-problem 5: Mathematical formulation of the decomposed-coordinating Lagrange method relative to how to solve the MAWTEED Problem.

1.3.6 Sub-problem 6: Mathematical formulation of PSO relative to how to solve the MAWTEED Problem.

1.4 Sub-problems of implementation

1.4.1 Sub-problem 1: Software Implementation relative to Lagrange's methods to solve the WTEED Problem based on the quadratic fuel cost of thermal generators and the Weibull Probability Distribution function of wind power generators.

1.4.2 Sub-problem 2: Software Implementation relative to the PSO method for the single area WTEED Problem based on quadratic fuel cost of thermal generators and Weibull probability distribution function of wind plants.

1.4.3 Sub-problem 3: Software Implementation relative to Lagrange's decomposition-coordinating method to solve the MAWTEED Problem based on the quadratic fuel cost of thermal generators and the Weibull probability distribution function of wind turbines

1.4.4 Sub-problem 4: Software Implementation relative to the PSO algorithm to solve the MAWTEED Problem.

1.5 Research aim and objectives

1.5.1 Research Aim

- The research aim focuses on developing the methods and algorithms for the wind-thermal economic emission dispatch problem solution for single and multi-area power systems. Develop a decomposition-coordinating method for the solution of the multi-area dispatch problem using Lagrange's algorithm. The software is implemented sequentially on one computer.

1.5.2 Objectives

- To survey the literature of already existing problem formulation, techniques, and algorithms of wind-thermal, wind-diesel, wind-PV, and hydrothermal economic dispatch problems.
- To mathematically formulate the wind-thermal economic emission dispatch problem with constraints for single-area and multi-area power systems.
- To develop the Lagrange's method for the wind-thermal economic dispatch problem for both single area and MAWTEED.
- To create a Particle Swarm Optimisation (PSO) method for both single area and MAWTEED.
- To develop MATLAB software for the developed Lagrange's and PSO methods for the wind-thermal economic dispatch problem for the single area power system.

- To develop MATLAB software for the Lagrange's and PSO methods for the wind-thermal economic dispatch problem for multi-area power systems through decomposition.
- To test the developed software for the standard IEEE benchmark models and compare the results with the ones already existing in the literature.

1.6 Hypotheses

The hypotheses related to the applicability of methods and algorithms to solve the single-area and multi-area wind-thermal dynamic economic dispatch problem have been investigated and can be stated as:

- The Weibull probability density function represents the best fit for the wind power plant formation. The quadratic fuel cost curve is assumed for the conventional generators (Coal, gas, and hydro plants).
- The methods and algorithms of the economic dispatch problem are based upon classical, heuristic, and hybrid optimization techniques, which ascertain that the hybrid algorithm possesses computational efficiency, providing better solutions and ease of implementation in practical applications.
- The recent findings of the multi-area dispatch problem postulate that the decomposed complex nature of dispatch problems for a vast interconnected area does, in fact, provide a solution concerning tie-line powers of the interconnected system.
- The Lagrange method has been developed for the economic emission dispatch problem for single-area dispatch purposes, and subsequently, the dispatch problem for multi-area dispatch has been created.
- The PSO method has also been developed and tested for both single-area and multi-area dispatch applications.
- Finally, results comparison can be made between the two developed methods (Lagrange's PSO).

1.7 Delimitation of the research

The thesis focuses on classical and heuristic methods for solving the single- and multi-area emission economic dispatch problem. The boundary conditions of the MAWTEED problem considered in this thesis are as follows:

- Wind-PV, Diesel-thermal, and hydrothermal economic dispatch problems are not considered in this research work. The wind-thermal economic emission dispatch

problem is formulated and implemented using classical and heuristic optimization methods.

- The hybrid optimization method is not considered in this research work. The classical (Lagrangian) and heuristic (PSO) methods are used to solve the single- and MAWTEED problems.
- The cubic cost function model of the conventional economic dispatch problem cannot be considered. The quadratic cost function is used to formulate the traditional economic dispatch problem.
- The decomposition-coordinating method is used to solve the complex multi-area economic emission dispatch problem. For the single-area economic emission dispatch problem, the decomposition-coordination method is not applicable without tie-line powers.

1.8 Motivation of the research

- Most of the electricity is currently generated by thermal plants. These plants affect communities in different ways. Firstly, the gases that are discharged, i.e., CO_2 , and NO_x are affecting global warming. Secondly, the raw material used is expensive.
- Other generating units like hydro power are better than fossil-fuel, because they use rainwater. However, they have drawbacks, such as the location of these plants being far from load centres and the need for long transmission lines to transport power over long distances, which adds to the cost of building new transmission lines for interconnected systems.
- The integration of renewable energies into the existing thermal plants can reduce the difficulties mentioned above. These renewables include wind, solar, and other sources, and they use natural gas to generate electricity. The problem with these energies is that they are less controllable than other generating units. The interconnection of thermal and wind renewable energy reduces the cost of production, maximizes reliability, and provides better operating conditions, such as reserve sharing and improved stability.
- Given the literature review, the following is true. Few decomposition-coordination approaches exist to solve the MAWTEED problem; therefore, the new area of deregulated economic dispatch for interconnected systems warrants exploration. In addition, other techniques and existing software enable the MAWTEED problem to be solved on a single computer. Therefore, this project constructs the MAWTEED problem and solves it with a Lagrange decomposition-coordination approach.

1.9 Assumption

The assumptions are made as follows:

- Each area's power demand is equal to the summation of wind power and thermal power.
- The network losses must be considered; however, in terms of distance, the greater the distance, the more power lost.
- The conventional generators have a minimum and maximum output power, i.e., no power plant will be utilized due to fluctuations in wind generation output.
- A quadratic cost function exists as a convex second-order function.
- The system operator owns the wind generators; thus, the expected cost of wind-generated output does not need to be factored into the cost function.
- Uncontrollability of wind power needs to account for over- and under-generation of wind power estimates in the cost function (Hetzer et al., 2008)
- Tie line constraints should be included in the MAWTEED problem.
- The number of areas in the interconnected power system is based on the IEEE benchmark models found in the literature.
- The MAWTEED problem is solved sequentially.
- The number of tie-lines must be calculated using (Krishnamurthy & Tzoneva, 2016).

Where

M =total number of areas

N_T =Number of tie-lines

- Smaller stop size provides the global solution for the search problem using either classical or heuristic optimization methods

1.10 The deliverables of the thesis

The primary deliverables of the study can be categorized as follows:

- An assessment of the literature on the single-area and multi-area economic emission dispatch problem comparatively.
- Mathematical formulation of the economic dispatch problem
- Formulation of the single area Wind-Thermal Economic Emission Dispatch (WTEED) problem with a quadratic fuel cost function and Weibull Distribution Function (WDF) based wind power.
- Formulation of the MAWTEED problem with a quadratic fuel cost function and WDF-based wind power.
- Optimization methods developed to solve the economic emission dispatch problems
- Development of Lagrange's methods for the solution of the single area WTEED problems.
- Created optimization methods to solve the economic emission dispatch problems

- Developed Lagrange's methods to solve the single area WTEED problems.
- Developed the PSO method to solve the single-area WTEED problem.
- Developed Lagrange's decomposition-coordinating method to solve the MAWTEED problem.
- Developed the PSO method to solve the MAWTEED problem.
- Created software to solve the economic emission dispatch problems in the single-area and multi-area cases
- Software was created based on Lagrange's methods and subsequent algorithms to solve the single-area WTEED problems.
- Software was created based on the PSO method and subsequent algorithms to solve the single-area WTEED problems in a sequential approach.
- Software was created based on Lagrange's decomposition-coordinating method to solve the MAWTEED problem.
- Software was created based on the PSO method to solve the MAWTEED problem.
- Software was created for the standard IEEE benchmark problems, and results were compared to those found in other literature.

For the summary of these contributions to the study, see Chapter 7.

1.11 Chapter breakdown

This study comprises seven chapters, and they are structured as follows:

Chapter 1 highlights the problem statement and the study's background. The study's aim and objectives, problem description, hypothesis, research delimitation, and assumptions are included in the thesis statement.

Chapter two documents the literature about the single-area and multi-area economic emission dispatch problems. It documents what is known about the economic emission dispatch problem and the pros and cons of different heuristic, hybrid, classical, and metaheuristic algorithms for solving it.

Chapter three formulates the Wind-Thermal Economic Emission Dispatch (WTEED) single-area problem with a quadratic fuel cost function and a Wind Distribution Function (WDF) for wind. Furthermore, the methodology for the single-area economic emission dispatch problem using Lagrange's method is established. Three different IEEE test benchmark models were simulated in MATLAB for the algorithms.

Chapter four formulates and explains the PSO algorithm for the WTEED single-area problem. Three different IEEE test benchmark models were simulated in MATLAB for the algorithms.

Chapter five formulates and establishes Lagrange's method for the Wind-Thermal Economic Emission Dispatch problem in the multi-area context with a quadratic fuel

cost function and WDF for wind. Three different IEEE test benchmark models were simulated in MATLAB for the algorithms.

Chapter six formulates and establishes PSO for the Wind-Thermal Economic Emission Dispatch problem in the multi-area context with a quadratic fuel cost function and WDF for wind. Three different IEEE test benchmark models were simulated in MATLAB for the algorithms.

Chapter 7 discusses the study's conclusions and deliverables. The results of the study, future work, and a listing of the author's published papers comprise the conclusion.

1.12 Conclusion

This chapter presents the research need, research aim, objectives, problem statement, background, rationale, assumptions, and hypothesis. The reader will be given a brief overview of the study's findings here, with a more detailed discussion reserved for Chapter Seven. Thus, this chapter reflects on the relevance of the study, based on findings from single- and multi-area wind-thermal economic emission dispatch problems. Furthermore, it supports the thesis's Literature Review in Chapter Two, demonstrating that the comparison of different approaches/algorithms to solve single- and multi-area problems is justified.

CHAPTER TWO LITERATURE REVIEW

2.1 Introduction

Electric power is essential to human survival in day-to-day life and serves as a driving force for many economic sectors. Conventional generation has been the sole method of provision of electric power for decades. Conventional generation exposes many cost and emission disadvantages.

This chapter introduces various optimisation strategies and algorithms for the economic emission dispatch problem, considering wind-thermal systems in a multi-area context. The optimisation methods are either search or gradient-based, as shown in Figure 2.1. The various formulations of the economic dispatch problem in the literature can be grouped into single-area and multiple-area dispatch, as illustrated in Figure 2.2.

The aim of this chapter is to investigate the solutions to single- and multi-area economic dispatch problems in the literature. This is organised in such a way that there are three types of solutions to the economic dispatch problem: 1) the single-area wind-thermal problem; 2) the single-area hybrid renewable energy resources problem; 3) the multi-area economic dispatch problem.

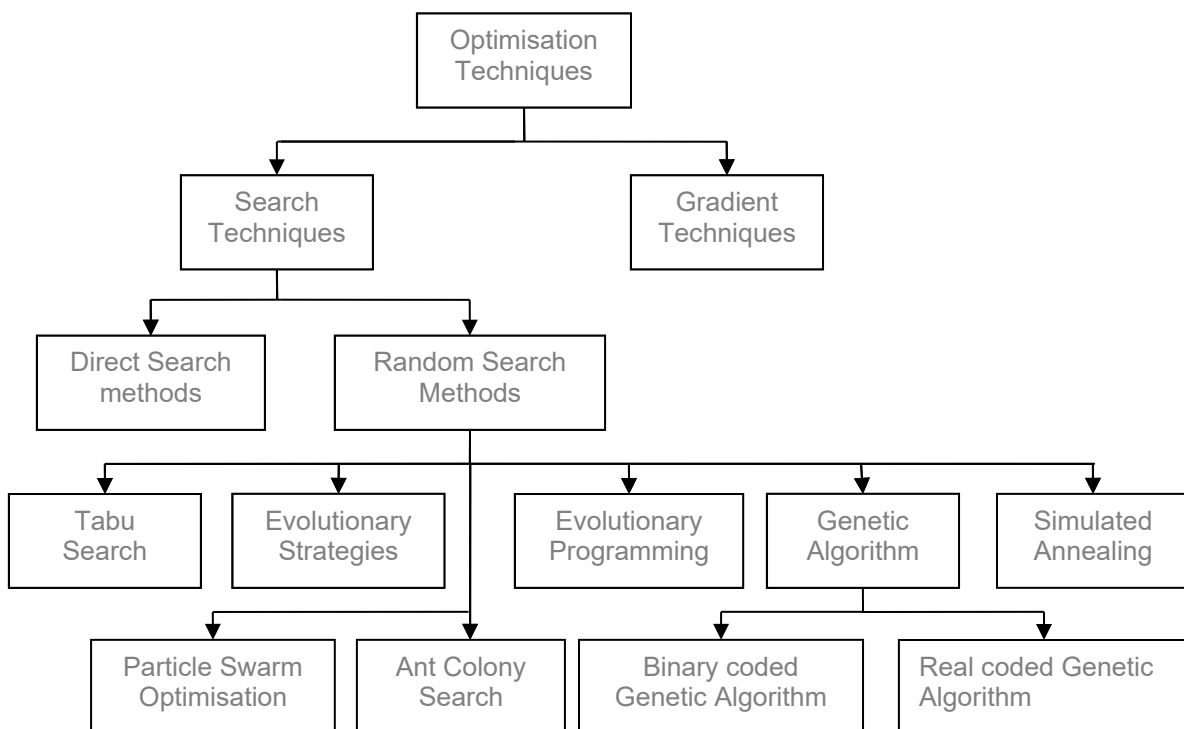


Figure 2.1: Organisation of optimisation techniques (Kothari & Dhillon, 2012)

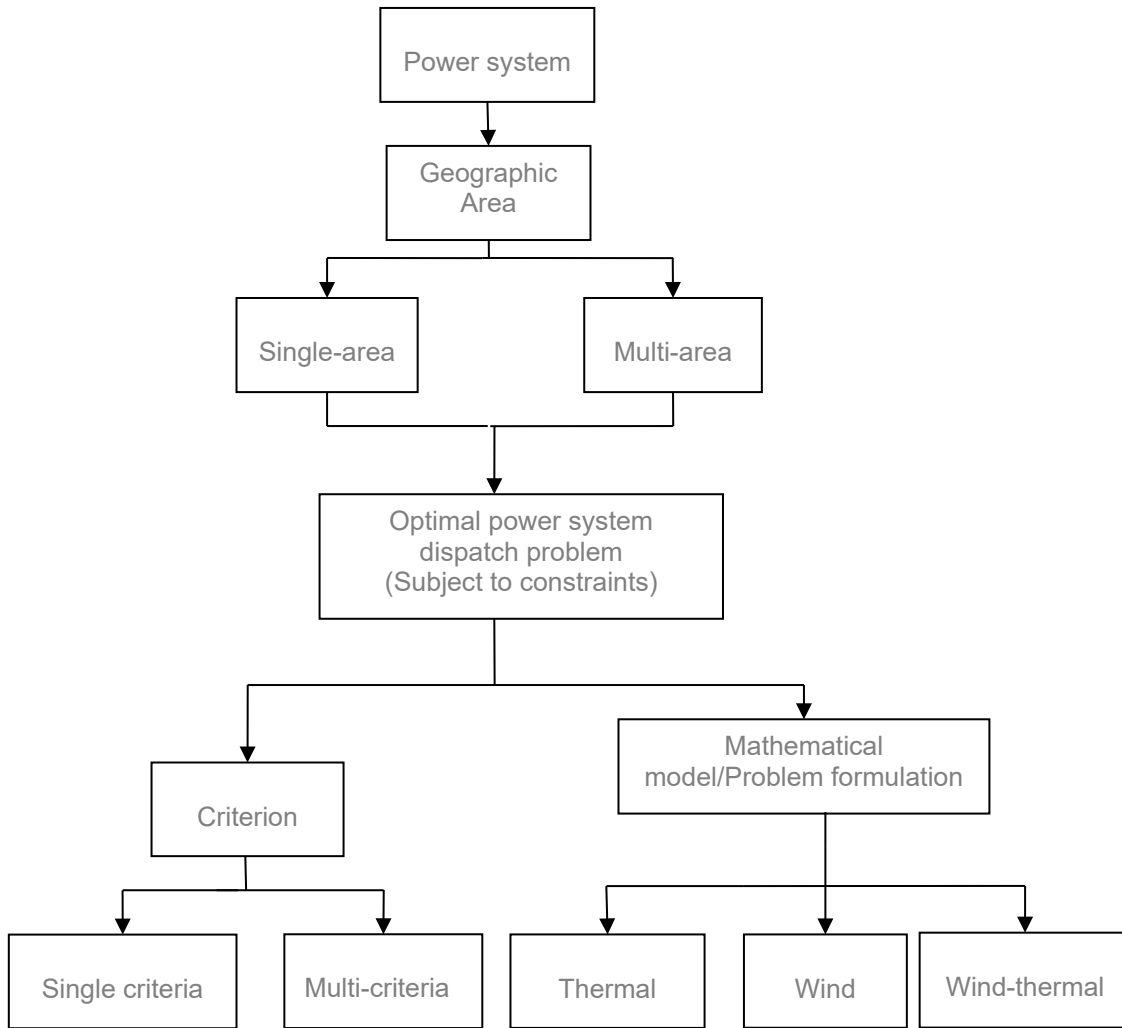


Figure 2.2: Single-area and Multi-area power systems dispatch problem organisation

2.2 Wind-thermal economic dispatch

The goal of the wind-thermal economic dispatch is to share power among conventional and renewable generating units and to minimize total operating cost, subject to equality or inequality design constraints. The time-varying wind-thermal economic dispatch is equivalent to a single-area and multi-area economic dispatch. The non-linear objective function can be a single or a two-objective function. One of the fundamental barriers to incorporating wind power into conventional economic dispatch is the uncontrollable, unpredictable nature of wind speed. Wind speed variability can best be modeled by a two-parameter Weibull probability density function, the most effective and reliable means(Jiang et al., 2015).

2.2.1 Problem formulation for single area wind-thermal economic dispatch

2.2.1.1 Problem formulation for single-criterion economic dispatch.

In this part of the chapter, the problem statement of the wind-thermal economic dispatch problem with a single criterion function is given. The cost function for dynamic economic dispatch (DED) determines the minimum total operating cost of the entire generation system, subject to operational constraints. The total cost that the conventional and wind generators can represent is given by (Ghasemi et al., 2016).

$$F(P_g, P_w) = \sum_{i=1}^{N_G} F_i(P_{gi}) + \sum_{j=1}^{N_F} \sum_{k=1}^{N_w} W_{j,k}(P_{w_{j,k}}) \quad [$/h] \quad (2.1)$$

Where

$F(P_g, P_w)$ Total cost of all generating units

N_G Number of thermal generators

N_F Wind farm

N_w Number of wind generators

The cost function of the thermal generator units is derived from a quadratic equation with valve-point loading effect, which is noted in (2.2) (Kothari & Dhillon, 2012). The thermal cost function can be with or without valve-point loading, as illustrated in Figure 2.3.

$$F_i(P_{gi}) = a_i + b_i P_{gi} + c_i P_{gi}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi}))| \quad [$/h] \quad (2.2)$$

where $a_i, b_i,$ and c_i is the fuel cost coefficient of the i^{th} generator and e_i and f_i are valve point coefficients. The last term $W_{j,k}(P_{w_{j,k}})$ Equation (2.1) represents the output power of the wind-generating units. This term can be defined using equation (2.3) (Hetzer et al., 2008).

$$W_{j,k}(P_{w_{j,k}}) = \varphi_{D_{j,k}} P_{E_{j,k}} + \varphi_{OE_{j,k}} \times (P_{A_{j,k}} - P_{E_{j,k}}) + \varphi_{UE_{j,k}} \times (P_{E_{j,k}} - P_{A_{j,k}}) \quad [$/h] \quad (2.3)$$

where

$P_{E_{j,k}}$ Expected wind power generation of the turbine j in a wind farm k [MW]

$P_{A_{j,k}}$ Actual/available wind power generation of the turbine j in a wind farm k [MW]

$\varphi_{D_{j,k}}$ Direct cost coefficient of the wind turbine j in a wind farm k [\$/MWh]

$\varphi_{OE_{j,k}}$ Overestimation cost coefficient of the turbine j in a wind farm k [\$/MWh]

$\varphi_{UE_{j,k}}$ Underestimation cost coefficient of the turbine j in a wind farm k [\$/MWh]

The thermal cost function is established with or without valve point loading (see Figure 2.3). Most economic dispatch studies address the combined economic emission dispatch problem from a linear-quadratic perspective, an idealization, since the incremental cost curves of generation units are assumed to be piecewise linear and continuously increasing. However, the actual input-output curves of thermal generating units are highly nonlinear, with fuel cost curves exhibiting valve-point loading. For instance, (Gernald & Aaron, 1958) demonstrate that valves permit economic adjustment in parallel turbines' loadings with one turbine operable under governor control for slight load demand adjustments so that power generation meets up-to-par standards with no incremental cost adjustments needed. But in actuality, a multitude of steam valves exist within generating stations. Thus, the thermal cost function, including the valve-point effect, is a truly nonlinear function that captures the true nature of the dynamic wind-thermal economic dispatch problem and thus operates within the cost function.

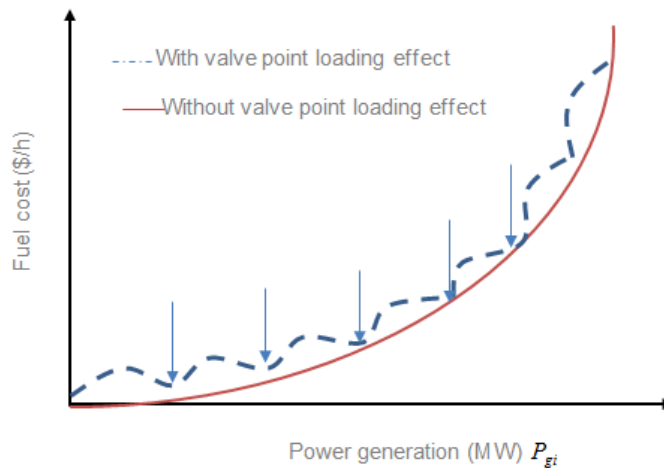


Figure 2.3: Conventional cost curve with/without VPLE(Ghasemi et al., 2016)

Equality constraints

(a) Real power balance constraints

The generated power of wind and thermal units is equal to power demand plus line losses and can be represented mathematically as in (2.4)(Ghasemi et al., 2016).

$$\sum_{i=1}^{N_G} P_{gi} + \sum_{k=1}^{N_W} P_{wh,j,k} = P_D + P_{Loss} \quad [\text{MW}] \quad (2.4)$$

where

P_D Total load demand of the power system

P_{Loss} Transmission line losses of the power system

In electric power transmission systems, losses are generated due to transmission over long distances. Thus, relative to low-load-density areas, across vast spaces, and in wind-thermal dynamic economic dispatch modeling, it is important to consider transmission losses. According to (Huang et al., 2018) The formula for transmission loss includes the term defined by the first quadratic term of equation (2.3), later referred to as George's formula. This is referred to as the loss formula or B-coefficient method. In addition, a linear term and a constant are added to the quadratic to provide a more accurate representation of transmission losses. According to (Huang et al., 2018), This is known as Kron's formula and is shown in equation (2.5) (Jiang et al., 2015). The B-coefficient method retains losses that could be avoided if each plant output were better scheduled based on the expected economic appeal to the projected load.

$$P_L = \sum_{m=1}^{N_G+N_W} \sum_{m'=1}^{N_G+N_W} P_m B_{mm'} P_{m'} + \sum_{m=1}^{N_G+N_W} B_{om} P_m + B_{00} \quad [\text{MW}] \quad (2.5)$$

where

m and m' Wind-thermal generator capacity

$B_{mm'}$, B_{om} and B_{00} Loss of generation factors

The objective function expressed in (2.1) is subjected to the following inequality constraints.

Inequality Constraints

(a) Generation capacitor upper limits

The supply power of each generating unit in operation should not surpass the upper and lower limits of an operational unit, as stated in Equation (2.6).

$$\begin{aligned} P_{gi}^{\min} &\leq P_{gi} \leq P_{gi}^{\max}, i = 1, 2, \dots, N_G \\ 0 &\leq P_{R,j,h} \leq P_{R,j,h}, j = 1, 2, \dots, N_w \end{aligned} \quad (2.6)$$

where

P_{gi}^{\max} Maximum output power of the i^{th} thermal generating unit

P_{gi}^{\min} Minimum output power of the i^{th} thermal generating unit

$P_{R,j,h}$ Rated power of j^{th} wind output generator

(b) Ramping up /down constraints

All online units have a limit to their operating range due to the ramping rate of an individual unit (Kothari & Dhillon, 2012). The generator can operate in three regions: steady-state operation, unit increasing its power output, and unit decreasing its power output. These regions can be represented diagrammatically by Figure 2.4.

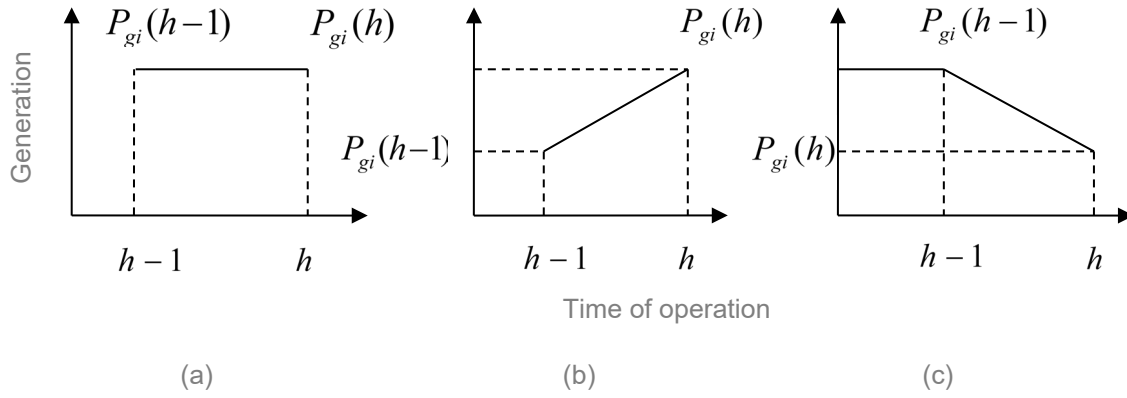


Figure 2.4: Ramp rate limits of a generating unit (Kothari & Dhillon, 2012)

Figure 2.4(a) represents steady state operation. Figure 2.4(b) shows the unit increasing its power output. Figure 2.4(c) depicts the unit decreasing power output. The operating boundaries are defined by Equation (2.7)

$$\begin{cases} -R_i^D \leq (P_{gi,h} - P_{gi,h-1}) \leq R_i^U, & \text{if } P_{gi,h-1} \geq P_{gi}^{\min} \\ R_i^0 \leq |P_{gi,h} - P_{gi,h-1}| \leq R_i^1, & \text{if } 0 < P_{gi,h-1} < P_{gi}^{\min} \end{cases} \quad (2.7)$$

Where

R_i^D Minimum ramping down rate

R_i^U Maximum ramping up rate

R_i^0 Lower limit of the variation rate

R_i^1 Upper limit of variation rate

(c) Minimum on/off constraints

These constraints denote the minimum time the generating unit must be committed once it starts up, and the minimum time it must be de-committed once it is shut down.

The minimum on/off constraints are presented as given in equation (2.8)

$$\begin{cases} [T_{i,h-1}^R - T_{\min}^R][s_{i,h-1} - s_{i,h}] \geq 0 \\ [T_{i,h-1}^S - T_{\min}^S][s_{i,h} - s_{i,h-1}] \geq 0 \end{cases} \quad (2.8)$$

Where,

$T_{i,h-1}^R$ Continuous online time

$T_{i,h-1}^S$ Continuous Offline time,

T_{\min}^R Minimum online time

T_{\min}^S Minimum offline time

$s_{i,h}$ Operating status of the i^{th} thermal generator

(d) Prohibited operating zone

The prohibited operating zones of the input-output characteristic curve for a conventional generator are as follows: vibration of the shaft bearing due to the steam valve, or due to machine malfunction, or malfunction of other ancillary components of the generator. Moreover, it's almost impossible to determine the real input-output characteristics curve near a prohibited zone from actual input-output testing or operational data (Kothari & Dhillon, 2012). These conditions are the ones in Equation (2.9) and are depicted in Figure 2.5.

$$\left\{ \begin{array}{l} P_{gi}^{\min} \leq P_{gi} \leq P_{gi,1}^L \quad (i = 1, 2, \dots, N_G) \\ P_{gi,j-1}^U \leq P_{gi} \leq P_{gi,j}^L \quad (j = 2, 3, \dots, Nz_i) \text{ and } (i = 1, 2, \dots, N_G) \\ P_{gi,Nz_i}^U \leq P_{gi} \leq P_{gi}^{\max} \quad (i = 1, 2, \dots, N_G) \end{array} \right\} \quad (2.9)$$

Where

Nz_i Number of prohibited zones of i^{th} thermal generating unit

$P_{gi,j}^L$ Lower bound of the j^{th} prohibited zone of the i^{th} thermal generating unit

$P_{gi,j-1}^U$ Upper bound of j^{th} prohibited zone of the i^{th} thermal generating unit

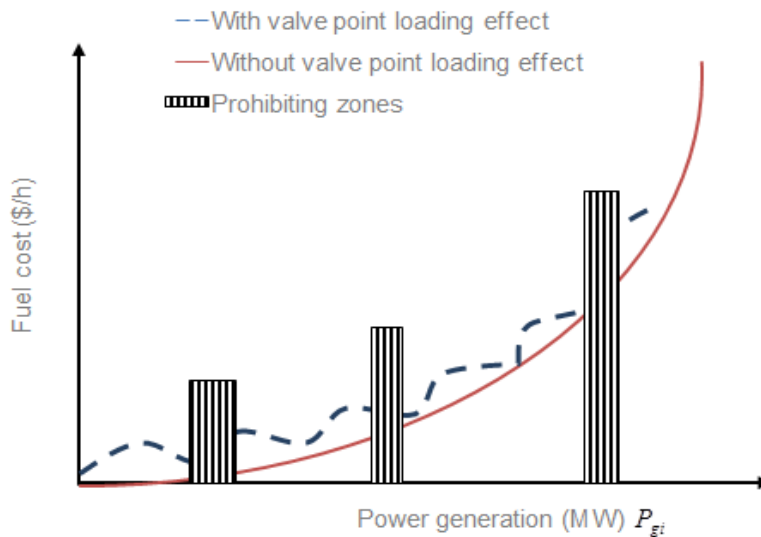


Figure 2.5: Effective cost attributes with restricted operational zones (Kothari & Dhillon, 2012)

(f) Wind Power constraints

The total power available from a wind turbine is equal to the product of the mass flow rate $\frac{dm}{dt}$, air density ρ , speed v and the blades swept the cross-sectional area A (Masters, 2004). Therefore, the wind turbine's output power is given by Equation (2.10).

$$P_w = \frac{\rho A v^3}{2} \quad [\text{MW}] \quad (2.10)$$

The power curve shown in Figure 2.5 is the power the wind turbine will produce as a function of turbine height and wind speed. Thus, the data related to this curve will dictate how much output power will be generated by this wind turbine and how much wind energy will be produced. The turbine curve shown in Figure 2.6, however, comprises three performance regions: the cut-in wind speed, the rated wind speed, and the cut-out/furling wind speed.

where

V_C	Cut in wind speed	[m/s]
V_R	Rated wind speed	[m/s]
V_F	Cut out or Furling wind speed	[m/s]

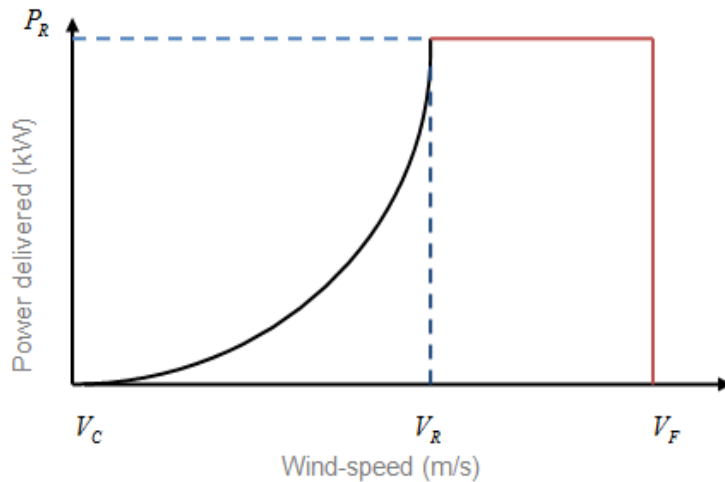


Figure 2.6: A power curve for a general wind turbine (Masters, 2004)

The wind generation output power as a function of wind speed is represented through a simplified linear piecewise function, which is given in equation (2.11) (Qu et al., 2016)

$$\begin{cases} P_w = 0, & v < v_C \text{ or } v > v_F \\ P_w = P_R \frac{v - v_C}{v_r - v_C}, & v_C \leq v \leq v_R \\ P_w = P_R, & v_R \leq v \leq v_F \end{cases} \quad [\text{MW}] \quad (2.11)$$

where

P_w	Power delivered by a wind turbine	[MW]
P_R	Rated power	[MW]
V_C	Cut in wind speed	[m/s]
V_R	Rated wind speed	[m/s]
V_F	Cut out or Furling wind speed	[m/s]

(i) Wind power probability density function (PDF)

Representing short-term wind speeds is important for assessing wind energy potential. PDFs are commonly used to assess wind speed. The applicability of various PDFs has been assessed in several regions worldwide. Since wind power is calculated as a simple function of wind speed distribution parameters, choosing a probability density function is important to the study of wind energy.

Using a PDF that better represents the wind speed data reduces the approximation error associated with uncertain wind power predictions. The Weibull two-parameter PDF and the Rayleigh PDF are the two most common PDFs when assessing wind speed data. In the literature, the Weibull PDF has been used to model wind speed data to solve the wind-thermal economic dispatch problem. The Weibull PDF retains several advantages over other probability distributions. For its many advantages, it requires only the estimation of two parameters and has a positively skewed probability density function that favours average wind speeds. Historically, it has proven a good fit for real-world wind speed data. If the Shape and Scale parameters are known at one height, a procedure exists to determine their equivalents at another height.

The Rayleigh PDF is a one-parameter distribution, a special case of the two-parameter Weibull PDF. A shape parameter of 2 can also be used. Many PDFs have been used in the literature to represent wind speed conditions, but for solving the economic dispatch problem of wind intermixed with gas units, the Weibull PDF is most commonly used.

The wind speed at a specific location can be assessed as a Probability Density Function (Masters, 2004) and is illustrated in Figure 2.7. The probability density function is given by $f(v)$, where v is defined as the wind speed. The area under the curve equals one, and this area under the curve equals the probability that the wind speed is equal to between v_1 and v_2 .

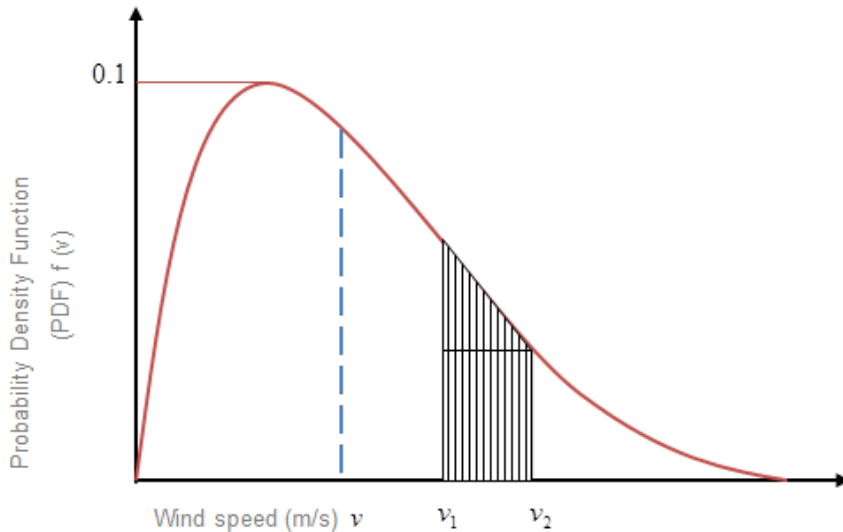


Figure 2.7: Wind velocity Probability Density Function (PDF) (Masters, 2004)

The PDF can be represented mathematically as given in Equations (2.12) and (2.13) respectively (Masters, 2004).

$$P(v_1 \leq v \leq v_2) = \int_{v_1}^{v_2} f(v) dv \quad (2.12)$$

$$P(0 \leq v \leq \infty) = \int_0^{\infty} f(v) dv = 1 \quad (2.13)$$

The PDF can be represented using the Weibull Probability Density Function (wpdf) (Masters, 2004) and is given in Equation (2.14).

$$f(V) = \frac{k}{c} \left(\frac{V}{c} \right)^{k-1} e^{-(V/c)^k} \quad 0 \leq V < \infty \quad (2.14)$$

Where

c Scale parameter at a given location [m/s]

k Shape parameter at a given location (dimensionless).

(ii) Cumulative Weibull distribution function (cdf)

The probability that the wind speed is less than some specified wind speed V and is given in Equation (2.15), and it is called a cumulative distribution function (Masters, 2004)

$$P(v \leq V) = F(V) = \int_0^V f(v) dv \quad (2.15)$$

Where

V Wind speed is a random variable

Wind speed

The cumulative distribution function of wind speed is given by Equation (2.16).

$$F(V) = P(v \leq V) = \int_0^V \left(\frac{k}{c} \left(\frac{V}{c} \right)^{k-1} e^{-(V/c)^k} \right) dV \quad (2.16)$$

Where

To solve Equation (2.16), let's assume the new integration variable $x = \left(\frac{V}{c} \right)^k$. The

limits of the integral $V = 0$ and $V = x$, become $x = 0$ and $x = \left(\frac{V}{c} \right)^k$. Differentiating the

definition of $x = \left(\frac{V}{c} \right)^k$ with respect V result to $dx = \frac{k}{c} \left(\frac{V}{c} \right)^{k-1} dV = \frac{kV^{k-1}}{c^k} dV$ and

$dV = \frac{c^k}{kV^{k-1}} dx$. Substituting the definition of x , the new limits, and the formula for

dV into Equation (2.16). Finally, all mathematical representation and resultant cumulative wind probability density function is given in Equation (2.17)

$$\begin{aligned} F(V) = P(v \leq V) &= \int_{V=0}^{V=x} \left(\frac{k}{c} \left(\frac{V}{c} \right)^{k-1} e^{-(V/c)^k} \right) dV = \int_{x=0}^{x=\left(\frac{V}{c}\right)^k} \left(\frac{kV^{k-1}}{c^k} e^{-x} \frac{c^k}{kV^{k-1}} \right) dx \\ &= \int_0^{\left(\frac{V}{c}\right)^k} e^{-x} dx = -e^{-x} \Big|_0^{\left(\frac{V}{c}\right)^k} = 1 - \exp\left(-\left(\frac{V}{c}\right)^k\right) \end{aligned} \quad (2.17)$$

If there is a probability that the wind speed exceeds a certain threshold, then the cumulative distribution function can be defined as in Equations (2.18) and (2.19).

$$P(v \geq V) = 1 - P(v \leq V) = 1 - F(V) \quad (2.18)$$

$$P(v \geq V) = 1 - P(v \leq V) = 1 - F(V) = 1 - \left[1 - \exp\left(-\left(\frac{V}{c}\right)^k\right) \right] = \exp\left(-\left(\frac{V}{c}\right)^k\right) \quad (2.19)$$

In several applications of the Weibull PDF, statistical moments are required (Altunkaynak et al., 2012). The computations for the mean, variance, and wind power can be simplified by a single integration over the distribution's moments. According to the PDF, the n^{th} moment for any probability density function $f(V)$ is defined by Equation (2.20) (Leon-Garcia, 2008).

$$\begin{aligned}\overline{V^n} &= \int_{V_{\min}}^{V_{\max}} V^n f(V) dV = \int_0^{\infty} V^n \frac{k}{c} \left(\frac{V}{c}\right)^{k-1} e^{-(V/c)^k} dV = k \int_0^{\infty} V^{n-1} \left(\frac{V}{c}\right)^k e^{-(V/c)^k} dV \\ &= k \int_0^{\infty} V^{n-1} x e^{-x} \frac{c}{k} x^{\frac{1}{k}-1} dx = c \int_0^{\infty} \left(cx^{\frac{1}{k}}\right)^{n-1} x^{\frac{1}{k}} e^{-x} dx = c^n \int_0^{\infty} x^{\frac{n}{k}} e^{-x} dx = c^n \Gamma\left(\frac{n}{k} + 1\right), \quad n = 1, 2, \dots\end{aligned}\tag{2.20}$$

Where

Γ is the Gamma function and is given in Equation (2.21)

$$\Gamma(\beta) = \int_0^{\infty} x^{\beta-1} \exp(-x) dx \tag{2.21}$$

Equation (2.20) is obtained precisely the same way as Equation (2.17). The mean and variance of the Weibull function are given in Equations (2.22) and (2.23), respectively.

$$\mu_{Weibull} = \int_{V_{\min}}^{V_{\max}} V f(V) dV = c \Gamma\left(\frac{1}{k} + 1\right) \tag{2.22}$$

$$(\sigma^2 + \mu^2) = \int_{V_{\min}}^{V_{\max}} V^2 f(V) dV = \int_0^{\infty} V^2 \frac{k}{c} \left(\frac{V}{c}\right)^{k-1} e^{-(V/c)^k} dV = \overline{V^2} = c^2 \Gamma\left(\frac{2}{k} + 1\right) \tag{2.23}$$

A continuous or discrete probability distribution defines the wind power curve. (Xian Liu & Xu, 2010). In a continuous probability function, the wind speed is between the cut-in and the rated wind speed. In a discrete probability function, the wind speed is between the rated and furling wind speed, and also where the output power has a constant zero value, i.e., below the cut-in and cut-out wind speed. The mathematical formulation of the continuous and discrete probability functions used to find the total output power of the wind generating units is described in the following section.

(iii) Continuous probability

The difference between continuous and discrete probability is that a constant probability distribution cannot be presented in tabular form; instead, a mathematical representation is used to illustrate a continuous PDF. The mathematical equation that describes continuous probability is called the probability density function and is given in Equation (2.14). It can also be called a density function, PDF, or a PDF. It possesses the following properties.

- The graphical representation of the probability density function is continuous over a particular range.
- The area circumscribed by the curve of the density function and the x-axis is equal to one when calculated over the domain of the variable.

- The probability that a random variable estimates a value between v_1 and v_2 is equal to the area under the density function bounded by v_1 and v_2 .

It is estimated that wind speed has a given distribution, such as the Weibull distribution; it is necessary to transform that distribution into a wind power distribution. This conversion can be achieved as follows, with V as the wind speed is a random variable and P_w is wind power a random variable? According to (Leon-Garcia, 2008) The linear transformation of a random variable P_w , such as the one presented in Equations(2.11) in the interval $v_C \leq v \leq v_R$ is given in Equation (2.24)(Leon-Garcia, 2008)

$$P_w = T(V) = aV + b \quad [\text{MW}] \quad (2.24)$$

Where a is the constant greater than zero, and V has CDF $F_V(v)$, Then we needed to find the CDF of the function $F_{P_w}(p_w)$. For simplicity, let $P_w = Y$ and $V = X$. Then Equation (2.24) becomes $Y = aX + b$ and CDFs of X and Y be $F_X(x)$ and $F_Y(y)$. The event $\{Y \leq y\}$ occurs when $A = \{aX + b \leq y\}$ occurs. If $a > 0$, then $A = \{X \leq (y-b)/a\}$ and If $a < 0$, then $A = \{X \geq (y-b)/a\}$. Then the CDFs of Y be represented by Equations (2.25).

$$\begin{aligned} F_Y(y) &= P\left[X \leq \frac{y-b}{a}\right] = F_X\left[\frac{y-b}{a}\right], a > 0 \\ F_Y(y) &= P\left[X \geq \frac{y-b}{a}\right] = 1 - F_X\left[\frac{y-b}{a}\right], a < 0 \end{aligned} \quad (2.25)$$

The PDF of Y can be obtained by differentiating Equation (2.25) with respect to y and using the chain rule for derivatives $dF/dy = dF/du \times du/dy$.

Where

u Argument of F

After differentiation of Equation (2.25) for both $a > 0$ and $a < 0$, the PDF of the function Y is given in Equations 2.26

$$\begin{aligned} f_Y(y) &= \frac{1}{a} f_X\left[\frac{y-b}{a}\right], a > 0 \\ f_Y(y) &= \frac{1}{-a} f_X\left[\frac{y-b}{a}\right], a < 0 \end{aligned} \quad (2.26)$$

The results in Equation (2.26) can be combined using one equation and is given in Equation (2.27).

$$f_Y(y) = \left| \frac{1}{a} \right| f_X \left[\frac{y-b}{a} \right] \quad (2.27)$$

Using Equation (2.24), and (2.27), the Weibull pdf of the wind power output random variable in the continuous range can be found and is given in Equation (2.28). Firstly, the constants a and b are represented by the following Equations.

$$a = \frac{P_R}{v_R - v_C}, b = \frac{-P_R v_C}{v_R - v_C}$$

The equations for a and b can be read directly from Figure 2.6 between cut-in and rated wind speed. The workout for the equation of the continuous range is as follows

$$\begin{aligned} \left| \frac{1}{a} \right| f_V \left[\frac{w-b}{a} \right] &= \frac{1}{\frac{P_R}{v_R - v_C}} f_V \left[\frac{w + \frac{P_R v_C}{v_R - v_C}}{\frac{P_R}{v_R - v_C}} \right] \\ \left| \frac{1}{a} \right| f_V \left[\frac{w-b}{a} \right] &= \frac{v_R - v_C}{P_R} f_V \left[\frac{w(v_R - v_C) + P_R v_C}{\frac{P_R}{v_R - v_C}} \right] \\ &= \frac{v_R - v_C}{P_R} f_V \left[\frac{w(v_R - v_C) + P_R v_C}{P_R} \right] = \frac{h v_C}{P_R} f_V \left[\frac{h w}{P_R} + 1 \right] v_C \\ h &= \frac{v_R - v_C}{v_C} \end{aligned}$$

Using the Weibull distribution function in Equation (2.14), the PDF in the continuous range is:

$$f_{P_w}(P_w) = \frac{k h v_C}{P_R c} \left[\frac{\left(1 + \frac{h w}{P_R}\right) v_C}{c} \right]^{k-1} \exp \left\{ - \left[\frac{\left(1 + \frac{h w}{P_R}\right) v_C}{c} \right]^k \right\}, v_C \leq v \leq v_R \quad (2.28)$$

(iv) Discrete probabilities

A discrete random variable is a random variable that takes values from a countable set, that is, a finite set $\mathcal{S}_F = \{f_1, f_2, f_3 \dots f_n\}$ (Leon-Garcia, 2008). A simple example that clearly describes the concept of a discrete random variable is a Coin toss. A coin is tossed two times, and the appearance of heads and tails is monitored. The probabilities

of the toss are defined by the following set $S = \{TT, TH, HT, \text{ and } HH\}$, where T and H represents tails and heads, respectively. Let F be the number of tails in the two tosses, and allocate each outcome in S from the $S_F = \{0, 1, 2\}$. The four outcomes and corresponding values F are monitored. Therefore, the discrete random variable takes on values in the set $S_F = \{0, 1, 2\}$. The discrete portion of the wind power output random variable must account for the piecewise-linear properties shown in Equation (2.11). The discrete probability is on intervals where $P_w = 0$ and $P_w = P_R$. The mathematical representation of the two events $P_w = 0$ and $P_w = P_R$ are given in Equations (2.29) and (2.30) separately (Hetzer et al., 2008)

$$\begin{aligned}
\Pr(P_w = 0) &= \Pr(V < v_C) + \Pr(V \geq v_F) \\
&= 1 - \exp\left[-(v_C / c)^k\right] + 1 - \Pr(V < v_F) = 1 - \exp\left[-(v_C / c)^k\right] + 1 - F(V) \\
&= 1 - \exp\left[-(v_C / c)^k\right] + 1 - \left[1 - \exp\left[-(v_F / c)^k\right]\right] \\
&= 1 - \exp\left[-(v_C / c)^k\right] + \exp\left[-(v_F / c)^k\right]
\end{aligned} \tag{2.29}$$

$$\begin{aligned}
\Pr(P_w = P_R) &= \Pr(v_R \leq V \leq v_F) \\
&= \Pr(V \leq v_F) - \Pr(V \geq v_R) \\
&= 1 - \exp\left[-(v_F / c)^k\right] - \left[1 - \exp\left[-(v_R / c)^k\right]\right] \\
&= \exp\left[-(v_R / c)^k\right] - \exp\left[-(v_F / c)^k\right]
\end{aligned} \tag{2.30}$$

(v) Total cumulative distribution function of wind power

The Cumulative Distribution Function (CDF) of wind power is represented by both continuous and discrete probabilities, and is given in equation (2.28) (Xian Liu, 2012). The solution of Equation (2.28) follows several axioms in probability theory (Leon-Garcia, 2008). The axiom allows us to view events as objects that possess a property with attributes similar to those of physical mass. There are three axioms in probability theory, namely, Axiom I, Axiom II, Axiom III, and Axiom IV. Axiom I states that the probability is nonnegative; Axiom II states that there is a fixed total amount of probability, namely 1 unit. Axiom III states that the probability of two disjoint events is the sum of their individual probabilities. Axiom III' is the special case of Axiom III, and is used to handle experiments with infinite sample spaces. These laws are shown mathematically and are given in Equation (2.31) (Leon-Garcia, 2008)

$$\begin{aligned}
\text{Axiom I} & \quad 0 \leq P[A] \\
\text{Axiom II} & \quad P[S] = 1 \\
\text{Axiom III} & \quad \text{If } A \cap B = \emptyset, \text{ then } P[A \cup B] = P[A] + P[B] \\
\text{Axiom III}' & \quad \text{If } A_1, A_2 \dots \text{ is a sequence of events such that} \\
& \quad A_i \cap A_j \text{ for all } i \neq j, \text{ then}
\end{aligned} \tag{2.31}$$

$$P\left[\bigcup_{k=1}^{\infty} A_k\right] = \sum_{k=1}^{\infty} P[A_k]$$

Where

$P[A]$, and $P[B]$ Probability of a random number A and B

S Sample space.

The random variable P_w is a piecewise linear function of V , and several cases need to be considered based on the axioms, laws, and are given in Equations (2.32) to (2.36)(Liu et al., 2021).

Case I

$$\begin{aligned}
P_w &= P_R \\
\Pr(P_w \leq p_w) &= \Pr(P_w \leq P_R) = 1
\end{aligned} \tag{2.32}$$

Case II

$$\begin{aligned}
P_w &> P_R \\
\Pr(P_w \leq p_w) &= \Pr(P_w < 0) + \Pr(P_R < P_w < p_w) \\
&= \Pr(P_w \leq P_R) + 0 = 1
\end{aligned} \tag{2.33}$$

Case III

$$\begin{aligned}
P_w &< 0 \\
\Pr(P_w \leq p_w) &= \Pr(P_w < 0) - \Pr(p_w < P_w < 0) \\
\Pr(P_w \leq p_w) &= 0 - 0 = 0
\end{aligned} \tag{2.34}$$

Case IV

$$\begin{aligned}
P_w &= 0 \\
\Pr(P_w \leq p_w) &= \Pr(P_w \leq 0) = \Pr(P_w < 0) + \Pr(P_w = 0) \\
&= 0 + \Pr(V \leq v_C) + \Pr(V > v_F) = F_V(v_C) + 1 - F_V(v_F)
\end{aligned} \tag{2.35}$$

Case V

$$\begin{aligned}
0 &< P_w < P_R \\
\Pr(P_w \leq p_w) &= \Pr(P_w \leq 0) = \Pr(P_w < 0) + \Pr(0 < P_w < p_w) \\
&= F_V(v_C) + 1 - F_V(v_F) + \Pr(0 < P_w < p_w)
\end{aligned} \tag{2.36}$$

Where

$$\begin{aligned}
\Pr(0 < P_w < p_w) &= \Pr[v_C < V < f_V(P_w)^{-1}] \\
&= F_V(P_w)^{-1} - F_V(v_C)
\end{aligned}$$

By substituting Equation (2.28) to Equation (2.36), the resultant expression is given in

Equation(2.36).

$$Pr(0 < P_w < p_w) = 1 - \exp\left\{-\left[\left(\frac{(1+\frac{hw}{P_R})v_C}{c}\right)^k\right] - F_V(v_C)\right\} \quad (2.37)$$

Lastly, substituting Equation (2.37) into Equation (2.36) yields the combined equation in Equation (2.38).

$$Pr(P_w \leq p_w) = 1 - \exp\left\{-\left[\left(\frac{(1+\frac{hw}{P_R})v_C}{c}\right)^k\right] - F_V(v_F)\right\} \quad (2.38)$$

By taking the inverse of $F_V(v_F)$ result with the expression given in Equation (2.39). This equation denotes the CDF of the output energy random character P_w .

$$\begin{cases} 0 & P < 0 \\ 1 & P \geq P_R \\ 1 - \exp\left\{-\left[\left(1 + \frac{\left(1 + \frac{hw}{P_R}\right)v_C}{c}\right)^k\right] + \exp\left\{-\left[\frac{v_F}{c}\right]^k\right\}\right\}; & 0 \leq P < P_R \end{cases} \quad (2.39)$$

Since wind speed is a stochastic variable at any given time, the system operator may overestimate or underestimate the actual capacity of the wind-generating unit. Due to the nonlinearity of the wind-generating system, it is convenient to model for underestimation and overestimation in the cost curve. These important concepts are discussed separately in the following sections.

(vi) Overestimation

It occurs when the actual output wind power from the wind power system is less than the predicted output, so the system operator must purchase power from another power generation source. The overestimation of wind power can be represented mathematically and is given in Equation (2.40) (Hetzer et al., 2008)

$$C_{r,w,i}(P_{w_i} - P_{W_{i,av}}) = k_{r,i}(P_{w_i} - P_{W_{i,av}}) = k_{r,i} \int_0^{w_i} (P_{w_i} - P_W) f_{P_W}(w) dw \quad (2.40)$$

Where

$k_{r,i}$ Reserve cost coefficient for the i^{th} wind power generator.

P_{w_i} Predicted wind power

$P_{W_{i,av}}$ Available/Generated random wind power

$f_{P_W}(w)dw$ Probability distribution function for a Random variable P_W

Equation (2.40) is solved through the wind power probability Equations (2.28), (2.29), and (2.30). The analysis of the overestimation of wind power output is presented in the following way, and an analytical expression is given in Equation (2.41)(Liu & Xu, 2010a). For simplicity, the presentation is focused on a particular wind energy conversion system, and actual wind power is only denoted by P_W and leave subscript i, av . The predicted wind power output for the first turbine is denoted by P_{w_1} . The overestimated wind power output is $\phi_{OE} = P_{w_1} - P_W$ and the rated power represented as P_R . The average of the overestimated wind power output is given by $\phi_{OE} = s_1 + s_2$ (Liu & Xu, 2010a).

Where

$$\begin{aligned} s_1 &= w_1 P(W = 0) \\ &= w_1 \left\{ 1 - \exp \left[- \left(\frac{v_{in}}{c} \right)^k \right] + \exp \left[- \left(\frac{v_{out}}{c} \right)^k \right] \right\} \end{aligned} \quad (2.41)$$

$$\begin{aligned} s_2 &= \int_0^{w_r} \max(w_1 - w, 0) f_W(w) dw \\ &= \int_0^{w_1} (w_1 - w) f_W(w) dw \\ &= w_1 \int_0^{w_1} f_W(w) dw - \int_0^{w_1} w f_W(w) dw \\ &= w_1 [F_W(w_1) - F_W(0)] - H_{31} \end{aligned} \quad (2.42)$$

The solution of the first term can be easily found using Equation (2.16) and H_{31} is given in Equation (2.43).

$$\begin{aligned} H_{31} &= \int_0^{w_1} w f_W(w) dw \\ &= \frac{khv_C}{P_R c} \int_0^{w_1} w \left[\frac{\left(1 + \frac{hw}{P_R} \right) v_C}{c} \right]^{k-1} \exp \left\{ - \left[\frac{\left(1 + \frac{hw}{P_R} \right) v_C}{c} \right]^k \right\} dw \end{aligned} \quad (2.43)$$

Equation (2.43) is expressed in terms of integrals, which makes it very inconvenient to execute and analyse. The expression is broken down using Equation (2.16) and the substitution of variables such as $t = \left(1 + \frac{hw}{w_r} \right) v_{in}$. The equation is solved as follows.

Knowing that $t = (1 + hw/w_r)v_{in}$, the variable w can be easily found to be $w = (tw_r - v_{in}w_r)/hv_{in}$, $dw = w_r/hv_{in}dt$ and $y = (t/c)$. Substituting these variables to Equation (2.43), leads to the following expression as given in Equation (2.44).

$$\begin{aligned}
&= \frac{khv_{in}}{w_r c} \int_0^{w_1} \left(\frac{tw_r - v_{in}w_r}{hv_{in}} \right) \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] \frac{w_r}{hv_{in}} dt \right. \\
&= \frac{khv_{in}}{w_r c} \left(\frac{tw_r}{hv_{in}} \right) \left(\frac{w_r}{hv_{in}} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt \right. \\
&- \frac{khv_{in}}{w_r c} \left(\frac{v_{in}w_r}{hv_{in}} \right) \left(\frac{w_r}{hv_{in}} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt \right. \\
&= \frac{khv_{in}}{w_r c} \left(\frac{t(w_r)^2}{(hv_{in})^2} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt \right. \\
&- \frac{khv_{in}}{w_r c} \left(\frac{v_{in}(w_r)^2}{(hv_{in})^2} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt \right. \tag{2.44}
\end{aligned}$$

$$\begin{aligned}
&= \frac{k}{c} \left(\frac{tw_r}{hv_{in}} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt - \frac{kw_r}{hc} \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt \right. \\
&= \left(\frac{kw_r}{hv_{in}} \right) \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt - \frac{kw_r}{h} \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp \left\{ - \left[\left(\frac{t}{c} \right)^k \right] dt
\end{aligned}$$

Knowing that $y = \left(\frac{t}{c} \right)^k \therefore dy = \frac{kt^{k-1}}{c^k} dt$, $t = cy^{\frac{1}{k}}$ and $dt = \frac{c^{\frac{1}{k}}}{kt^{k-1}} dy \therefore$

$$\begin{aligned}
&= \left(\frac{kw_r}{hv_{in}} \right) \int_0^{w_1} cy^{\frac{1}{k}} \left[\frac{t}{c} \right]^{k-1} \exp(-y) \left(\frac{c^k}{kt^{k-1}} dy \right) - \frac{kw_r}{h} \int_0^{w_1} \left[\frac{t}{c} \right]^{k-1} \exp(-y) \left(\frac{c^k}{kt^{k-1}} dy \right) \\
&= \frac{w_r c}{hv_{in}} \int_{v_{in}}^{v_1} y^{\frac{1}{k}} \exp(-y) dy - \frac{w_r}{h} \int_{v_{in}}^{v_1} \exp(-y) dy, \text{ where } v_1 = \frac{v_{in} + (v_r - v_{in})w_1}{w_r}
\end{aligned}$$

According to Equations (2.16) and 2.21, Equation (2.44) can be fully solved and is given in Equation (2.45).

$$\begin{aligned}
&= \frac{w_r c}{hv_{in}} \Gamma \left[1 + \frac{1}{k}, \left(\frac{v_{in}}{c} \right)^k \right] - \frac{w_r c}{hv_{in}} \Gamma \left[1 + \frac{1}{k}, \left(\frac{v_1}{c} \right)^k \right] + \\
&\quad + \frac{w_r}{h} \left[\exp \left(- \frac{v_{in}}{c} \right)^k - \left[\exp \left(- \frac{v_1}{c} \right)^k \right] \right] \tag{2.45}
\end{aligned}$$

The combination of Equations (2.41), (2.42), and (2.45) represents the mathematical model of overestimation of wind power output and is given in Equation (2.46).

$$\begin{aligned}
E(Y_{oe,j,t}) = & w_{j,t} \left[1 - \exp\left(-\frac{v_{C,j,t}}{c_{j,t}}\right)^{k_{j,t}} + \exp\left(-\frac{v_{F,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
& + \left(\frac{P_{R,j,t} v_{C,j,t}}{v_{R,j,t} - v_{C,j,t}} + w_{j,t} \right) \left[\exp\left(-\frac{v_{C,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
& + \left(\frac{P_{R,j,t} c_{j,t}}{v_{R,j,t} - v_{C,j,t}} \right) \left[\Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) - \Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) \right]
\end{aligned} \tag{2.46}$$

(vii) Underestimation

The principle of underestimation is the opposite of overestimation; it occurs when the actual wind output power exceeds the forecast, so the excess is wasted, and the operator must reimburse the wind power output. It can be represented by the following mathematical expression and is given in Equation (2.47) (Hetzer et al., 2008)

$$C_{p,w,i}(P_{W_{i,av}} - P_{w_i}) = k_{p,i}(P_{W_{i,av}} - P_{w_i}) = k_{p,i} \int_0^{w_i} (P_W - P_{w_i}) f_{P_W}(w) dw \tag{2.47}$$

Where

$k_{p,i}$ Reserve cost coefficient for the i^{th} Wind power generator.

The analyses of underestimation are done the same way as those of the overestimation. The average of the underestimated wind power output is given by

$$\varphi_{UE} = s_1 + s_2$$

Where

$$\begin{aligned}
s_1 &= w_r P(W = w_r) \\
&= w_r \left\{ \exp\left[-\left(\frac{v_r}{c}\right)^k\right] - \exp\left[-\left(\frac{v_{out}}{c}\right)^k\right] \right\}
\end{aligned} \tag{2.48}$$

$$\begin{aligned}
s_2 &= \int_{v_r}^{v_{out}} \max(w - w_1) f_W(w) dw \\
&= \int_0^{w_1} (w - w_1) f_W(w) dw \\
&= \int_{v_r}^{v_{out}} w f_W(w) dw - w_1 \int_{v_r}^{v_{out}} f_W(w) dw \\
&= \int_{v_r}^{v_{out}} w f_W(w) dw - w_1 \left[\int_{v_r}^{v_{out}} f_W(w) dw + \int_{v_r}^{v_1} f_W(w) dw \right] \\
&= H_{32} - w_1 [F_W(v_{out}) - F_W(v_r)] + w_1 [F_W(v_1) - F_W(v_r)] \\
&= H_{32} - w_1 \left[\exp\left[-\left(\frac{v_r}{c}\right)^k\right] - \exp\left[-\left(\frac{v_{out}}{c}\right)^k\right] \right] + w_1 \left[\exp\left[-\left(\frac{v_r}{c}\right)^k\right] - \exp\left[-\left(\frac{v_1}{c}\right)^k\right] \right]
\end{aligned} \tag{2.49}$$

The derivation of H_{32} is exactly the same as H_{31} which is derived in Equation (2.44), but the difference is the limits of the definite integral. The integral for H_{32} is from $v_r \leq v \leq v_1$. The expression for H_{32} is given in Equation (2.50).

$$\begin{aligned}
&\frac{w_r c}{h v_{in}} \Gamma\left[1 + \frac{1}{k}, \left(\frac{v_1}{c}\right)^k\right] - \frac{w_r c}{h v_{in}} \Gamma\left[1 + \frac{1}{k}, \left(\frac{v_r}{c}\right)^k\right] + \\
&+ \frac{w_r}{h} \left[\exp\left(-\frac{v_r}{c}\right)^k - \exp\left(-\frac{v_1}{c}\right)^k \right]
\end{aligned} \tag{2.50}$$

Then, the combination of Equations (2.44), (2.48), (2.49), and (2.50) result in the following expression as presented in Equation (2.51).

$$\begin{aligned}
E(Y_{ue,j,t}) &= (P_{R,j,t} - w_{j,t}) \left[\exp\left(-\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{F,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
&+ \left(\frac{P_{R,j,t} v_{C,j,t}}{v_{R,j,t} - v_{C,j,t}} + w_{j,t} \right) \left[\exp\left(-\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
&+ \left(\frac{P_{R,j,t} c_{j,t}}{v_{R,j,t} - v_{C,j,t}} \right) \left[\Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) - \Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) \right]
\end{aligned} \tag{2.51}$$

2.2.1.2 Multi-criterion economic dispatch.

Atmospheric pollution has increased tremendously due to industrial advancement. When coal is used in the thermal plant utilities, harmful gaseous pollutants such as carbon oxides(CO_2), sulphur oxides(SO_2), and nitrogen oxides(NO_x). The Green Power committee suggests using low-emission sources to address the economic dispatch problem. Therefore, there is a need for improved control techniques that can achieve lower pollution levels at a realistic fuel cost. The emission gases, such as CO_2 , SO_2 and NO_x , and polluted by thermal generators, should be included in the optimisation objective function. Wind turbine generators are not subject to pollution, and the output power of a wind plant depends on wind speed, so the emission cost for the wind generator is zero. The overall emission of these pollutants is the sum of the quadratic cost function and the emission values, with the exponential function of the valve-point loading effect. This can be represented mathematically as (Abdelaziz et al., 2016)

$$E_T = \sum_{i=1}^{N_E} E_i(P_i) = \sum_{i=1}^{N_E} (\alpha_i + \beta_i P_i + \gamma_i P_i^2 + \lambda_i \times \exp(\varepsilon_i \times P_i)) \quad [\text{kg/h}] \quad (2.52)$$

Where

E_T Total emission [kg/h]

$\alpha_i, \beta_i, \gamma_i,$ Emission coefficients of the generating unit i in [kg/h], [kg/MWh], and [ton/MW²h]

ε_i, λ_i Valve point loading effect emission coefficients of the generating unit i

The pollutants CO_2 , SO_2 and NO_x The conventional generator can be formulated as given in Equations (2.53) to (2.55) respectively.

$$E_{CO_2i} = \sum_{i=1}^n (\alpha_{CO_2i} + \beta_{CO_2i} P_{gi} + \gamma_{CO_2i} P_{gi}^2 + \lambda_{CO_2i} \times \exp(\varepsilon_{CO_2i} \times P_{gi})) \quad [\text{kg/h}] \quad (2.53)$$

$$E_{SO_2i} = \sum_{i=1}^n \alpha_{SO_2i} + \beta_{SO_2i} P_{gi} + \gamma_{SO_2i} P_{gi}^2 + \lambda_{SO_2i} \times \exp(\varepsilon_{SO_2i} \times P_{gi}) \quad [\text{kg/h}] \quad (2.54)$$

$$E_{NO_xi} = \sum_{i=1}^n \alpha_{NO_xi} + \beta_{NO_xi} P_{gi} + \gamma_{NO_xi} P_{gi}^2 + \lambda_{NO_xi} \times \exp(\varepsilon_{NO_xi} \times P_{gi}) \quad [\text{kg/h}] \quad (2.55)$$

Where

$\alpha_{CO_2i}, \beta_{CO_2i}, \gamma_{CO_2i}, \lambda_{CO_2i}$ and ε_{CO_2i} CO_2 emission coefficients of i^{th} thermal generator in [kg/h], [kg/MWh], [kg/MW²h], [kg/h], and [kg/MWh]

$\alpha_{SO_2i}, \beta_{SO_2i}, \gamma_{SO_2i}, \lambda_{SO_2i}$ and ε_{SO_2i} SO_2 emission coefficients of i^{th} thermal generator in [kg/h], [kg/MWh], [kg/MW²h], [kg/h], and [kg/MWh]

$\alpha_{NO_xi}, \beta_{NO_xi}, \gamma_{NO_xi}, \lambda_{NO_xi}$ and ε_{NO_xi} NO_x emission coefficients of i^{th} thermal generator in [kg/h], [kg/MWh], [kg/MW²h], [kg/h], and [kg/MWh]

Therefore, the total emission is the sum of the three emissions and is given in Equation (2.56):

$$E_T = E_{CO_2i} + E_{SO_2i} + E_{NO_xi} \quad [\text{kg/h}] \quad (2.56)$$

The fuel cost function of the wind-thermal dispatch problem is given in Equation(2.2), and the emission functions of CO_2 , SO_2 and NO_x gases are given in Equations (2.53)-(2.55) individually. To formulate the multi-objective functions into a single objective function by using the price penalty factors given in Equations (2.57) to (2.59), respectively(Abdelaziz et al., 2016; Bhattacharya & Chattopadhyay, 2010; Jiang et al., 2015).

$$F_{CO_2} = \sum_{i=1}^{N_E} \left(a_i + b_i P_{gi} + c_i P_{gi}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi}))| + h_{CO_2i} \times (\alpha_{CO_2i} + \beta_{CO_2i} P_{gi} + \gamma_{CO_2i} P_{gi}^2 + \lambda_{CO_2i} \times \exp(\epsilon_{CO_2i} \times P_{gi})) \right) \quad [\$/\text{h}] \quad (2.57)$$

$$F_{SO_2} = \sum_{i=1}^{N_E} \left(a_i + b_i P_{gi} + c_i P_{gi}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi}))| + h_{SO_2i} \times (\alpha_{SO_2i} + \beta_{SO_2i} P_{gi} + \gamma_{SO_2i} P_{gi}^2 + \lambda_{SO_2i} \times \exp(\epsilon_{SO_2i} \times P_{gi})) \right) \quad [\$/\text{h}] \quad (2.58)$$

$$F_{NO_x} = \sum_{i=1}^{N_E} \left(a_i + b_i P_{gi} + c_i P_{gi}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi}))| + h_{NO_xi} \times (\alpha_{NO_xi} + \beta_{NO_xi} P_{gi} + \gamma_{NO_xi} P_{gi}^2 + \lambda_{NO_xi} \times \exp(\epsilon_{NO_xi} \times P_{gi})) \right) \quad [\$/\text{h}] \quad (2.59)$$

Where

F_{CO_2} CEED fuel cost of CO_2 emission

F_{SO_2} CEED fuel cost of SO_2 emission

F_{NO_x} CEED fuel cost of NO_x emission

The total fitness function is given in Equation (2.60) by considering CO_2 , SO_2 and NO_x emissions.

$$F_T = \sum_{i=1}^{N_E} \left(a_i + b_i P_{gi} + c_i P_{gi}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi}))| + h_{CO_2i} \times (\alpha_{CO_2i} + \beta_{CO_2i} P_{gi} + \gamma_{CO_2i} P_{gi}^2 + \lambda_{CO_2i} \times \exp(\epsilon_{CO_2i} \times P_{gi})) + h_{SO_2i} \times (\alpha_{SO_2i} + \beta_{SO_2i} P_{gi} + \gamma_{SO_2i} P_{gi}^2 + \lambda_{SO_2i} \times \exp(\epsilon_{SO_2i} \times P_{gi})) + h_{NO_xi} \times (\alpha_{NO_xi} + \beta_{NO_xi} P_{gi} + \gamma_{NO_xi} P_{gi}^2 + \lambda_{NO_xi} \times \exp(\epsilon_{NO_xi} \times P_{gi})) \right) \quad [\$/\text{h}] \quad (2.60)$$

The PPFs for CO_2, SO_2 and NO_x are calculated using a ratio of quadratic fuel cost to the emission and are given in Equations (2.61) to (2.63)

$$h_{CO_2i} = \frac{a_i + b_i P_{gi \max} + c_i P_{gi \max}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi \max}))|}{(\alpha_{CO_2i} + \beta_{CO_2i} P_{gi \max} + \gamma_{CO_2i} P_{gi \max}^2 + \lambda_{CO_2i} \times \exp(\epsilon_{CO_2i} \times P_{gi \max}))} \quad [\$/\text{kg}] \quad (2.61)$$

$$h_{SO_2i} = \frac{a_i + b_i P_{gi\max} + c_i P_{gi\max}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi\max}))|}{(\alpha_{SO_2i} + \beta_{SO_2i} P_{gi\max} + \gamma_{SO_2i} P_{gi\max}^2 + \lambda_{SO_2i} \times \exp(\varepsilon_{SO_2i} \times P_{gi\max}))} \quad [$/kg] \quad (2.62)$$

$$h_{NO_xi} = \frac{a_i + b_i P_{gi\max} + c_i P_{gi\max}^2 + |e_i \sin(f_i (P_{gi}^{\min} - P_{gi\max}))|}{(\alpha_{NO_xi} + \beta_{NO_xi} P_{gi\max} + \gamma_{NO_xi} P_{gi\max}^2 + \lambda_{NO_xi} \times \exp(\varepsilon_{NO_xi} \times P_{gi\max}))} \quad [$/kg] \quad (2.63)$$

Where

h_{CO_2i} Max-Max price penalty factor of CO_{2i} emission

h_{SO_2i} Max-Max price penalty factor of SO_{2i} emission

h_{NO_xi} Max-Max price penalty factor of NO_{xi} emission

2.2.2 Study of optimisation techniques employed in solving the single-area dynamic wind-thermal economic dispatch problem

2.2.2.1 Single criteria

This section investigates different optimisation methods for solving the wind-thermal economic dispatch problem to optimally control a single-area power system, accounting for the dynamic behaviour of renewable energy sources. Several optimisation methods have been used to solve a dynamic economic dispatch problem, including classical and heuristic methods (Zhu, 2015). The conventional classical methods include Unconstrained Optimisation Approach(UCA), Nonlinear Programming(NLP), Linear Programming(LP), Quadratic Programming (QP), Generalised Reduced Gradient Method(GRGM), Newton Method(NM), Network Flow Programming(NFP), Mixed-Integer Programming(MIP), and Interior Point methods(IP). The heuristic search methods, such as Artificial Neural Network(ANN), Evolutionary Algorithms(EAs), Tabu Search(TS), Particle Swarm Optimisation(PSO), and Non-quantitative approaches that address uncertainties in objectives and constraints, such as Probabilistic Methods(PM), Fuzzy logic(FL), and Analytic Hierarchical Process(AHP).

In a power system including wind generating units, it is necessary to consider spinning reserves such as Up Spinning Reserve (USR) and Down Spinning Reserve (DSR). The Up Spinning Reserve (USR) is the reserve capacity for an unexpected increase in load, a random drop in wind turbine generator power output, or the required outage of thermal generators. The Down Spinning Reserve (DSR) is the reserve capacity designed for rapid load decreases and erratic increases in wind turbine generator power output. (Chen et al., 2006), presented a Direct Search Method (DSM) to solve the economic dispatch problem with wind integration. The objective function considered in their work included both conventional operation cost and wind turbine generation

cost (WTGs) that are owned by the Independent Power Producer (IPP). Several optimisation constraints were considered, including minimum/maximum spinning reserves (up/down), power balance, and minimum/maximum capacity for both thermal and wind generators. The wind power is modelled using the Weibull Probability Density Function (WPDF). Also, Lee 2017 formulated the Optimal Spinning Reserve Wind-thermal (OSRWT) economic dispatch to determine the optimal spinning reserve (both USR and DSR) schedule for a wind-thermal power system that minimizes total social cost over a given period while satisfying system operating constraints. An efficient algorithm, Evolutionary Iteration Particle Swarm Optimization (EIPSO), is used to solve the OSRWT problem. This algorithm is a modification of PSO and Evolutionary Programming (EP). The Hybrid Optimization of Multiple Energy Resources (HOMER) software is used to simulate hourly wind speed data at a test site, and then generate the wind speed probability using the Weibull probability density function:-

The Authors (Hetzer et al., 2008) and (Meyyappan & Pandu, 2015), investigated the penalty cost for overestimation and underestimation of the available wind power output, which are included in their objective cost function for the optimum dispatch problem. The MATLAB optimisation toolbox is used to evaluate the optimal solution of the overall cost function, subject to linear/nonlinear optimisation constraints. In addition to that, the Authors (Meyyappan & Pandu, 2015) Provided a brief explanation of how the Wavelet Neural Network (WNN) can be used as an alternative to the Probabilistic Neural Network (PNN), Artificial Neural Network (ANN), and General Regressive Neural Networks (GRNNs) for extracting wind forecast data, as shown in Figure 2.8. The wind-thermal dispatch optimisation problem is first solved using the Primal-Dual-Interior-Point (PDIP) method, and later using Differential Evolution (DE) and Bacterial Foraging Technology (BFT). The solution is compared between the two heuristic methods.

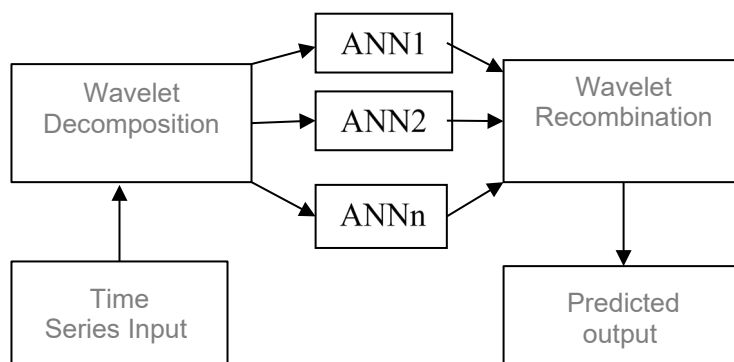


Figure 2.8: Predicted model for WNN (Meyyappan & Pandu, 2015)

The WNN (Wavelet Neural Network) forecast model in Figure 2.7 comprises three stages: pre-signal processing, signal forecasting, and post-signal processing. The time-

series input signal is decomposed using wavelets, with the signals treated with multiple wavelet factors. The neural networks' input is the result of the wavelet decomposer. The neural network's output is processed by wavelet recombination, which enhances all signals, and the resulting output is the forecast. The Weighted Probabilistic Neural Network (WPNN) (Krishnasamy & Nanjundappan, 2016) is a more generalized version of the predictive PNN applied by Meyyappan & Pandu (with respect to data extraction efficiency). The cost function for fuel application considers multiple fuel-producing units with valve-point loading, subject to various power system limitations, and BBO + SQP is applied to obtain a better solution.

A new optimal method, the Genetic-Teaching Learning-Based Optimisation (G-TLBO), was introduced by Güçyetmez & Çam (2016) for global optimisation of the wind-thermal dispatch problem. The wind-thermal dispatch problem is defined as an optimal power flow problem applied to the cost function relative to system constraints, with wind-speed generation over- and under-estimations.

In the article by Lu et al. (2008), the valve-point loading quadratic cost function was researched. An Independent Power Producer (IPP) owns a wind farm with a great dispersion of wind turbines. The economic use of the IPP will significantly reduce generation costs, as the utility will purchase the required wind power. Wind power generation depends on wind speed, as shown in the wind power curve. The authors solve the economic dispatch problem using the Direct Search Method (DSM) and the Evolutionary Simulated Annealing (ESA) algorithms, where ESA is employed to find the global optimal solution, and DSM is used to improve the solution and reduce computing time. Authors (Boqiang & Chuanwen, 2009) assess an instantaneous economic dispatch model with wind power and a temporary economic dispatch model with wind power, where wind power is certain, for the economic emission generation system problem, using an optimization algorithm and the power city risk dispatch framework. According to Morales et al. (2009), their work created a dispatch problem that quantifies the reserves produced in a market-clearing scenario that accounts for wind uncertainty and represents the best spinning/non-spinning reserves of a robust system with substantial wind penetration. The limits are provided by the market for energy selling and first-stage variables (variables that are not impacted by scenario realization at each time step at each scenario, i.e. the start-up and shut-down scheduling for each generation unit), reality system operation, and second-stage variables (these variables, which are dependent on the specific scenarios and are connected to actual operation of the system i.e. wind power spilling). Constraints on market versus real system operation and on first-stage versus second-stage variables are taken into account. In Xian Liu & Xu's work, wind economic dispatch is understood.

Therefore, in this research, the optimal solution to thermal dispatch problems uses probabilistic infeasibility prevention and the Lagrangian method to obtain optimal results. In Jiang et al. (2011), a quadratic cost function with valve-point loading effects was studied as a dynamic economic dispatch problem. Transmission losses and real power requirements are treated as equality constraints; however, bulk constraints for thermal and wind generating units, as well as up/down spinning reserves, are treated as inequality constraints in this study. This study requires 24-hour-ahead wind energy predictions. The dispatch problem is solved by the Improved Particle Swarm Optimization (IPSO) technique (X. Liu, 2010), which utilizes the Beta distribution to operate generation units forecasted at the time of the studied sharewind generation output. The issue is optimized for wind-thermal dispatch using a chance-constrained nonlinear programming (CCNP).

The authors (Li & Jiang, 2011) measured an economic dispatch for 24 hours with a combined Risk administration, which involves in estimating the risk assessment, and this would benefit the system operator (SO) to vary a decent adjustment between revenues and risks, depending on system equality and inequality limitations. The particle swarm optimisation (PSO) heuristic is used to optimise the power system problem. Wind power output is viewed as a stochastic (random) variable by the authors (Zhou et al., 2011) and the reserve cost is accounted for in the total objective function. The dynamic economic dispatch problem is solved via a nonlinear Primal-Dual Interior-Point (PDIP) method. Constraints, such as risk-based spinning reserves, minimum and maximum wind power outputs, absolute power limits of the thermal plant, and ramp speed limits of conventional units, are considered. The authors (Reddy et al., 2013), formulated the economic dispatch fuel cost function with valve-point loading effect. The spinning reserve supplied by the thermal units is included in the cost function, along with the underestimation and overestimation of wind power and the direct cost of wind power. Covariance Matrix Adaptation with Evolution Strategy (CMA-ES) and Mean Learning Technique (MLT) are used to find solutions to the economic dispatch problem, which considers both. Inequality and equality constraints. The authors (Liang et al., 2015) formulated the economic dispatch problem, which includes both active and reactive power. The Firefly algorithm is used as a heuristic optimization approach. The authors (Li et al., 2013) presented a Lagrangian approach to solve a dynamic economic dispatch problem. The quasi-Newton method (QNM) is used to optimise the economic dispatch problem, subject to equality and inequality constraints. The review summary of the wind-thermal economic emission dispatch problem is given in Table 2.3.

2.2.2.2 Multi-criteria

In recent years, research on multi-criteria optimisation methods has increased. Decisions with multiple criteria are predominant in government, military, industry, and other organisations (Kothari & Dhillon, 2012). Research from a wide range of fields, such as mathematics, management, science, economics, engineering, and others, has contributed to solution methods for multi-criteria optimisation problems. The multi-criteria optimisation problem is also called multi-performance, multi-objective, or vector optimisation. The engineer's goal is to maximize or minimize not a single objective function but numerous objective functions simultaneously. The purpose of multi-performance problems in the mathematical programming framework is to optimize multiple objective functions, subject to a set of system constraints.

(Kuo, 2010) and (Qu et al., 2016) Formulated the Economic Emission Dispatch (EED) problems with a stochastic wind power model. The dispatch problem is solved by using a Summation-based Multi-Objective Differential Evolution Algorithm (SMODE). The wind power output is modelled as a system constraint by using stochastic variables and applying probability theory. Ramp rate limits, prohibited zones, and transmission losses are treated as nonlinear constraints, while power balance is treated as a linear constraint. PSO and GA optimisation methods are used by (Kuo, 2010). The Summation-based Multi-Objective Differential Evolution (SMODE) and NSGAI are used as heuristic optimisation methods in (Qu et al., 2016). The authors (Xian Liu & Xu, 2010), solved the economic emission dispatch problem, including overestimation and underestimation constraints in the cost function. The impact of wind power is presented using the Weibull Distribution function. The authors (Bhattacharya & Chattopadhyay, 2010) presented a biogeographical optimization method to solve the Economic Emission Dispatch (EED) problem. The EED problem is formulated to minimize total emissions from conventional power-generating units.

The authors (Azizipanah-Abarghooee et al., 2015; Dubey et al., 2015; A. Ghasemi et al., 2016; Jadhav & Roy, 2013a; Mondal et al., 2013a; Peng et al., 2012a) examined the formulation of the economic dispatch problem, taking into account a quadratic cost function with valve-point loading effects. The Weibull probability distribution function (PDF) is used to model wind power. Depending on who owns the wind farm, the cost function also includes the reserve cost resulting from the unavailability of wind power (overestimation) and the penalty for underutilising available wind (underestimation).

Equation 2.27 provides a representation of the emission cost function in terms of the quadratic cost and an exponential function. Several optimisation techniques, such as the Modified Teaching-Learning Algorithm (MLTA) (Azizipanah-Abarghooee et al., 2012), Bi-Population Chaotic Differential Evolution (BPCDE) (Peng et al., 2012b), Gbest

Guided Artificial Bee Colony(GABC) algorithm (Jadhav & Roy, 2013b), and Gravitational Search Algorithm(GSA)(Mondal et al., 2013b), the combination of Hybrid Flower Pollination(HFPA-TVFSM) Algorithm and Time Varying Fuzzy Selection Mechanism(Dubey et al., 2015), Gravitational Acceleration Enhanced Particle Swarm Optimization(GAEPSSO) algorithm(Jiang et al., 2015) and Online Learning Honey Bee Mating Optimization(OLHBMO) (Ghasemi et al., 2016) are used to solve the wind-thermal economic dispatch problem subject to system linear and nonlinear constraints.

The authors(Chaudhary et al., 2020; Pandit, Chaudhary, et al., 2015a; Zhu et al., 2014) used a quadratic fuel cost to solve the Combined Emission Economic Dispatch (CEED) problem, omitting the cost function for overestimation and underestimation. The optimisation problem is resolved using a decomposition-based Multi-Objective Evolutionary Algorithm (MOEA/D). (SPSO-DE) Series Particle Swarm Optimization-Differential Evolution(Chaudhary et al., 2020; Pandit, Chaudhary, et al., 2015a; Zhu et al., 2014). The problem is broken down into several smaller problems. Subject to system restrictions on both wind and thermal generating units. The Weibull Probability Distribution Function (WPDF) is used as a modelling tool for wind generator output. To reduce the multi-objective optimisation to a single objective function, (Niu & Wei, 2013) developed an economic dispatch problem utilising the Karush-Kuhn-Tucker conditions. The constraint optimisation problem is solved by combining the multiplier approach with the particle swarm algorithm.

The authors (Alham et al., 2016) considered flexible distributed energy resources, such as an energy storage system (ESS) and Demand Site Management(DSM), in the objective function. Different ESS are explained in(Patel, 1999). The ESS, DSM, and minimum and maximum power output for both wind and thermal generating units are included in the nonlinear constraints. The GAMS software is utilised to solve this Dynamic Economic Emission Dispatch (DEED) problem.

(Chen et al., 2017)The multi-objective optimisation problem is formulated with wind, thermal, and short-term hydro power plants. The power balance is represented by equality constraints without losses, and the inequality constraints are represented by minimum and maximum power limits for wind, thermal, and hydro energy. The cost function compensates for both wind overestimation and underestimation. A Modified Gravitational Search Algorithm based on the Non-dominated Sorting Genetic Algorithm-III (MGSA-NSGA-III) is used to find the optimal solution. It is associated with other methods described in the reported survey. The process is validated with four cascaded hydropower plants, three conventional units, and two wind power plants.

In (Elattar, 2018), the bio-objective optimisation problem is formulated with wind, thermal, and solar power plants. The power balance is represented by equality

constraints without losses, and the inequality constraints are minimum and maximum power limits for wind, thermal, and solar energy. A Modified Harmony Search (MHS) algorithm is used to find the minimum cost for fuel and emissions for the optimization problem. Three thermal generators and a wind-and-solar unit are used to validate the process efficiency. Two of the conventional generators are synchronous generators, while the third one is a combined heat and power generator.

In (Hu et al., 2019) The economic dispatch problem is considered a dynamic optimization problem in which the conventional ramp rate is included in the power balance constraints. Wind power is modelled using a PDF, with wind represented by a direct cost function, an overestimation cost function, and an underestimation cost function. The problem is solved using a hybrid optimization method that combines GA (Genetic Algorithm) with Sequential Quadratic Programming (SQP) to form GA-SQP. Also, (Zhang et al., 2019), presented a multi-optimisation method that minimises both fuel and emission cost, using a quadratic cost function with valve-point loading effects and equality and inequality constraints in the objective function. Wind power is modelled using a PDF, including direct, overestimation, and underestimation terms in the cost function. The Gravitational Particle Swarm Optimization Algorithm (GPSOA) is used as a hybrid optimization algorithm to solve the WTEED problem.

In (Behera et al., 2021) The multi-objective optimisation problem is formulated with wind, thermal, and solar power. The power balance is represented by equality constraints without losses, and the inequality constraints are represented by minimum and maximum power limits for wind, thermal, and solar energy. The overestimation and underestimation of wind and solar are included in the cost function. A Constriction Factor-Based Particle Swarm Optimization (CFBPSO) algorithm is used to find the optimal solution and is compared with other algorithms reported in the literature. The algorithm is validated across six bus systems: three conventional units with valve-point loading, two wind, and two solar power plants.

The economic emission dispatch problem is solved using a decision-making technique, the Technique for Order Preference by Similarity to an Ideal Solution (TOPSIS) (Jin et al., 2021). Transmission losses are incorporated into the optimisation bi-function; balance restrictions are expressed as equalities and inequalities; and the concern is represented by a quadratic cost function and valve-point loading.

A non-convex optimization problem is presented in (Salkuti, 2021), where transmission losses are included in the equality constraints and ramp rate and forbidden zones are treated as inequality constraints. Wind energy modeling is presented as a stochastic function using a PDF.

In (Yan et al., 2022) The economic dispatch problem is formulated with valve-point loading effects in the quadratic function, and power balance constraints are included as equality constraints. Electric vehicles are used as energy storage systems to smooth the intermittency of wind power. This is done by developing the interactive model between wind power and Electric vehicles. Wind power is modelled using a two-parameter PDF. A self-adaptive multiple-learning multi-objective harmony-search(SAMLHS) algorithm is proposed for solving this complex optimization problem.

(Nagarajan et al., 2022), presented a paper on the economic dispatch problem that includes wind, thermal, and solar units. The economic dispatch is solved using the Improved Mayfly (IM) Optimization Algorithm. Different scenarios were considered: conventional units with solar, thermal units with wind, thermal-only units, and all combinations to validate the algorithm's effectiveness.

A non-convex optimization problem is formulated with wind and solar power (Azeem et al., 2023). The bio-objective function is transformed to a single one with PPF. A heuristic algorithm, the Salp Swarm Algorithm, is used to solve the optimization problem. This nonlinear optimization problem involves ramp rates of thermal units in inequality constraints and a loss term in equality constraints. Thereafter, the algorithm is tested against the latest survey. A combined heat and power(CHP) system is simulated with solar generation and wind generation with the global nondominated sorting genetic algorithm II (GNSGA-II(Zou et al., 2023). The following constraints, including power generation limits, heat generation limits, CHP unit capacity limits, power balances, heat balances, ramp rate limits, and spinning reserve, are considered in the optimization concern. Different scenarios are presented to illustrate the algorithm's effectiveness.

In the work of (Lalhmachhuana et al., 2024) Optimisation is performed with and without wind power integration; the power balance is treated as an equality, whereas the maximum and minimum powers of wind and thermal sources are treated as inequality constraints. Multi-Objective Particle Swarm optimisation (MOPSO) and Multi-Objective Ant-Lion optimisation (MOALO) are used, and the results for fuel and emissions are later compared.

In the work of (Secui et al., 2024b), Modified Social Group Optimization (MSGO) is used to verify the effectiveness of the optimization algorithm. The algorithm is further tested on an IEEE30 bus system that consists of 10-unit and 40-unit systems: two systems, each with 550MW, supply wind power injection. The equality and inequality constraints are incorporated into the objective function as power balance constraints and minimum and maximum limits for the wind and thermal generating units. Overestimation and underestimation of wind power are treated as penalty coefficients.

(Qiao et al., 2025) formulated the DEED problem with wind power, and an Electric Vehicle is used as a storage system to compensate for wind uncertainties. The intermittence between wind power and Electric vehicles is modelled using the conditional value-at-risk (CVaR) of IWEv. Constraints such as the power balance, the residual power of the EVs, travel constraints for EV owners, charging and discharging power, and climbing rate are included in DEEDR-IWEv. A self-adaptive multi-mode teaching-learning-based optimization (SaMmTLBO) algorithm is used to solve the DEED problem. The algorithm's feasibility is tested on a 10-unit system across different scenarios.

(Xiong et al., 2025) presented an EED problem that includes wind, solar, and small hydro runoff. The problem is solved using a Multi-Objective Artificial Gorilla Troops(MOAGT) optimizer. The algorithm is validated using the IEEE 30- and IEEE 18-bus systems. The bus allocation for RES differs across test systems. Recently, in (Meng et al., 2025), studied a day-ahead economic dispatch framework for microgrids with wind integration, combining battery storage and hybrid demand response (DR). The system is benchmarked across the following cases: conventional, wind-only, wind+storage, wind+DR, and fully integrated. The algorithm demonstrated that a fully integrated method can reduce cost, renewable utilization, and grid stability.

In the study of (Li et al., 2024), an economic scheduling prototype for combined energy units with stochastic wind and PV uncertainty. This paper efficiently utilizes electrolyzer thermal energy, incorporates carbon trading, and demand response. Information Gap Decision Theory (IGDT)-based methods manage risk while reducing operating cost and emissions.

(Mao et al., 2026)presented an integrated energy system scheduling framework that considers dynamic carbon trading and efficiency improvements. Optimizes multi-energy resources with carbon pricing to reduce operational cost and emissions. The problem is solved using Distributed Robust Optimization (DRO)-Model Predictive Control (MPC).

The review summary of the problem for wind-thermal economic dispatch is given in Table 2.1. Figure 2.9 illustrates the graphical representation of Table 2.1. This figure shows the number of publications per year. The review summary of single-area, single- and multi-criteria wind-thermal economic dispatch is presented in Table 2.3.

Table 2.1: Quantity of papers for wind-thermal economic dispatch on a yearly basis

Quantity of papers year-wise		
Reference	Year of publication	Number of publications
(George.,1945)	1945	1

(Kron.,1951)	1951	1
(Gernald & Aaron.,1958)	1958	1
(Schlueter et al, 1983)	1983	1
(Schlueter et al, 1985)	1985	1
(Masters., 2004)	2004	1
(Miranda,and Pun Sio Hang, 2005)	2005	1
(Chen et al 2006), (Denny, and O'malley, 2006), (Patel., 2006)	2006	3
(Lee,. 2007), (Ummels et al 2007), (Ruey-Hsun Liang, & Jian-Hao Liao, 2007),(Methaprayoon, et al, 2007), (Balamurugan & Subramanian ., 2007)	2007	5
(Hetzer et al 2008), (Lu et al., 2008), (Garcia., 2008)	2008	3
(Boqiang, and, Chuanwen, 2009), (Pappala et al, 2009), (Morales, et al 2009)	2009	3
(Kuo, 2010), (Yongpinget al, 2010), (Liu. 2010), (Liu, and Xu. 2010), Liu and Xu 2010), (Da silva, 2010), (Kothari & Dhillon.,2010),)Bhattacharya & Chattopadhyay.,2010), Zhou et al.,2010)	2010	10
(Zhou, et al 2011), (Liu, 2011), (Jiang et al, 2011), (Makarov et al, 2011), (Constantinescu et al, (2011), (Meibom, et al 2011), (Li,& Jiang. 2011), (Hafiz, et al 2011),	2011	8
(Azizipannah-Abarghooee, et al 2012), (Peng, et al 2012 (Liang, et al 2012), (Ciornei, & Kyriakides,. 2012), (LIU,et al. 2012), (Altunkaynak et al., 2012)	2012	6
(Adhav, and Roy .,2013), (Reddy et al., 2013), (Zhao, et al., 2013), (Mondal, et al., 2013), (Wang, et al., 2013), (Hafiz, et al., 2013), (Zhou et al.,2013), (Niu & Wei., 2013), (Krishnamurthy., 2013), (Abul'Wafa, 2013)	2013	10
(Zhu, et al .,2014), (Moeini-Aghtaie, et al., 2014), (Cheng & Zhang.,2014)	2014	3
(Geetha, et al., 2015), (Dubey, et al 2015), (Han, et al., 2015), (Osório, et al., 2015), (Pandit, et al 2015), (Liang, et al., 2015), (Jiang, et al., 2015), (Hedayati-Mehdiabadi, et al., 2015),(Meyyappan and Pandu, 2015), (Güçyetmez, & Çam, 2016),	2015	10
(Ghasemi, et al., 2016), (Krishnasamy, & Nanjundappan, 2016), (Lujano-Rojas, et al 2016), (Fu, et al., 2016), (Li, et al., 2016), (Zhou, et al., 2016), (Alham et al, 2016), (Qu et al, 2016), (Abdelaziz et al., 2016), (Patel., 2016), (Velamuri et al.,2016)	2016	10
(Chen et al.,2017)	2017	1
(Elatter 2018)	2018	1
(Hu et al., 2019), (Jiang et al., 2019)	2019	2
(Behera et al., 2020)	2020	1
(Jin et al., 2021), (Salkuti., 2021)	2021	2
(Yan et al., 2022), (Nagarajan et al.,2022)	2022	2
(Azeem et al.,2023), (Zou et al., 2023).	2023	2
(Lalmachhuana et al.,2024), (Secui et al. 2024)	2024	2
(Qiao et al., 2025), (Xiong et al.,2025), (Meng et al., 2025)	2025	3

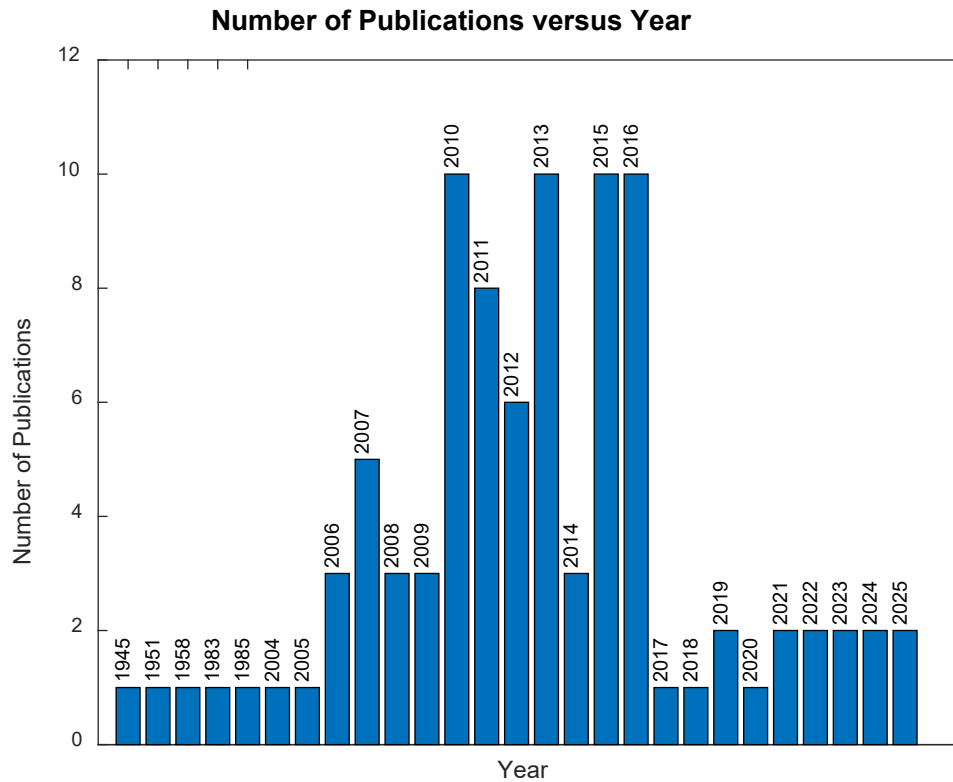


Figure 2.9: Quantity of papers for wind-thermal economic dispatch on yearly basis

Table 2.2: Techniques and algorithms applied to solve the single-area wind-thermal economic dispatch problem

Most used methods and algorithms		Reference paper	No. of publications
Algorithm	Abbreviation		
Artificial Neural Networks	ANN	(Methaprayoon, et al, 2007)	1
Biogeography-Based Optimization.	BBO	Bhattacharya & Chattopadhyay.,2010)	1
Bi-Population Chaotic Differential Evolution algorithm	BPCDE	(Peng, et al 2012)	1
Covariant Matrix Adaptation with Evolution Strategy with Mean Learning Technique	CMA-ES/MLT	(Reddy et al., 2013)	1
Diffusion Particle Optimization	DPO	(Han, et al., 2015	1
Direct Search Method	DSM	(Chen et al 2006), Alham et al, 2016)	2
Energy Storage System	ESS	(Alham et al, 2016)	1
Evolutionary Iteration Particle Swarm Optimisation	EIPSO	(Lee,., 2007),	1
Evolutionary Simulated Annealing	ESA	(Lu et al., 2008)	1

Feasible Operation Region	FOR	(Hafiz, et al 2011), (Hafiz, et al 2013)	2
FireFly Algorithm	FFA	Liang, et al., 2015	1
Flower Pollination Algorithm	FPA	(Velamuri et al,2016), (Abdelaziz et al., 2016)	2
Flying-Blick Method	FBM	(Makarov et al, 2011)	1
Forecasted Approach	FA	(Denny, and O'malley, 2006), (Constantinescu et al, (2011)	2
Fuzzy Logic	FL	(Miranda,& Pun Sio Hang, 2005), (Liang et al., 2015) (Jian-Hao Liao, 2007), (Geetha, et al., 2015)	4
Gbest guided Artificial Bee Colony algorithm	GABC	(Adhav, and Roy .,2013)	1
Genetic Algorithm –Ant Colony Approach	GA-API	(Ciornei, & Kyriakides, . 2012)	1
Genetic Teaching Learning-Based Optimization	(G-TLBO)	(Güçyetmez, & Çam, 2015)	1
Gravitational Acceleration Enhanced Particle Swarm Optimization algorithm	GAEPSO	Jiang, et al., 2015	1
Gravitational Search Algorithm (GSA)	GSA	(Mondal, et al., 2013),	1
Group Search Optimizer with Multiple Producers	GSOMP	(Li, et al., 2016),	1
Hybrid Flower Pollination Algorithm (HFPA)- Time Varying Fuzzy Selection Mechanism (TVFSM)	HFPA-TVFSM	(Dubey, et al 2015	1
Hybrid Particle Swarm Optimization	HPSO	(Niu & Wei, 2013)	1
Interior Point Method	IPM	(Zhou, et al 2011), (Fu, et al., 2016)	2
Lagrangian Relaxation	LR	(Li, 2013),(Niu, & Wei, 2013)	2
Markov chain forecast model	MCFM	(Hedayati-Mehdiabadi, et al., 2015),	1
Mixed Interger	MI	(Meibom, et al 2011)	1
Modified Teaching-Learning Algorithm(MTLA)	MTLA	(Azizipanah-Abarghoee, et al 2012)	1
Multi-Objective Evolutionary Algorithm based on Decomposition	MOEA/D,	Zhu, et al .,2014	1
Multi-Agent Genetic Algorithm	MAGA	(Moeini-Aghtaie, et al., 2014)	1
Non-dominated Sorting Genetic Algorithms	NSGA	(Abul'Wafa, 2013)	1
Online-Learning Honey Bee Mating Optimization	OLHBMO	(Ghasemi, et al., 2016),	1

Optimality Decomposition Coordination	ODC	(Zhou, et al., 2016)	1
Particle Swarm Optimisation	PSO	(Pappala et al, 2009), (Kuo, 2010), (Jiang et al, 2011), (Li, & Jiang. 2011), (Wang et al., 2013), (Salkuti., 2021)	6
Probabilistic Approach	PA	(Osório, et al., 2015), (Lujano-Rojas, et al 2016), (Da Silva., 2010), (Liu, 2011)	4
Probabilistic Kernel Density Forecasting	PKDF	Zhou et al., 2013	1
Series Particle Swarm Optimization-Differential Evolution	(SPSO-DE)	Pandit, et al 2015	1
Singular Weighted Method	SWM	(Yongping et al., 2010)	1
Stochastic Programming	SP	(Morales, et al 2009)	1
Summation based Multi-Objective Differential Evolution algorithm	SMODE	(Qu et al, 2016)	1
Weighted Probabilistic Neural Network	WPNN	(Krishnasamy, & Nanjundappan, 2016),	1
Weibull Probability Density Function	WPDF	(Hetzer et al 2008), (Liu, & Xu. 2010), (, Xu & Liu. 2010), (Liu. 2010),	4
Modified Gravitational Search Algorithm based on the Non-dominated Sorting Genetic Algorithm-III (MGSA-NSGA-III)	MGSA-NSGA-III	(Chen et al. 2017)	1
Modified Harmony Search (MHS)	MHS	(Elatter., 2018)	1
Genetic-Sequential Quadratic Programming	GA-SQP	(Hu et al., 2019)	1
Gravitational Particle Swarm Optimization Algorithm (GPSOA)	GPSOA	(Jiang et al., 2019)	1
Constriction Factor-Based Particle Swarm Optimization (CFBPSO)	CFBPSO	Behera et al., (2020)	1
Technique for Order Preference by Similarity to an Ideal Solution (TOPSIS)	TOPSIS	(Jin et al., 2021)	1
Self-Adaptive Multi-Learning Harmony-Search Algorithm (SAMLHS)	SAMLHS	(Yan et al., 2022)	1
Improved Mayfly (IM) Algorithm	IM	(Nagarajan et al., 2022)	1
Chaotic Salp Swarm Algorithm (CISSA)	CISSA	(Azeem et al., 2023)	1
Global Nondominated Sorting Genetic Algorithm II (GNSGA-II)	GNSGA-II	(Zou et al., 2023)	1
Multi-Objective Particle Swarm optimisation (MOPSO) and Multi-Objective Ant-Lion optimisation (MOALO)	MOPSO and MOALO	(Lalhmachhuana et al., 2024)	1
Modified Social Group Optimization (MSGO)	MSGO	(Secui et al., 2024)	1
Self-adaptive Multi-mode Teaching-Learning-Based	SaMmTLBO	(Qiao et al., 2025)	1

Optimization (SaMmTLBO) algorithm			
Multi-Objective Artificial Gorilla Troops(MOAGT) optimizer	MOAGT	(Xiong et al.,2025)	1
Combining battery storage and hybrid demand response (DR)	DR	(Meng et al.,2025)	1
Information Gap Decision Theory(IGDT)	IGDT	(Li et al., 2024)	1
Distributed Robust optimization (DRO)-Model Predictive Control (MPC).	(DRO)-(MPC)	(Mao et al., 2026)	1

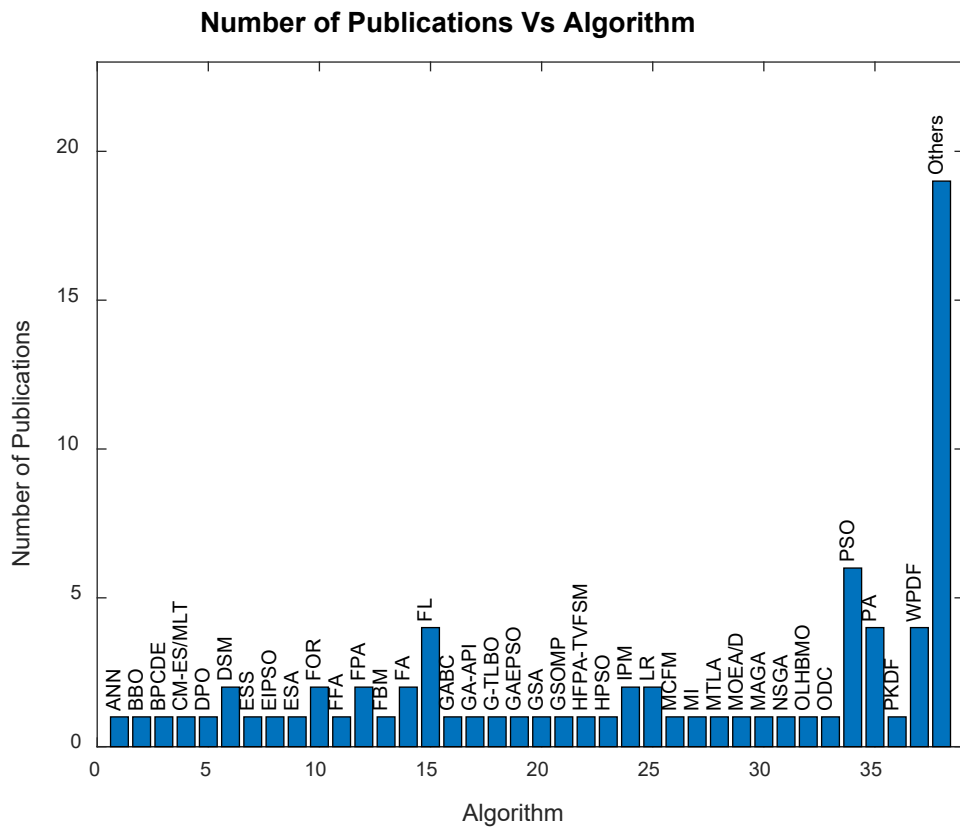


Figure 2.10: Quantity of papers vs algorithm of wind-thermal economic dispatch

Table 2.3: Study of the literature on wind-thermal economic emission dispatch problem with single and multi-criteria

Reference Paper	System Components			Objective Function		Constraints		Algorithm	Software	Power System Considered	Real life implementation
	Wind	Storage	Coal, Diesel & Other	Single Objective	Multi Objective	Equality Constraints	Inequality Constraints				
(Miranda, and Pun Sio Hang, 2005)	Yes	Nil	yes	Minimize fuel cost	Nil	Real power balance constraints	Minimum and maximum thermal technical limits for generators. Minimum wind power and maximum available wind power(predicted wind power)	Fuzzy logic	Not Specified	Not Specified	No
(Chen et al., 2006)	Yes	Nil	yes	Minimize fuel cost	Nil	Real power balance constraints. Generators' maximum up/ down spinning reserves. Thermal plant up/down spinning reserve contribution constraints.	Unit capacity constraints. Wind power curve constraints. System maximum ramping capability constraint	Direct search Method	FORTRAN	The Taiwan power system has 52 generating units.	No
(Denny, and O'malley, 2006)	Yes	Pumped storage	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Wind power forecast errors and load forecast errors constraints. system reliability criteria, and forced outage probabilities constraints	Forecast Approach	Not mentioned	Not specified	No
(Methaprayoonet al, 2007)	Yes	Nil	Nil	Fuel cost reduction	Nil	Nil	Nil	Artificial Neural Network	MATLAB	Wind farm in Lawton City that consists of 45 wind turbines, each rated at 1.65 MW	No
(Tsung-Ying Lee. 2007)	Yes	Nil	Yes	Operation and outage cost	Nil	Real power balance constraints.	Generator limits constraints. Min and Max wind turbine output power.	Evolutionary Iteration Particle Swarm	HOMER	Two practical power systems are used as numerical examples	No

							Min and Max ramping speed of a thermal generator. Minimum up time and down time of generation units. Up/down spinning reserve.	Optimization (EIPSO)		to test the new algorithm.	
(Hetzer et al 2008),	Yes	Nil	Yes	Fuel cost minimisation	Nil	Real power balance constraints.	Thermal generator limits. Wind turbine limits.	Not Specified	MATLAB	Two thermal and Wind turbine generators	No
(Lu et al., 2008)	Yes	Nil	Yes	Fuel cost with valve point effect	Nil	Real power balance constraints. Conventional Unit's maximum up/down reserve contribution constraints. Thermal Unit's up/down spinning reserve contribution constraints.	System up/down spinning reserves. System Min/max power output constraints. Thermal plant capacity constraints. Conventional plant ramp-rate limits constraints. Wind power curve constraints. Total actual wind generation limit. Wind power penetration limit. Wind generation fluctuation constraints	Evolutionary Simulated Annealing (ESA) algorithm combined with the Direct Search Method (DSM)	FORTRAN	Not Mentioned	No
(Morales, et al 2009)	Yes	Nil	Nil	Minimize fuel cost	Nil	Real power balance constraints.	Constraints Pertaining to the Electricity Market and Involving First-Stage Variables. Constraints pertaining to the actual system operation and involving second-stage variables. Constraints linking the market and the actual system operation, involving first and second-stage variables.	Stochastic Programming(SP)	Not Mentioned	Not Mentioned	No

(Kuo, 2010)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission loss constraints.	Ramp rate limits. Prohibited operating zone and generation limits.	Strength Pareto Evolutionary Algorithm (SPEA)	MATLAB	TAI-POWER and IEEE 30-bus systems	No
(Liu and Xu 2010a)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Total actual wind generation limit. Thermal plant capacity constraints.	Incomplete gamma(Probability Approach)	MATLAB	Standard IEEE 30-bus test system. Case studies included six thermal generators and two wind turbines.	No
(Liu and Xu 2010b)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Total actual wind generation limit. Thermal plant capacity constraints.	Incomplete gamma(Probability Approach) and Lagrangian Approach	MATLAB	Case studies included six thermal generators and one wind turbine unit.	No
(Liu., 2010)	Yes	Nil	Yes	Minimize fuel cost	Nil	Real power balance constraints.	Total actual wind generation limit. Thermal plant capacity constraints.	Incomplete gamma(Probability Approach) Lagrangian Method	MATLAB	A case study considered has six thermal generators and one wind turbine.	No
(Yongping et al., 2010)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Balance supply and demand constraints.	The upper and lower limits of the generating units.	Singular Weighted Method (SWM)	MATLAB	Power system with five power-generating units.	No
(Jiang et al, 2011)	Yes	Nil	Yes	Fuel cost with valve point loading effect	Nil	Real power balance constraints. Transmission loss constraints	Real power operating limits of the generation unit. Spinning reserve constraint(USR and DSR) Generating unit ramp rate limits.	PSO	Not Specified	6-unit system and the 15-unit system.	No
(Liu, 2011)	Yes	Nil	Yes	Minimize fuel cost	Nil	Real power balance constraints.	Real power operating limits of generation units.	Beta distribution of the PDF(Probabili	MATLAB	Not Mentioned	No

								stic Approach)			
(Li & Jiang. 2011)	Yes	Nil	Yes	Minimize fuel cost	Nil	Real power balance constraints. Transmission constraints:	Generator limits constraints. Ramping rate constraints. Minimum up/down-time:	PSO	Not Mentioned	IEEE 30-bus power system. The Shanghai network which consists of a wind turbine and five thermal generating units	Yes
(Alhasawi, & Milanovic, 2012)	Yes	Nil	Yes	Minimize fuel cost	Nil	Power balance constraints.	Minimum and Maximum active and reactive power limits. Min and Max voltage magnitude.	Genetic Algorithm and Lagrangian Method.	MATLAB	Not Specified	No.
(Azizipanah-Abarghoee, et al 2012)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve loading effect and emission function	Power balance constraints. Transmission loss constraints	Real power operating limits of generation units. Prohibited operating zone.	Modified Teaching-Learning algorithm(MT LA)	Not Specified	(i.) The first system consists of 6 units, neglecting power losses. (ii.) The second system includes 14 units and the power losses are considered. (iii.) The third system comprises 40 units, of which 5 out of 40 exhibit prohibited zones, and the effect of power losses is neglected.	No
(Peng, et al 2012)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve effect and emission	Power balance and transmission loss constraints.	Prohibiting zones. Minimum and maximum operating limits of both wind and thermal generators. Ramp rate constraints. Minimum on/off time constraints. Ramping up/down rate constraints.	Bi-population Chaotic Differential Evolution (BPCDE)	Not specified	Power system with 5 thermal power units integrated with large-scale wind farms, which consist of 160 wind turbines.	No

(Hafiz et al.,2012)	Yes	Nil	Yes	Minimize fuel cost	Nil	Power balance constraints.	Capacity constraints Ramp rate constraints	Feasible Operation Region (FOR)	Not mentioned	Not specified	No
(Jadhav & Roy., 2013)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve point loading effect and emission function	Power balance and transmission loss constraints	Min/Max generators operating limits. Prohibited operating zone of thermal generators. Ramp rate limits of thermal generators	Gbest Guided Artificial Bee Colony algorithm (GABC)	MATLAB	IEEE 30 bus system.	No
(Mondal, et al., 2013)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve effect and emission	Power balance constraints	Max/Min operating limits of both wind and thermal generators.	Gravitational Search Algorithm (GSA)	MATLAB	IEEE 30-bus test system.	
(Reddy et al., 2013),	Yes	Nil	Yes	Minimize fuel cost with valve-point loading.	Nil	Power balance and transmission loss constraints	Total spinning reserve requirement constraints. Max/Min operating limits of both wind and thermal generators. Generator spinning reserve constraints.	Mean Learning Technique (MLT)	MATLAB	The algorithm is implemented on 6 units and 40-unit test systems.	No
(Zhao, et al 2013)	Yes	Hydropower (pumped storage)	Yes	Nil	Minimize fuel cost and emissions	Power balance constraints.	Generator spinning reserve. Max/Min operating limits of wind and thermal generators. Ramping rate constraints. Minimum up/down time constraints.	General Algebraic Modelling System Branch-And-Reduce Optimization Navigator (GAMS BARON) solver Algorithm	General Algebraic Modelling System (GAMS) Software	Not Mentioned	No
(Li et al., 2013)	Yes	Nil	Yes	Minimize fuel cost	Nil	Power balance constraints.	Ramping rate constraint. Generation output limit of thermal units. The generation output limit of wind power generators. Positive spinning reserve constraint.	Lagrangian Approach	VC++ 9,0	Not Mentioned	No

							Up/Down spinning reserve constraints.				
(Niu and Wei, 2013)	Yes	Nil	Yes	Nil	Minimize fuel cost and emission	Power balance constraints. Transmission losses	Power operating limits. Spinning reserves.	Karush-Kuhn-Tucker(KKT) and Hybrid Particle Swarm Optimization(HPSO)	Not specified	Not specified	No
(Zhu, et al .,2014)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Power balance constraints.	Reserve capacity constraint. Units output constraint for both thermal and wind generators	Multi-Objective Evolutionary Algorithm based on Decomposition (MOEA/D)	MATLAB	6-generator system and a 40-generator system with wind farms.	No
(Dubey, et al 2015)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve point loading effect and emission function	Power balance constraints. Transmission losses	Ramping rate constraint. Generation output limit of thermal units and wind turbines.	Flower Pollination Hybrid Algorithm (HFPA)-TVFSM(Time Varying Fuzzy Selection Mechanism)	Not specified	Tested on two wind-thermal power systems	No
(Han, et al., 2015)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve point loading effect and emission function	Power balance constraints.	Lower and upper generating capacities for thermal and Wind generator. Ramp rate limits of thermal generators.	Diffusion Particle Optimization (DPO)	MATLAB	(i). Thirteen thermal generating system without considering emissions and wind power. (ii)Test system with a modified IEEE 30-bus/6-generators test system. (iii) The test system consists of an economic dispatch problem considering emissions.	No

(Jiang, et al., 2015)	Yes	Nil	Yes	Nil	Minimize fuel cost with valve point loading effect and emission function	Power balance constraints. Transmission losses	Lower and upper generating capacities of the thermal and wind generator system. Ramp rate limits of thermal generators. Prohibited operating zone of thermal generators.	Gravitational Acceleration Enhanced Particle Swarm Optimization algorithm (GAEPSO).	MATLAB	40 thermal generators and 2 wind turbines test system.	No
(Liang, et al., 2015)	Yes	Nil	Yes	Minimize fuel cost.	Nil	Power balance constraints. Transmission losses	Minimum/Maximum thermal generator reactive and active power output. Min/Max wind turbine output. Min/max voltage magnitude output. Min/max voltage phase angle. Minimum/Maximum load tap changer position of the power transformer. Minimum/Maximum reactive power injection using capacitor banks. The maximum line flow of the transmission line.	Firefly Algorithm (FA)	MATLAB	The IEEE 30-bus system.	No
(Meyyappan and Pandu, 2015)	Yes	Nil	Yes.	Minimize operational cost.	Nil	Power balance constraints.	Lower and upper generating capacities for thermal and Wind generator system.	Primal Dual Interior Point(PDIP), Differential Evolution(DE), and Bacterial Foraging Technology (BFT). Using ANN and wavelet transform to predict the wind forecast(WNN	MATLAB	Three, 13, and 40 thermal units systems, along with three wind generators of the same rating.	No

								(Wavelet neural network)			
(Pandit, et al 2015)	Yes	Nil	Yes	Nil	Minimize operating cost with valve point loading effect and emission function	Power balance constraints. Transmission losses.	Lower and upper generating capacities for the thermal and wind generator system. Ramp rate limits of thermal generators. Prohibited operating zone of thermal generators	PSO-DE	MATLAB	30 bus system with six conventional thermal generating units and one wind farm which consists of 20 similar wind turbines	No
(Geetha, et al., 2015)	Yes	Nil	Yes	Minimize operating cost.	Nil	Power balance constraints.	Lower and upper generating capacities for thermal and Wind generator systems. Ramp rate limits of thermal generators. Minimum on/off time constraints.	Genetic Algorithm.	MATLAB Fuzzy logic model.	Genco system comprises ten thermal units and two wind farms.	No
(Güçyetmez & Çam, 2016)	Yes	Nil	Yes	Minimize operating cost.	Nil	Power balance constraints. Transmission losses	Minimum/Maximum thermal generator reactive and active power outputs. Min/Max wind turbine output. Min/max voltage magnitude. Min/max voltage phase angle.	Hybrid Genetic-Teaching Learning-Based Optimization (G-TLBO) algorithm	MATLAB/SIMULINK	Thermal-wind-powered Turkish energy generation system of 19 buses	No
(Alham et al, 2016)	Yes	Yes	Yes	Nil	Minimize operating cost and	Power balance constraints. Transmission losses.	Lower and upper generating capacities for thermal and Wind generator.	Genetic Algorithm (GA)	The GAMS software/ MATLAB	Standard IEEE 30-bus system.	No

					emissions . Several cases as the fuel cost minimization, Emission minimization, and emission and cost minimization simultaneously	Load demand without /with using DSM.	Ramp rate limits of thermal generators. Constraints of energy storage. Upward demand variation and downward demand variation at each hour of DSM(Demand Site Management)				
(Ghasemi, et al., 2016)	Yes	Nil	Yes	Nil	Minimise Fuel and emission cost	Real power balance constraints. Transmission losses.	Minimum/Maximum thermal generator reactive and active output. Min/Max wind turbine output. Min/max voltage magnitude output. Prohibited operating zone of thermal generators Transmission line security constraints.	Online Honey Bee Matting optimisation (HBMO) (OLHBMO)	MATLAB	IEEE 30-bus 6-unit, the IEEE 118-bus 14-unit, and the 40-unit with valve point loading effect test systems	No
(Krishnasamy & Nanjundappan, 2016)	Yes	Nil	Yes	Minimize fuel cost with valve-point loading. Multiple fuel option is considered	Nil	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator system.	Weighted Probabilistic Neural Network (WPNN) - Biogeography -Based Optimization (BBO) algorithm	MATLAB	Not Mentioned	Yes
(Qu et al, 2016)	Yes	Nil	Yes	Minimize fuel cost with	Nil	Real power balance constraints	Lower and upper generating	Summation-based Multi-Objective Differential	MATLAB	(i) IEEE 30-bus 6-generator system.	No

							capacities of thermal and wind generator systems.	Evolution (SMODE) algorithm		(ii) IEEE 30-bus 6-generator system including the transmission losses. (iii) 40-thermal-generator lossless system.	
(Velamuri et al, 2016)	Yes	Nil	Yes	Minimize fuel cost.	Nil	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems.	Flower Pollination Algorithm (FPA)	MATLAB	IEEE 30 bus system.	No
(Chen et al.,2017)	Yes	Nil	Yes	Nil	Minimise Fuel and emission cost	Real power balance	Lower and upper generating capacities of thermal wind, and hydro generating systems	Modified Gravitational Search Algorithm based on the Non-dominated Sorting Genetic Algorithm-III (MGSA-NSGA-III)	MATLAB	Four cascaded hydropower plants, three thermal plants, and two wind power plants.	No
(Hu et al.,2019)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints	Lower and upper generating capacities of thermal and wind generator systems. Ramp rate limits of thermal generators.	Genetic-Sequential Quadratic Programming Algorithm(GA-SQP)	MATLAB	IEEE 30 bus test system with six thermal generators and large scale wind-farm	No.
(Jiang et al., 2019)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems.	Gravitational-Particle Swarm Optimisation Algorithm (GPSOA)	MATLAB	IEEE 30 bus test system with six thermal generators and two wind turbines	No
(Behera et al.,2020)	Yes	Nil	Diesel and Solar	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Lower and upper generating	Constriction Factor-Based Particle Swarm	MATLAB	Six bus systems with three TGs, two	No

							capacities of thermal, Solar, and wind generating systems	Optimization (CFBPSO)		WPGs, and two SPGs	
(Jin et al., 2021)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems.	Technique for Order Preference by Similarity to an Ideal Solution(TOPSIS)	MATLAB	Six classical generating units and one wind system are used.	No
(Salkuti., 2021)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems. Ramp rate limits of prohibited zones for thermal generators.	Particle Swarm Optimisation(PSO)	MATLAB	Six thermal generating units, but later generator one is replaced by a wind power system	No
(Yan et al., 2022)	Yes	Yes Electrical Vehicle (EV)	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems. Ramp rate limit, spinning reserves for thermal generators. Travel constraints of EV owners, EVs' remaining power constraints, and charging and discharging EVs.	Self-Adaptive Multi-Learning Harmony-Search Algorithm (SAMLHS)	MATLAB	Ten thermal units were used, and a Toyota RAV4 served as the EV. Different EV-to-Wind scenarios are used.	No
(Nagarajan et al.,2022)	Yes	Nil	Diesel and Solar	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Lower and upper generating capacities of thermal, Solar, and wind generating systems	Improved Mayfly (IM) Algorithm	MATLAB	Three conventional generators, solar, and wind units	No
(Azeem et al.,2023)	Yes	Nil	Diesel and Solar	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Lower and upper generating capacities of thermal, Solar, and wind generating systems	Chaotic Salp Swarm Algorithm (CISSA)	MATLAB	Different test cases, scenarios, and combinations of thermal, solar, and wind units.	No

Zou et al., 2023).	Yes	Nil	Diesel and Solar	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Lower and upper generating capacities of thermal, Solar, and wind generating systems. Ramp rate limit, spinning reserves for thermal generators. Heat-generating limits, capacity limits of the CHP units	Global Nondominated Sorting Genetic Algorithm II (GNSGA-II)	MATLAB	Four CHPDEED cases with or without renewable energies are considered.	No
(Lalmachhuana et al.,2024)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints	Lower and upper generating capacities of thermal and wind-generating systems. Security constraints, minimum and maximum reactive power	Multi-Objective Particle Swarm optimisation(MOPSO) and Multi-Objective Ant-Lion optimisation(MOALO)	MATLAB	IEEE-30 bus system, Ten 3.2MW wind power system	No
(Secui et al., 2024)	Yes	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind-generating systems.	Modified Social Group Optimization (MSGO)	MATLAB	IEEE30 bus system with 10 and 40 units. The wind power consists of two wind systems, each having 550MW	No
(Qiao et al., 2025)	Yes	Yes	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints. Transmission losses.	Lower and upper generating capacities of thermal and wind generator systems. Ramp rate limit, spinning reserves for thermal generators. Travel constraints of EV owners, EVs' remaining power constraints, and charging and discharging EVs.	Self-adaptive Multi-mode Teaching-Learning-Based Optimization (SaMmTLBO) algorithm	MATLAB	Ten thermal units were used, and a Toyota RAV4 served as the EV. Different EV-to-Wind scenarios are used.	No
(Xiong et al.,2025)	Yes	Nil	Diesel ,	Nil	Minimize fuel cost	Real power balance constraints.	Lower and upper generating	Multi-Objective	MATLAB	Modified IEEE 30-bus system with two thermal	No

			Solar, and hydro power		and emissions	Transmission losses.	capacities of thermal wind, hydro, and solar generating systems, constraints, and minimum and maximum reactive power constraints.	Artificial Gorilla Troops (MOAGT) optimizer		units. One wind and SRH power plants The combined wind and SRH power plant and the Modified IEEE 118-bus system have 54 thermal units, three wind plants, and two solar plants. Combination of PV and SRH, and of Wind and SRH.	
(Meng et al., 2025)	Yes	Yes	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints.	Lower and upper fan power, SOC, wind, Photovoltaic, and transfer load.	Demand Response(DR)	Not mentioned	conventional, wind-only, wind+storage, wind+DR, and fully integrated.	No
(Li et al., 2024)	Yes	Yes	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints, which include: Electric Power Balance Constraints, Thermal Power Balance, and Gas Power Balance Constraints	Lower and upper, Photovoltaic, wind, Energy Storage Unit Operational Constraints, Purchased Energy Power Constraints, Hydrogen Equilibrium Constraints	Information Gap Decision Theory(IGDT)	Not mentioned	Six different scenarios are used to validate the effectiveness of the algorithm	No
(Mao et al., 2026)	Yes	Yes	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints, which include:	Lower and upper, Photovoltaic, wind, Energy Storage Unit Operational Constraints, Purchased Energy Power Constraints	Distributed Robust Optimization (DRO)-Model Predictive Control (MPC).	MATLAB	Uncertainty scenarios are consist of the PV, WT and fluctuations of diverse form of energy demands.	Real-time formula presented

2.3 Hybrid Renewable Energy Systems (HRES) economic dispatch

The ever-rising oil prices, declining fuel resources, insatiable demand for electrical energy, and the worldwide concern for atmospheric pollution and environmental protection have caught the attention of many researchers. The use of Distributed Energy Resources (DERs) has caught the attention of many researchers. These resources are considered environmentally friendly and have lower operational cost. Power generation from such resources is consistent and could reduce the overall cost of a power system if they are operated and scheduled wisely. However, integrating these resources into the current thermal generation may disrupt some security constraints of the Economic Dispatch (ED) model of the existing system, due to the erratic and random nature of these DERs. Therefore, a correctly modelled system and more secure constraints need to be added to the thermal ED formulation to avoid casualties during power system operation.

A hybrid system's main goal is to provide users with dependable AC/DC power at a reasonable price. It can be set up as a grid-connected system or as an off-grid, standalone, or island HRES. Figure 2.11 displays many classes. According to (Theo et al., 2017) HRES is composed of various power-generating technologies, including solar PV, wind turbines, fuel cells, traditional diesel generators, biogas generation, biomass generation, and CHP.

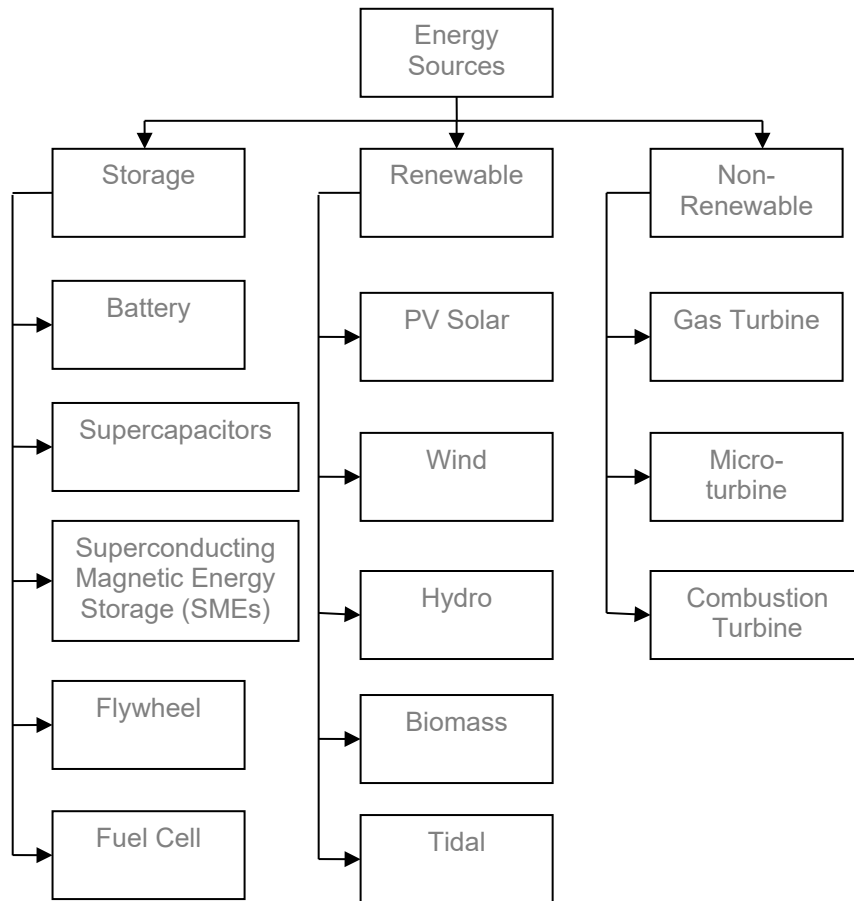


Figure 2.11: Power sources and storage for a mixed renewable energy system
(Ogunjuyigbe et al., 2016)

A storage battery system is what makes an HRES better than a non-HRES. According to various authors, for example, Kaldellis (2010) states that the storage battery can be a capacitor, flywheel system, pumped hydro, or compressed air.

2.3.1 Study of techniques applied in solving the single-area economic dispatch problem for Hybrid Renewable Energy Systems (HRES)

2.3.1.1 Single-criteria

The economic dispatch dependability of hybrid power systems has been examined using a variety of mathematical models and techniques with several goals, including cost minimization, pollution reduction, and dynamic load control. (Diaf et al., 2008), studied the optimum formation of a stand-alone hybrid photovoltaic-wind system that ensures the energy autonomy of a typical remote consumer with the lowest levelized cost of energy. The techno-economic optimization method is used to investigate different combinations. (Kashefi Kaviani et al., 2009), used a PSO to improve a hybrid wind-photovoltaic-fuel cell generation system to minimise the yearly cost of the hybrid system, subject to a reliable supply to meet the demand. (Giannakoudis et al., 2010) used an optimisation method based on heuristic algorithms called Simulated

Annealing(SA) for the design and operation of a hybrid power generation system that consists of wind generators, a diesel generator, PV panels, accumulators, an electrolysis apparatus, hydrogen storage tanks, a compressor, and a fuel cell.

(Kaabeche et al., 2011), suggested an optimisation model based on an iterative technique to optimise the size of a hybrid wind/photovoltaic system combined with a battery bank, to reduce power supply insufficiency and the levelized unit electricity cost, subject to system equality and inequality constraints. A two-stage adaptive robust optimization model for the Security Constrained Generation Scheduling (SCGS) problem, where the first-stage unit commitment decision and the second-stage ED decision are solved (EIDesouky, 2014).

An adaptive hybrid technique involving an Artificial Neural Network (ANN) and a Genetic Algorithm (GA) is used. The authors (Arabali et al., 2014) Used a stochastic optimization method to optimally size the hybrid system components while satisfying the system reliability requirements. A sequential Monte Carlo simulation (SMCS) method is used to create data in a time sequence and then analyse reliability indices from the simulated results. The SMCS method examines the system's sequential performance by generating consecutive samples of system states over multiple time intervals. This offers a better illustration of the hybrid system's behaviour for reliability analysis. The Direct Search (DS) method, Pattern Search (PS), is used to solve the non-smooth optimal sizing problem for the hybrid power system.

The authors (Som & Chakraborty, 2014) Presented a power system that consists of fuel cells, solar modules, and biomass gasifier units as DERs. A facility for buying electricity in a contract with a utility is also considered in both types of power-delivery systems. The mathematical investigations are performed using a Real-Valued Cultural Algorithm (RVCA). The authors (Arriagada et al., 2015) Presented a probabilistic economic dispatch model considering thermal units (fuel generators), photovoltaic arrays, and wind energy conversion systems. The thermal generator is modelled with a quadratic cost function. The Weibull distribution is used to represent the wind power output. Lastly, the PV plant is modelled with a Beta distribution.

In this study, the authors (Azizpanah-Abarghoee et al., 2015), a CCP (chance constrained programming) based on the (Jointly Distributed Random Variables Method (JDRVM) is considered to solve the problem of stochastic Multi-Objective Combined Heat and Power Economic Dispatch (SMCHPED), including random behaviours of wind energy conversion system and photovoltaic output power, as well as electrical and thermal load demand. The uncertainty of each random variable is modelled by a PDF (Probability Density Function). The output power risk of WPGs and PVUs can be covered by other thermal units and Combined Heat and Power (CHP) devices.

The authors (Plathottam & Salehfar, 2015) Formulated an economic dispatch problem for a power system control area with more diffusion of renewable production and power storage. The PV/wind/storage system considered has 20% wind generation and 10% distributed PV compared to the overall generation capacity. The cost functions and constraints related to each component are considered. Simulated Annealing(SA) and PSO are used to solve the optimization problem.

The authors (Malheiro et al., 2015), Formulated economic dispatch(ED) to minimise the operation cost of the power system subject to inequality and quality constraints, using the Mixed-Integer Linear Programming technique. A battery bank, wind, PV solar, and a backup diesel generator make up the HRES.

In the study of (Maleki & Askarzadeh, 2014)The discrete harmony search approach was used to solve the ED problem with the wind/PV solar/diesel/battery system. The simulation results were compared using the Discrete Simulated Annealing (DSA) methodology. (Belmili et al., 2014), examined sizing techniques for independent photovoltaic-wind hybrid systems. The first section of the article presents various software for addressing the HRES issue (HYBRID2, HYBRIDS, HOMER (Hybrid Optimisation Model for Electric Renewable), HOGA (Hybrid Optimisation by Genetic Algorithms). It provides modeling of various HRES components and solutions in the context of power supply balance constraints, including inequality and equality constraints. To approximate all aspects of electricity consumption, the TRNSYS software is used to simulate the dynamic thermal behaviour of residential buildings and forecast the electrical energy required to meet the thermal load, which partly contributes to the non-controllable load of the residential area.

(Atia & Yamada, 2016). The probability distributions of electric load and renewable energy resources are described by Probability Distribution Functions (PDFs) and introduced into the optimization using scenario generation techniques. The optimisation method uses a mixed-integer linear programming (MILP) approach. The authors (Cao et al., 2016)presented a weather-dependent optimal power flow algorithm with wind farm integration that considers temperature-related resistance and Dynamic Line Rating (DLR) of overhead lines.

The authors (Guo et al., 2014) studied a stand-alone microgrid with a seawater desalination system. An EMS for a stand-alone micro-grid consisting of a WT generator, a diesel generator, an ESS, and a seawater desalination system. The energy management system (EMS) can control supply-demand balance and maximize the environmental or economic benefits. The stand-alone wind-diesel micro-grid uses an EMS strategy that optimizes the charging/discharging cycles of the storage system and the system's operational cost based on predictions of wind turbine output and load

demand. Neural Network-based wind forecasting is used to forecast real-time wind data, and the Genetic Algorithm is used as an optimization method.

(Theo et al., 2017) and (Kusakana, 2019), provides a thorough analysis of various hybrid system configurations, examining modelling, reliability, optimisation techniques, and optimal operation control.

2.3.1.2 Multi-criteria

(B. Lu & Shahidehpour, 2005), created a short-term grid-connected PV/battery system using the Lagrangian method through a security-constrained unit commitment algorithm. The terminal current-voltage (I-V) characteristics of solar cells are established through a two-diode model and equality/inequality constraints. In (Liang & Liao, 2007) The optimal control problem is defined with respect to PV solar, wind, conventional, and hydropower, with environmental pollutants such as and . Power balance is taken into account as inequality constraints. The problem is solved using a fuzzy-logic optimization approach.

The authors (Dufo-López & Bernal-Agustín, 2008; Shayeghi et al., 2015) also present papers based on a multi-objective optimization problem, including cost minimization and carbon dioxide emissions, and the various mathematical models used are derived from previous research.

(Dufo-López et al., 2007; Dufo-López & Bernal-Agustín, 2005, 2008) present the HRES problem as a synthesis of a PV-Wind-Diesel-Hydrogen-Battery system, where a Multi-Objective Evolutionary Algorithm (MOEA) and a Genetic Algorithm (GA) are used to find the optimal solution for hybrid system synthesis and control.

The authors (Shayeghi et al., 2015) Used the Artificial Bee Colony(ABC) method. In (Ogunjuyigbe et al., 2016) The objective is to minimise life-cycle cost, energy losses, and carbon dioxide emissions, with the GA used to find solutions subject to component constraints. The total power generation from PV, wind, Diesel, and stored energy must always be greater than the load demand. A three-split diesel generator model is used to replace standard single diesel units, enabling multiple generators to meet the user's demands at specified times while minimising use at low load factors.

(Kamjoo et al., 2016), solved the stand-alone HRES optimisation problem, which synthesises solar, wind, and battery bank using Non-dominated Sorting Genetic Algorithm (NSGA-II) in combination with Chance Constrained Programming (CCP). The nonlinear constraints require that the summed output powers from both PV and wind must provide the overall load balance, or otherwise, the stored power in the battery must. The nonlinear constraints depend solely on the battery bank's state of charge and the physical constraints of the other two components of the HRES.

According to the authors' research (Abul'Wafa, 2013), the dispatch problem includes wind/ PV solar/ thermal units, as well as emissions. The wind and solar output power are presented using the Weibull distribution. The underestimation and overestimation of PV and wind are included in the objective cost function. The conventional generators and emissions are represented by a quadratic cost function with valve-point loading and by a quadratic function with an exponential term, subject to equality and inequality constraints.

(Bilil et al., 2014), proposed the probabilistic economic dispatch (EED) problem for a power system integrating RESs. The main objective is to minimize the cost of power generation and the greenhouse gas emissions of the system, subject to the operation limits of RESs. The multi-objective optimisation problem is investigated using CE-NSGA-II. The review summary of the HRES economic dispatch is given in Table 2.4. Figure 2.12 illustrates the graphical representation of Table 2.4. This figure shows the number of publications per year.

Table 2.4: Quantity of paper for HRES economic dispatch on a yearly basis

Quantity of papers year-wise		
Reference	Year of publication	Number of publications
(Lu & Shahidehpour,2005), (Dufo-López, & Bernal-Agustín, 2005)	2005	2
(Dufo-López, & Bernal-Agustín, 2006)	2006	1
(Liang, and Liao., 2007), (Dufo-López et al., 2007)	2007	2
(Diaf et al., 2008), (Dufo-Lopez, & Bernal-Agustin.,2008)	2008	2
(Kashefi Kaviani et al., 2009)	2009	1
(Giannakoudis et al., 2010), (Kaldellis.,2010)	2010	2
(Kaabeche et al., 2011)	2011	1
(Shengwei Mei et al., 2012)	2012	1
(Abul'Wafa, 2013)	2013	1
(Som & Chakraborty., 2014), Trifkovic., et 2014), (Bilil et al, 2014) (EIDesouky, 2014), Arabali et al., 2014), Belmili et al., 2014), (Maleki & Askarzadeh., 2014)	2014	7
(Arriagada et al., 2015), (Plathottam, & Salehfar., 2015) (Azizipanah-Abarghooee et al., 2015), (Arriagada et al., 2015), (Malheiro et al.,2015)	2015	5
((Kamjoo et al., 2016), (Guo et al., 2016), (Cao et al., 2016), (Atia & Yamada.,2016), (Ogunjuyigbe et al.,2016), (Kusakana., 2016)	2016	6

(Theo., 2017)	2017	1
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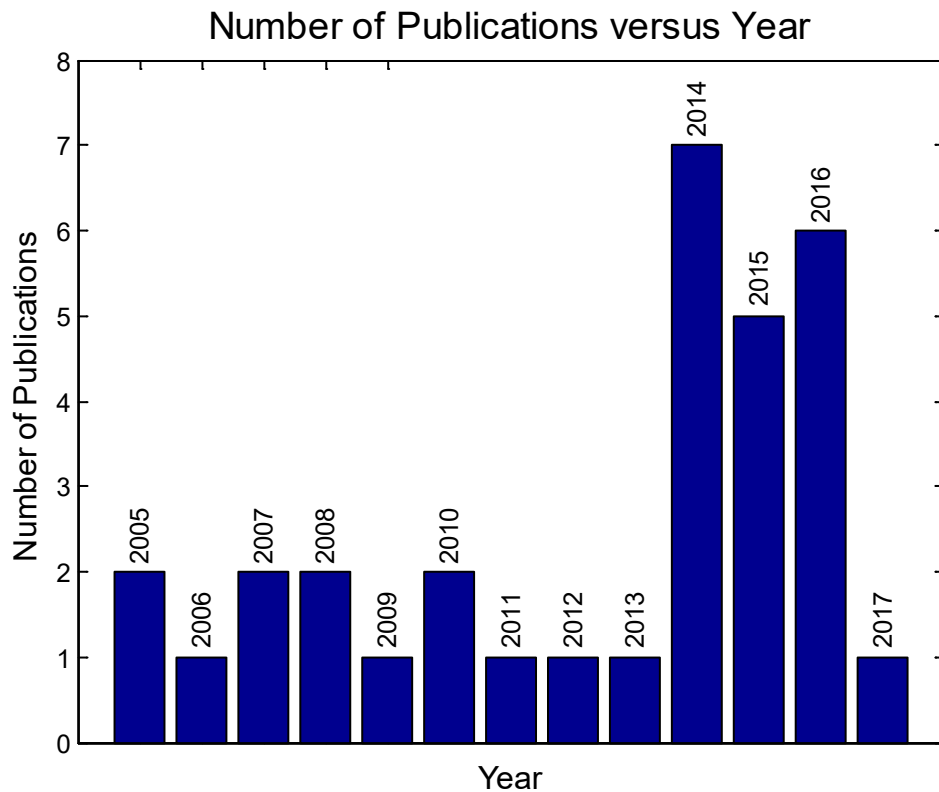


Figure 2.12: Number of publications of HRES economic dispatch on a yearly basis

Table 2.5: Techniques and algorithms applied to the HRES single-area economic dispatch problem.

Most used methods and algorithms		Reference paper	No. of publications
Algorithm	Abbreviation		
Artificial Neural Network	ANN	(EIDesouky, 2014), (Guo et al., 2016)	2
Controlled Elitist – Non-Dominated Sorting Geneti Algorithm-II	CE-NSGA-II	(Abul'Wafa, 2013), (Bilil et al, 2014), (Kamjoo et al., 2016)	3
Differential Evolution	DE	(Basu et al., 2012)	1
Fuzzy optimization method	FL	(Liang, and Liao., 2007)	1
Game theory	GT	(Mei,et al., 2012)	1
Genetic algorithm	GA	(EIDesouky, 2014), (Guo et al., 2016), (Ogunjuyigbe et al.,2016), (Dufo-Lopez, & Bernal-Agustin.,2008)	4
Harmony Search	HS	(Maleki & Askarzadeh., 2014)	1
Hybrid Modified Cuckoo Search Algorithm And Differential Evolution	H-MCSA-DE	(Azizipanah-Abarghooee et al., 2015)	1
Iterative Optimisation	IO	(Kaabeche et al., 2011)	1
Iterative Optimization Technique	IOT	(Kaabeche et al., 2011)	1

Lagrangian Method	LR	(Lu & Shahidehpour,2005)	1
Mix Integer Linear Programming	MILP	(Malheiro et al.,2015)	1
Mixed Integer linear Programming	MIP	(Atia & Yamada.,2016)	1
Multi Objective Evolutionary Algorithm	MOEA	(Dufo-Lopez, & Bernal-Agustin.,2008)	1
Particle swarm optimisation	PSO	(Kaviani et al., 2009), (Plathottam, & Salehfar., 2015)	2
Pattern Search-based optimization method	PS	Arabali et al., 2014)	1
Probalistic Method	PM	(Arriagada et al., 2015)	1
Real Valued Cultural Algorithm	RVCA	(Som & Chakraborty., 2014)	1
Sequential Monte Carlo simulation	SMCS	Arabali et al., 2014)	1
Simulate Annealing	SA	(Giannakoudis et al., 2010), (Plathottam, & Salehfar., 2015), (Maleki & Askarzadeh., 2014)	3
Techno-Economical optimisation	TE	(Diaf et al., 2008), (Belmili et al., 2014)	2
Weather-Based Optimal Power Flow algorithm	WB-OPF	(Cao et al., 2016)	1

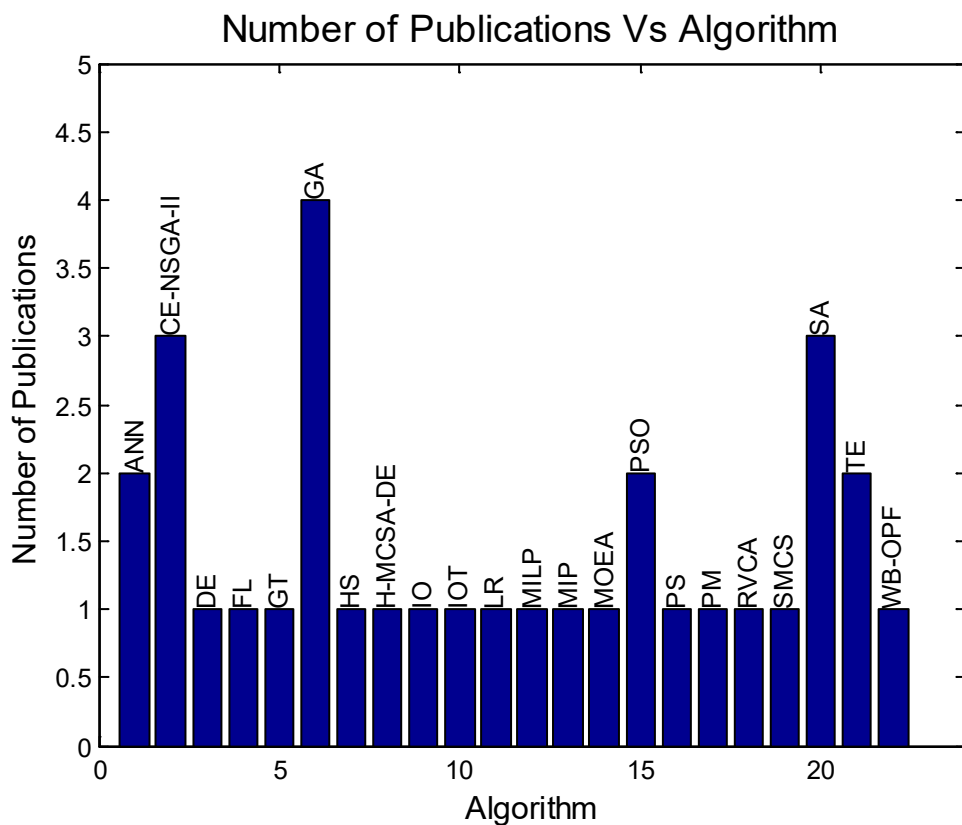


Figure 2.13: The quantity of papers pertaining to the HRES economic dispatch algorithms

Table 2.6 provides a summary of the review for single-area, single-criteria, and multi-criteria hybrid renewable systems.

Table 2.6: Study of the literature for single and multi-criteria mix renewable energy systems.

Reference Paper	System Component						Objective Function		Constraints		Algorithm	Software	Power System Considered	Real life implementation
	PV Panel	Wind	Fuel cell/other	Hydro Power	Storage	Diesel & Other	Single objective	Multi objective	Equality Constraints	Inequality Constraints				
(Lu & Shahidehpour, 2005)	Yes	Nil	Nil	Nil	Yes	Yes	Minimize operation cost	Nil	State of charge power balance and power balance constraints	State of charge limits. Charge/discharge current limits. Output power limits	Lagrangian	Not mentioned	Eight-bus system.	No
(Liang and Liao., 2007)	Yes	Yes	Nil	Yes	Yes	Yes	Nil	Minimize operation cost and emissions	Power balance constraints	Spinning reserve constraints for hydro and thermal units. Capacity limits for thermal generator with and without prohibiting zones. Min/max of water volume released from each reservoir. Power output limits of the wind energy system. Power output limits on the solar energy system.	Fuzzy optimization method	MATLAB	Not specified	No
(Diaf et al., 2008)	Yes	Yes	Nil	Nil	Yes	Yes	Optimum size of the system, able to fulfil the energy requirements of a given load distribution	Nil	Power balance equations constraints	Maximum and Minimum allowable storage capacity constraints. Min/Max constraints of PV and wind generator systems	Techno-economic optimisation method	Not specified	Three selected sites located in Corsica Island (Calvi, Ajaccio, and Cape Corse)	No

(Duflo-Lopez, & Bernal-Agustin., 2008)	Yes	Yes	Nil	Nil	Yes	Yes	Nil	Minimise cost and emission, and unmet load	Power balance constraints	Maximum and Minimum allowable storage capacity constraints. Min/Max constraints of PV and wind generator systems	Multi-Objective Evolutionary Algorithm (MOEA) and a Genetic Algorithm (GA)	Not Specified	PV-Wind-Diesel-Hydrogen-Battery system in Zaragoza	No
(Kaviani et al., 2009)	Yes	Yes	Nil	Nil	Yes	Yes	Minimize operation cost.	Nil	Power balance constraints	Minimum and Maximum capacity of PV, WT, electrolyser, hydrogen tank, and Fuel cell.	PSO	MATLAB	System consisting of 14 wind generating units and 199 Photovoltaic arrays.	No
(Giannakoudis et al., 2010)	Yes	Yes	Nil	Nil	Yes	Yes	Minimize operation cost. Two different case studies were used, with changing design variables and uncertain parameters. The load was either constant or variable.	Nil	Power balance constraints	Minimum and Maximum capacity of Diesel, PV, WT, electrolyser, hydrogen tank, and Fuel cell.	SA	Grid computing environment	(i) Case I: 21 PV panels, 7 wind turbines, 15 Accumulators, one Fuel cell, and 0.3 Buffer tank. (ii) Case II: 27 PV panels, 11 wind turbines, 6 Accumulators, one Fuel cell, and 0.2 Buffer tank.	No
(Kaabeche et al., 2011)	Yes	Yes	Nil	Nil	Yes	Nil	Minimize operation cost.	Nil	Nil	Minimum and Maximum capacity of PV, WT. State of charge(SOC) minimum and maximum of the battery bank.	Iterative optimization technique	MATLAB	Arco-Solar with a max power rating of 43W, an AIR 403 wind turbine with 400W of rated power, and a Varta Solar battery with 100Ah capacity	No

(Mei,et al., 2012)	Yes	Yes	Nil	Nil	Yes	Nil	Nil	Minimise the total cost of generation and maximize the annual power selling income. To minimize the payment for power loss	Real power balance constraints	The battery's energy shouldn't be below the minimum permitted storage level. Also, it shouldn't exceed the batteries' planned capacity.	Game theory	Not specified	A fictitious hybrid power system consisting of wind turbines and PV panels.	No
(Basu et al., 2012)	Nil	Nil	Yes	Nil	Nil	Yes	Nil	Minimize fuel cost and emissions	Real power balance constraints	Bus Voltage Tolerance Limit. Limit on the active and reactive power Generation of the DERs. Line Flow Limits.	Differential Evolutionary	MATLAB	14-bus radial micro-grid With 4 DERs.	No
(Abul'Wafa, 2013)	Yes	Yes	Nil	Nil	Nil	Yes	Nil	Minimize operating cost with valve-point loading and emission functions.	Real power balance constraints	Minimum and maximum operational constraints for solar, wind, and conventional generating systems.	Controlled elitist NSGA-II (CE-NSGA-II)	MATLAB	Six Fossil-Fuel-Fired generators (FFGs), two Wind Energy Conversion Systems (WECS), and two photovoltaic (PV) systems are used.	No
(Bilil et al, 2014)	Yes	Yes	Nil	Nil	Nil	Yes	Nil	Minimize fuel cost and emission	Real power balance constraints	Min/Max magnitude voltage and active power.	Controlled elitist NSGA-II (CE-NSGA-II)	Not restricted	IEEE 30-bus test system in two cases, with and without Renewable Energy Sources(RESs).	No
(EIDesoky, 2014)	Yes	Yes	Nil	Nil	Nil	Yes	Minimize operating cost.	Nil	Real power balance constraints	Real power operating limits of thermal, wind and PV generating units. Unit minimum up/down (MUT/MDT) time for thermal generating units.	Artificial Neural Network (ANN)with Genetic Algorithm	MATLAB	Modified IEEE 24-bus system without hydro generation. Its transmission network consists of 24-bus location connected by 38	No

										The transmission line constraints. The ramp rate constraints for thermal generating units	(GA) and a priority list (PL), ANN/GA/PL.		lines and transformers.	
Arabali et al., 2014)	Yes	Yes	Nil	Nil	Yes	Nil	Minimize operating and maintenance cost.	Nil	Real power balance constraints	Storage Constraints. Min/Max operational constraints of Wind and PV units.	A pattern search-based optimization method is used in conjunction with a sequential Monte Carlo simulation (SMCS)	Not specified	Not specified	No
(Belmili et al., 2014)	Yes	Yes	Nil	Nil	Yes	Yes	Minimise cost of the system	Nil	Real power balance constraints	Storage Constraints. Min/Max operational constraints of Wind and PV units	Techno-economic Algorithm	HOMER	Not specified	No
(Som & Chakraborty., 2014)	Yes	Yes	Yes	Nil	Yes	Nil	Minimize the total operating cost	Nil	Real power balance constraints	Upper and lower limits of DERs	Real Valued Cultural Algorithm (RVCA)	Not specified	Two different cases of DERs, i.e., case 1 Biomass Gasifier Unit (BMGU) and Solar Photovoltaic System (SPS) as DERs) and case 2 Phosphoric Acid Fuel Cells (PAFC)and SPS as DERs) was conducted.	No
(Maleki & Askarzadeh., 2014)	Yes	Yes	Yes	Nil	Yes	Nil	Minimise the total annual cost	Nil	Power balance constraints	Upper and lower limits of DERs	Harmony Search(HS) and Simulated	MATLAB	System with PV, wind turbine and battery storage	No

											Annealing(SA)			
(Shayeghi et al.,2015)	Yes	Yes	Nil	Nil	Yes	Nil	Nil	Minimise cost and emission	Power balance constraints	Upper and lower limits of DERs	Artificial Bee Colony (ABC)	MATLAB	System with PV, wind turbine and battery storage	No
(Arriagada et al., 2015)	Yes	Yes	Nil	Yes	Nil	Yes	Minimise fuel cost	Nil	Power balance constraints	Min/Max constraints for wind, PV and thermal generating units.	Probabilistic Method	MATLAB	17 thermal units , 205 MW of wind energy, 160 MW of solar PV and 5% and1% of thermal and NCRE failure rates, respectively. The wind turbine model used is 5 MW G132 (cut-in: 3 m/s, cut-off 25 m/s). The solar PV module used is the STP290-24 (290 W nominal power) and PV inverter used isSC 500HE (500 kW rated power).	Yes
(Azizipannah-Abarghoee et al., 2015)	Yes	Yes	Nil	Nil	Nil	Yes	Minimizing both the operation cost and risk level	Nil	Power balance constraints Heat balance constraint	Min/Max constraints for wind, PV, thermal, and CHP generating units.	Hybrid MCSA-DE (Modified Cuckoo Search Algorithm And Differential Evolution)	MATLAB	6- and 40-unit test systems respectively.	No
										Ramp rates, operating levels and			The power system consists of three different nodes. (i) Node A, consists of 2x500MW of	

(Plathottam, & Salehfar., 2015)	Yes	Yes	Nil	Yes	Yes	Yes	Minimize the operation cost	Nil	Power balance constraints Transmission losses.	min/max constraints of the conventional units. Min/max reservoir volumes of hydro plants. Min/Max operating constraints of DERs. Conventional Spinning reserves	Simulated Annealing(SA) and Particle Swarm Optimization(PSO) algorithms	MATLAB	thermal plant, Load (30%&20%) (ii) Node B consists of 4x200MW of Hydro plant and distributed solar PV of 200MW with 20% load. (iii) Node C, consists of 50MW of pumped hydro, 500MW of wind farm, load(20%) and tie line connecting neighboring control area	No
(Malheiro et al.,2015)	Yes	Yes	Nil	Nil	Yes	Yes	Cost Minimisation	Nil	Power balance constraints	Min/Max output power of wind, and PV. Min/max permissible storage of the battery.	Mixed Integer linear Programming(MIP)	GAMS	The study consists of Diesel, PV, and wind generating units	No
(Atia & Yamada.,2016)	Yes	Yes	Nil	Nil	Yes	Yes	Reduce operation cost.	Nil	Power balance constraints	Dispatched power by the maximum available generation for PV and WECS constraints. maximum contracted power constraints. Min/Max SOC for BESS	Mixed Integer linear Programming(MIP)	MATLAB	A residential microgrid in Okinawa with a daily demand of 4000 kWh.	No
(Cao et al., 2016)	Nil	Yes	Nil	Nil	Nil	Yes	Minimize the generation costs.	Nil	Power balance constraints Transmission losses.	Min/Max reactive and active power for thermal generators. Wind generator Min/max constraints.	Weather-Based Optimal Power Flow (WB-OPF) algorithm	MATLAB/MATPOWER	Modified the IEEE 9-node system and the New England transmission Grid system	No
							Maximize the utilization of wind energy and minimize	Nil		Min/Max generator limits. Min/Max SOC constraints and	Genetic Algorithm-BP (GA-BP) neural		The system consists of a wind turbine, a PV	

(Guo et al., 2016)	Nil	Yes	Nil	Nil	Yes	Yes	the consumption of diesel fuel.		Power balance constraints	high/low constraints. Minimum start-up time of the desalination system.	SOC	network-based wind speed forecasting method	MATLAB/RSCAD	panel, and a battery bank.	Yes
(Kamjoo et al., 2016)	Yes	Yes	Nil	Nil	Yes	Nil	Nil	Minimise the system total cost and maximum reliability index	Power balance constraints	Min/Max charge constraints. Min/Max output power of wind and Solar PV.	State-Of (SOC)	Non-dominated Sorting Genetic Algorithm (NSGA-II)	Not restricted	Case studies	No
(Ogunju yigbe et al.,2016)	Yes	Yes	yes	Nil	Yes	Yes	Nil	Minimise the system total cost and Emission	Power balance constraints	Min/Max charge constraints. Min/Max output power of wind and Solar PV.	State-Of (SOC)	GA	Not specified	PV system, wind turbine system, battery storage, and 3-split small-rated Diesel generators	No

2.4 Multi-area wind-thermal economic dispatch

The multi-area/interconnected power system focuses on moving the electricity from one region to another because the purchase and sale of electricity is a market-oriented agreement between two parties to reach an economically viable agreement (Zhu, 2015). The tie-line connects two or more separate areas of the power system, as shown in Figure 2.14.

The results of the literature review are compiled in Table 2.7 for the multi-area wind-thermal economic dispatch. Figure 2.15 represents Table 2.7 visually. This figure represents the number of papers per year.

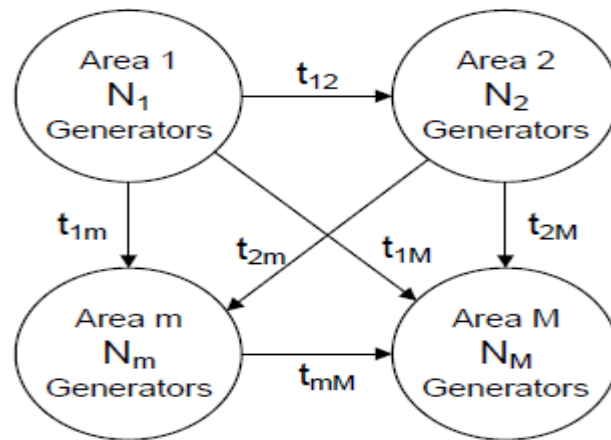


Figure 2.14: Interconnected power system(Krishnamurthy & Tzoneva, 2016)

Table 2.7: Quantity of papers for the multi-area dispatch problem on a yearly basis

Number of publications year-wise		
Reference	Year of publication	Number of publications
(Wang & Shahidehpour.,1992)	1992	1
(Streiffert, 1995)	1995	1
(Jayabarathi, 2005)	2005	1
Jeyakumar et al., 2006),	2006	1
(Wang & Singh., 2007).	2007	1
(Manoharan et al., 2009), (Manoharan et al., 200ba), (Wang, & Singh., 2009), (Fesanghary & Ardehali.,2009)	2009	4
(Chen & Wang., 2010).	2010	1
(Sharma et al., 2011), (Somasundaram & Swaroopan., 2011)	2011	2
(Basu, 2013), (Soroudi, & Rabiee., 2013), and (Krishnamurthy., 2013)	2013	3
(basu, 2014)	2014	1
(Jadoun et al., 2015), (Secui et al., 2015),and (Pandit et al., 2015)	2015	3
(Ghasemi et al., 2016)	2016	1

(Basu., 2019)	2019	2
(Chaudhary et al.,2020)	2020	1
(Sakthivel et al., 2021)	2021	1
(Ahmed et al.,2022)	2022	1
(Lotfi.,2023)	2023	1
Wang et al.,(2025),	2025	1

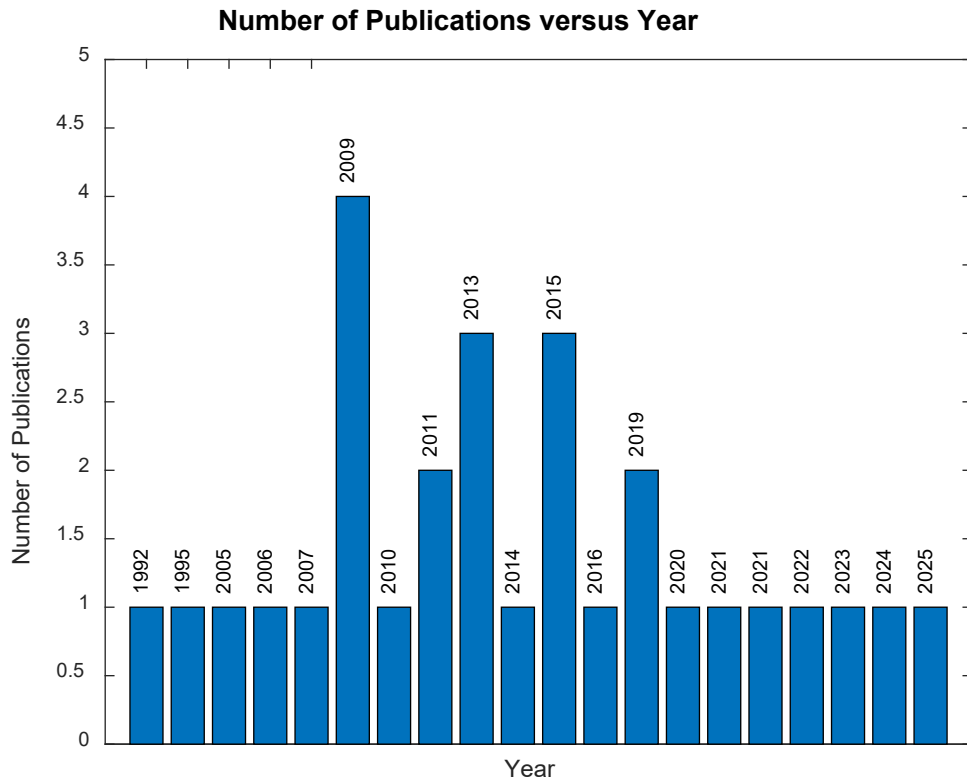


Figure 2.15: Quantity of papers for the multi-area wind-thermal dispatch problem on a yearly basis.

Table 2.8: Techniques and algorithms applied to solve the multi-area wind-thermal economic dispatch problem

Most used methods and algorithms		Reference paper	No. of publications
Algorithm	Abbreviation		
Artificial bee Colony	ABC	(Basu, 2013)	1
Chaotic Global Best Artificial Bee Colony algorithm	CGBABC	(Secui et al., 2015),	1
Covariance Matrix Adapted Evolution Strategy	CMAES	(Manoharan et al., 2009)	1
Differential Evolution	DE	Manoharan et al., 2009), (Sharma et al., 2011),	2

Dynamically Controlled Particle Swarm Optimisation	DCPSO	(Jadoun et al., 2015).	1
Evolutionary Programming	EP	(Jayabarathi., 2005)	1
Evolutionary Programming with Levenberg-Marquardt Optimization	EP-LMO	(Manoharan et al., 2009b)	1
Expert systems	ES	(Wang & Shahidehpour., 1992)	1
Fuzzified Particle Swarm Optimisation	FPSO	(Wang & Singh., 2007) (Somasundaram & Swaroopan., 2011)	2
Harnomy Search	HS	(Fesanghary & Ardehali.,2009)	1
Hybrid Differential Evolution Particle Swarm Optimisation	DEPSO	(Ghasemi et al., 2016)	1
Multi-Objective Particle Swarm Optimisation	MPSO	(Wang & Singh, 2009).	1
Network Flow Programming	NFP	(Streiffert, 1995)	1
Optimality Condition Decomposition	OCD	(Soroudi, & Rabiee., 2013), and (Krishnamurthy, 2013)	2
Particle swarm optimisation	PSO	(Jeyakumar et al., 2006), (Chen & Wang, 2010). (Sharma et al., 2011), Manoharan et al., 2009)	4
Real-coded Genetic Algorithm,	RGA	(Manoharan et al., 2009)	1
Teaching-Learning-Based Optimisation	TLBO	(Basu, 2013)	1
Nondominated Sorting Genetic Algorithm-II (NSGA-II)	NSGA II	(Basu., 2019)	1
Chaotic Fast Convergence Evolutionary Programming (CFCEP)	CFCEP	(Basu., 2019)	1
Salp Swarm Algorithm (SSA)	SSA	(Chaudhary et al.,2020)	1
Multi-Objective Squirrel Search Algorithm (MOSSA)	(MOSSA)	(Sakthivel et al., 2021)	1
Crow Search Optimization algorithm (CSOA)	CSOA	(Ahmed et al.,2022)	1
Modified Grasshopper Optimization (MGO)	(MGO)	(Lotfi,2023)	1
Semi-Definite Programming(SDP)	SDP	(Alli.,2024)	1
Fractional order refined comprehensive learning (FORCL) LSHADE	(FORCL) LSHADE	(Wang et al.,2025),	1

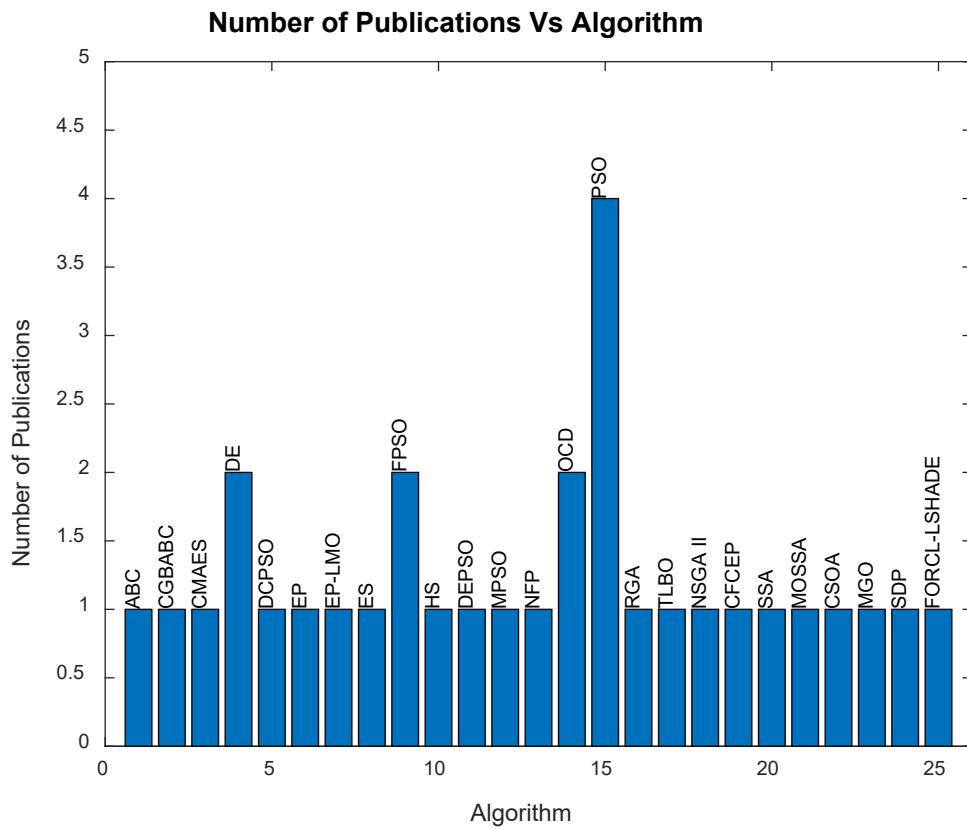


Figure 2.16: Quantity of papers for the multi-area wind-thermal dispatch problem versus the algorithm

2.4.1 Study on mathematical models and techniques applied to resolve the multi-area wind-thermal economic dispatch

2.4.1.1 Single-criteria

Many researchers have solved the multi-area economic dispatch problem using the incremental cost method, decomposition method, incremental network flow, etc. In a medium-sized power system, solution times may be fast and efficient. However, in a larger, interconnected power system, the solution space and computational burden may increase due to the higher dimensionality of the optimization problem. To reduce computational burden, new hybrid optimisation methods are used.

The multi-area dispatch problem is solved using incremental network flow programming in (Streiffert, 1995). The tie line between two areas in a multi-area power system, along with the power balance equality and inequality constraints of a conventional generator, is formulated. In the work of (Sharma et al., 2011), the dispatch problem is formulated as a multi-area reserve-constrained problem. The objective function included both generator and transmission line power flows, subject to the linear area power balance excluding losses, and nonlinear constraints such as generating limits, ramp-rate limits, prohibited zones, tie-line limits, and area-wise spinning reserves. PSO and DE optimisation methods are used to solve the MAED, and the quality of the solutions is

compared with that reported in the existing literature. The authors (Basu, 2013, 2014; Fesanghary & Ardehali, 2009) solved the MAED with the transmission losses included in the power balance constraints. The Artificial Bee Colony (ABC), Teaching-Learning-Based Optimization (TLBO), and Harmony Search (HS) algorithms were used to solve an optimization problem involving multiple fuels. A Dynamically Controlled Particle Swarm Optimization (DCPSO) is used to solve the multi-area dispatch problem, and is formulated with the quadratic fuel cost with valve point loading effect, area power balance is considered without transmission losses, generator limits, and nonlinear area spinning reserves constraints, and multi-area tie-line security limits are considered in (Jadoun et al., 2015).

In the research work of the authors (Manoharan, Kannan, Baskar, et al., 2009; Manoharan, Kannan, & Ramanathan, 2009) The multi-area optimisation problem is solved using Real-Coded Genetic Algorithm (RGA), Particle Swarm Optimization (PSO), Differential Evolution (DE), and Covariance Matrix Adapted Evolution Strategy (CMAES). Their solutions are compared with the Direct Search Method (DSM) and the Hopfield Neural Network (HNN), Evolutionary Programming (EP), and the Nelder–Mead simplex (NMS). The optimum values of the PSO method are validated using the Karush–Kuhn–Tucker (KKT) condition and Evolutionary Programming with Levenberg–Marquardt Optimization (EP-LMO). The improved Hopfield neural network approach is adopted to solve the economic dispatch problem of a multi-area system, considering power transfer security constraints, transmission losses, and power balance constraints (Yalcinoz & Short, 1998). In the research work of the authors (Somasundaram & Swaroopan, 2011) PSO is amended with fuzzy logic to form a fuzzified particle swarm optimisation method to solve the security-constrained Multi-Area Economic Dispatch (MAED) in order to obtain an optimal pareto solution. The security constraints for tie-line, generator limits, and power balance constraints with transmission losses are considered in their research work.

2.4.1.1 Multi-criteria

Recently, hybrid optimisation techniques have gained popularity. In (M. Ghasemi et al., 2016), the authors integrated Differential Evolution (DE) and Particle Swarm Optimisation (PSO) to develop a hybrid Differential Evolution Particle Swarm Optimisation (DEPSO) to address the Multi-Area Economic Load Dispatch (MAED). In (Secui, 2015), the Multi-Area Economic Load Dispatch (MAEED) problem is solved utilising the Chaotic Global Best Artificial Bee Colony Algorithm (CGBABC). The Multi-Objective Particle Swarm Optimisation (MPSO) technique is employed to determine the Pareto optimal solutions for the MAEED problem, which is intended to reduce both fuel cost and emissions (Wang & Singh, 2009). In the research work of authors (Wang

& Shahidehpour, 1992), and (Krishnamurthy & Tzoneva, 2016), the multi-area dispatch problem is explained using a decomposition technique. The multi-area dispatch problem is defined using a decomposition strategy. This includes a top (master problem) and bottom (sub-problems) formation of a two-level decomposed hierarchy as seen in Figure 2.17. Thus, the master problem is broken down into sub-problems, in which the master distributes load demands to the sub-problems, and each area returns its solution as a cost to the system. Thus, the system's minimum operating cost acts as the aggregator at this level. The sub-problems are the sub-areas of the power system network. The subproblem for every network incorporates system λ and provides the network λ , where λ is the tie-line coordinator's variable vector.

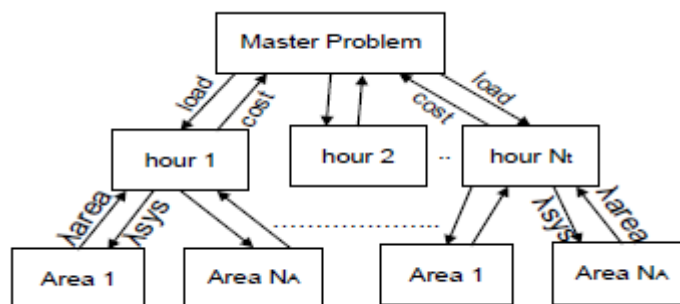


Figure 2.17: Decomposition structure with two levels
(Krishnamurthy & Tzoneva, 2016)

The multi-area economic dispatch problem is extended as a Piecewise Quadratic cost Function with multiple fuels (PQCF) in (Jayabarathi et al., 2005; Jeyakumar et al., 2006) Operating zones (POZ) are identified, and the optimal solution is obtained using Particle Swarm Optimisation (PSO), which is also compared with results from the classical Evolutionary Programming (EP). Furthermore, PSO is used for the MAEED dispatch problem in (Ming Chen & Wang, 2010) where the tie-line and tie-loss constraints between the areas represent additional constraints on the problem.

In addition, emissions are included in the cost function to establish the Multi-Area Nonconvex Combined Economic Emission (MANCEED) dispatch problem (Pandit, Srivastava, et al., 2015; Sharma et al., 2011). Then, the Differential Evolution with Fuzzy Selection (DEFS) is implemented to address the MANCEED problem, using a fuzzy framework. The mutation and crossover processes are optimised to reduce the complexity of multi-attribute decision-making, and a penalty factor technique with a limitation incorporated into the objective function. In the work of Wang and Singh, the MANCEED is solved using the Fuzzified Multi-Objective Particle Swarm Optimisation (FMPSO) technique, which successfully discovered a collection of non-dominated solutions in a single run. Compared with other techniques such as weighted

aggregation and Multi-Objective Evolutionary Algorithms (MOEAs), it is far more effective at obtaining a global optimal solution.

The authors (Soroudi & Rabiee, 2013) published a paper on the multi-area dispatch problem, in which the objective function includes thermal, hydrothermal, and wind units, as well as a power-pool market for each area. The Optimality Condition Decomposition (OCD) method is used to solve this power system. The MAED problem is first decomposed into simple sub-problems, each representing a single area. This results in less computation time. Parallel computing is used to improve the computational time required to solve the MAED dispatch optimisation problem.

In (Basu, 2019a) The optimisation problem for MAWTEED is formulated using the power balance and inequality constraints, including power losses, tie-line power limits, and minimum and maximum power limits for hydro, thermal, and wind power plants. The problem is presented as a nonlinear optimisation with a non-smooth quadratic cost function and ramp-rate constraints. A Nondominated Sorting Genetic Algorithm-II (NSGA-II) is used to solve the problem. The method's performance is tested across a network of four Reservoir Hydro Plants in a multi-chain cascade, along with ten conventional power plants and two wind power plants in each region. Each region has its own load demand, and regions are interconnected through tie lines with other regions.

The same author (Basu, 2019b), extended the multi-area problem now including solar in the cost function and tested the effectiveness of chaotic fast convergence evolutionary programming (CFCEP) first using a three-area test system, that consists of a multi-chain cascade of four reservoir hydro plants, one wind power, solar PV, ten thermal power plants with Valve Point Loading Effect (VPLE) and one pumped hydro energy storage power plants. Secondly, using forty generating units and dividing the power system into four areas with different power demands of 15%, 40%, 40%, and 15% of the maximum demand of 10500MW. Lastly, using a 140-unit test system with a load demand of 49 342MW.

A Salp Swarm algorithm (SSA) is used to solve the MAWTEED problem where the effectiveness of the optimisation method is verified with different case studies, first case consists of 4 areas with four generators each, second has forty units divided into four areas and third has 2 areas with 20 generators each, fourth has two area network that consists of forty units with 20 units in each area, and three wind thermal having 110MW. In (Ahmed et al., 2022), the multi-area power system is formulated as a power balance problem with inequality constraints and tie-line limits. The problem includes thermal, wind, and solar generating units. The problem uses the Crow Search Optimization

(CSOA) algorithm. This optimization algorithm is validated using different test systems, as illustrated in Table 2.9 below.

(Wang et al., 2025) formulated an MAWTEED problem with thermal, wind, and solar power systems. The power balance and inequality constraints are included in the constraints. A WDF and a lognormal distribution are used to model uncertainty in wind power and solar power, respectively. A Fractional order refined comprehensive learning (FORCL) LSHADE is used to determine the optimal values of fuel and emissions during the optimization process. The algorithm is validated with a test system having 3 areas with 10 units, including VPE, MFO, and the following cases are examined: case(i) No solar and wind power, only thermal generation, case (ii) Both solar and wind power are considered. Test system II has four areas and 40 generating units, 10 units in each area, and the following cases are considered: case (i) No Solar and Wind Power units. Case(ii) Both Wind and Solar are included. Test System III includes a practical provincial power system in China with 46 units. The case includes one without wind or solar power, and the latter includes both.

(Sakthivel et al., 2024) developed a Multi-Objective Squirrel Search Algorithm (MOSSA) to solve a multi-objective optimisation problem with multiple fuels and valve-point effects. The problem is validated through different case studies: one with 10 units and three areas, another with 40 units and four area systems, and, lastly, a complex 140-unit Korean power system that considers valve-point effects and multiple fuels.

(Alli, 2024) used the Semi-Definite Programming (SDP) method to solve a multi-area wind-thermal economic dispatch problem. Both equality and inequality constraints are included in the nonconvex optimization problem. The algorithm's effectiveness is first tested on a two-area, six-unit system with three generators in each area, without wind power. Secondly, in a two-area system with 40 generating units (20 in each area), without wind power. Lastly, tested on a two-area system with 40 generating units in each area, three conventional units are replaced by identical wind power units of 110MW each.

In (Lotfi, 2022), a multi-objective optimization problem is solved using the Modified Grasshopper Optimization (MGO) algorithm. The power balance and inequality constraints are considered as presented in Table 2.9. A 10- and 40-unit system with 3 zones is used to validate the algorithm. The algorithm is then contrasted with other heuristic algorithms reported in the survey.

2.4.2 Multi-area economic emission dispatch problem formulation

The goal of Multi-Area Wind-Thermal Dynamic Economic Dispatch (MAWTDEED) is to reduce total emissions from thermal units; limit the power outputs of thermal units and

wind farms in each region; and allow power transfer among power generation regions. This is mathematically formulated (Ghasemi et al., 2016; Hetzer et al., 2008; Ming Chen & Wang, 2010; Secui, 2015).

$$F_{mai}(P_{gi}, P_w, E_i) = \sum_{ma=1}^M \sum_{i=1}^n F_{wmai} + F_{Tmai} \quad [$/h] \quad (2.64)$$

Where n is the number of online generators for the area ma is represented by n in a M area generation unit. F_{wmai} is the total amount of power that the wind generating units can produce. F_{Tmai} is a combined economic emission dispatch objective function provided by equation (2.60). The following equality and inequality limitations bind the objective function. The overall power balance must equal the demand for power per area, including power flows to and from other areas. This is mathematically expressed as:

$$\sum_{i=1}^n P_{mai} - \sum_{\substack{m=1 \\ m \neq k}}^M [t_{mak} - (1 - \rho_{kma}) \times t_{kma}] - P_{D,ma} - P_{L,ma} = 0 \quad [$/h] \quad (2.65)$$

In this particular instance P_{mai} , represents the output power from combined thermal and wind generators, as shown by equation (2.64). The following are the tie-line limits:

$$t_{kma}^{\min} \leq t_{kma} \leq t_{kma}^{\max} \quad (2.66)$$

Where

t_{kma} Power transfer through a tie-line

ρ_{kma} Transfer loss ratio through the tie-line

t_{kma}^{\max} and t_{kma}^{\min} Maximum and Minimum power transfer capacity limits through the tie-

line

Other limitations are similar to those mentioned in the previous formulation of the single-area dispatch problem. Table 2.9 summarises the review for single, multi-objective, and multi-area economic dispatch.

Table 2.9: Multi-area review papers for single and multi-criteria dispatch problem

Reference	System Component				Objective function		Constraints		Multi-area constraints	Algorithm	Software	Power system considered	Real-time implementation
	Wind	PV	Hydro	Diesel	Single	Multi	Equality	Inequality					
(Streffert., 1995)	Nil	Nil	Nil	Yes	Fuel cost minimisation	Nil	Real power balance with transmission line constraints.	Minimum and maximum power limits for a conventional generator. Minimum and maximum tie line limits	Min/Max tie line flow limit	Network flow programming	Not mentioned	T Three case studies were done on a four-area network system with four generators.	No
(Sharma et al., 2011)	Nil	Nil	Nil	Yes	Fuel cost Minimisation with valve point loading effect	Nil	Real power balance	Generating limits. Ramp rate limit. Prohibiting zones. Area-wise spinning reserves	Min/Max tie line flow limits	Particle swarm optimisation(PSO) and Differential evolution(DE)	MATLAB	Two area networks, each with two generators. Four area power system with four generators in each area. Two-area, 40-unit system.	No
(Basu, 2013)	Nil	Nil	Nil	Yes	Fuel cost Minimisation with valve point loading effect with multiple fuels	Nil	Real power balance with transmission line constraints.	Generating limits. Ramp rate limit. Prohibiting zones. Area-wise spinning reserves	Min/Max tie line flow limits	Artificial Bee Colony(ABC)	MATLAB	Three different test systems were used. (i) The first system consists of two areas with three generators in each area, with prohibiting zones. Transmission line considered (ii) The second system consists of three areas, with area 1 having 4 units, area 2 having 3, and area 3 having the last 3.	No

												(iii) The third system consists of four areas; each area consists of 10 units to make a total of 40 generating units.	
(Basu, 2014)	Nil	Nil	Nil	Yes	Fuel cost Minimisation with valve point loading effect with multiple fuels	Nil	Nil	Generating limits. Ramp rate limit. Prohibiting zones. Area-wise spinning reserves	Min/Max tie line flow limits	Teaching-Learning-Based Optimisation(TLBO)	MATLAB	Three different test systems were used. The first system comprises two areas, each with three generators, and includes prohibiting zones. The second system has three areas: area 1 has 4 units, area 2 has 3, and area 3 has the last 3. (iii) The third system consists of four areas; each area consists of 10 units to make a total of 40 generating units.	No
(Jadoun et al., 2015).	Nil	Nil	Nil	Yes	Fuel cost Minimisation with valve point loading effect.	Nil	Nil	Generating limits. Ramp rate limits. Area-wise spinning reserves	Min/Max tie line security limits	Dynamically Controlled Particle Swarm Optimisation(DCPSO)	MATLAB	Three case studies are considered. Case study 1 has two areas with two generators each. Case study 2 has 4 areas with 10 generators each. Case study 3, with, consists of 5 areas with 28 generators in each area.	No
(Manoharan et al., 2009)	Nil	Nil	Nil	Yes	Fuel cost Minimisation with multiple fuels	Nil	Real power balance with the	Generating limits. Ramp rate limit.	Min/Max tie line power flow limits	Real-coded Genetic Algorithm (RGA), Particle Swarm	MATLAB	Case 1: 4-unit system with two areas. Case 2: 10-unit system including multi-fuel options with three areas.	No

							transmission line	Area-wise spinning reserves		Optimization (PSO), Differential Evolution (DE), and Covariance Matrix Adapted Evolution Strategy (CMAES)		Case 3: 120-unit large-scale system with two areas.	
(Ghasemi et al., 2016)	Nil	Nil	Nil	Yes	Nil	Fuel cost Minimization with valve point loading effect with multiple fuels and emissions	Real power balance with transmission line constraints	Generating limits. Ramp rate limit. Area-wise spinning reserves. Prohibiting zones	Min/Max tie line power flow limits.	Differential Evolution Particle Swarm Optimisation (DEPSO)	MATLAB	4 area systems with 16 generators and two area networks with 40 units.	No
(Secui., 2015)	Nil	Nil	Nil	Yes	Nil	Fuel cost Minimization with valve point loading effect with multiple fuels and emissions	Real power balance with transmission line constraints	Generating limits. Ramp rate limit. Area-wise spinning reserves. Prohibiting zones	Min/Max tie line power flow limits.	Chaotic Global Best Artificial Bee Colony algorithm (CG BABC)	Mathcad	(i) 3 area systems with 10 generators. (ii) 4 areas network with 40 units.	No
(Wang, & Singh., 2009)	Nil	Nil	Nil	Yes	Nil	Fuel cost Minimization and emission	Real power balance constraints	Generating limits. Ramp rate limit. Area-wise spinning reserves.	Min/Max tie line power flow limits.	Multi-Objective Particle Swarm Optimisation (MOPSO)	MATLAB	Four areas with 4 generators in each area	No

								Prohibiting zones					
(Wang & Shahidehpour., 1992)	Nil	Nil	Nil	Yes	Fuel cost function minimisation	Nil	Real power balance constraints.	Generating limits. Ramp rate limit. Area-wise spinning reserves. Prohibiting zones	Tie-line active power flow limits	Expert systems	Not Mentioned	4 area system with 26 units in each area	No
(Manoharan et al., 2009)	Nil	Nil	Nil	Yes	Fuel cost Minimization with multiple fuels	Nil	Real power balance with transmission line constraints	Generating limits. Ramp rate limit. Area-wise spinning reserves	Min/Max tie line power flow limits	The Evolutionary Programming with Levenberg-Marquardt Optimization (EP-LMO)	MATLAB	Case 1: 4-unit system with two areas. Case 2: 10-unit system including multi-fuel options with two areas.	No
(Jeyakumar et al., 2006),	Nil	Nil	Nil	Yes	Fuel cost Minimization with multiple fuels. Four different examples to illustrate the effectiveness of PSO, with MAED, MAPQCF, MACEED, and MAED with prohibiting zones	Fuel cost Minimization with multiple fuels and emissions	Real power balance with the transmission line	Generating limits. Prohibiting zones	Min/Max tie line power flow limits	Particle Swarm Optimisation(PSO)	MATLAB	(i) Four-area system interconnected by six tie lines. (ii) Ten generating units, each with an area of four areas, with three types of fuel. (iii) Six generating units, considering emission and transmission (iv) a fifteen-unit power system with four of the units having up to three prohibited operating zones.	No
					Fuel cost reduction with multiple fuels. Four different examples to	Fuel cost	Real power				MATLAB	(i) Four-area system interconnected by six tie lines. (ii) Ten generating units, each with an	

(Jayabarathi, 2005)	Nil	Nil	Nil	Yes	illustrate the effectiveness of PSO, with MAED, MAPQCF, MACEED, and MAED with prohibiting zones	reduction with multiple fuels and emissions	balance with transmission line constraints	Min/Max generator limits. Prohibiting zones	Power flows from one area to other minimum and maximum values	Evolutionary Programming (EP)		area of four areas, with three types of fuel. (iii) Six generating units, considering emission and transmission (iv) a fifteen-unit power system with four of the units having up to three prohibited operating zones	No
(Somasundaram & Swaroopan., 2011)	Nil	Nil	Nil	Yes	Minimise fuel cost	Nil	Power balance and Transmission losses constraints	Min/Max generator limits.	Tie-line power flow limits	Fuzzified Particle Swarm optimisation	Not Mentioned	Three-area 32-bus system.	No
(Fesanghary & Ardehali., 2009)	Nil	Nil	Nil	Yes	Fuel cost minimisation	Nil	Power balance and Transmission losses constraints	Min/Max generator limits. Prohibited zones. Ramp rate limit	Tie-line power flow limits	Harmony Search (HS) algorithm	Visual C++	Six different case studies are studied. (i) Standard MAED with 38 units. (ii) ED problem with valve-point loading effect with 13 generating units. (iii) ED problem with prohibited operating zones with 15 units MAED with tie line flow limits in four area network. (iv) ED problem with ramp-rate limits, with 6 units having ramp rate and prohibited zone limits.	No

(Chen & Wang, 2010).	Nil	Nil	Nil	Yes	Nil	Fuel cost reduction and emission	Power balance Transmission losses	Min/Max generator	Tie-line power flow limits.	PSO	MATLAB	EEE 30-bus system with 6 generators	No
(Pandit et al., 2015),	Nil	Nil	Nil	Yes	Nil	Minimise fuel and emission	Power balance Transmission losses	Prohibiting zones. Area-wise spinning reserves. Generator capacity constraints	Tie-line power flow limits.	Differential Evolution with Fuzzy Selection (DEFS)	MATLAB	Four area network system with 16 generators.	No
(Wang & Singh., 2007)	Nil	Nil	Nil	yes	Nil	Fuel cost reduction and emission	Power balance. Transmission losses	Generator capacity constraints	Tie-line power flow limits.	Fuzzified Multi-Objective Particle Swarm Optimisation (FMOPSO)	C++	IEEE 118-bus test system with 14 generators	No
(Soroudi, & Rabiee., 2013)	Yes	Nil	Yes	Yes	Fuel cost minimisation	Nil	Power balance. The purchased power from the pool market	Wind and thermal generator limits. reservoir volume min/max constraints	Tie-line power flow limits.	Optimality Condition Decomposition (ODC)	GAMS environment solved by the CONOPT solver	Case I: three interconnected systems with assumed power generated by wind, hydro, and the power pool. Case II used five interconnected areas, with given power generation from wind, hydro, and pool market	Yes
(Basu., 2019)	Yes	Nil	Yes	Yes	Nil	Fuel cost reduction and emission	Power balance. Transmission losses	Wind and thermal generator limits. reservoir volume min/max constraints	Tie-line power flow limits.	Nondominated Sorting Genetic Algorithm-II (NSGAI)	MATLAB	Comprises a multi-chain cascade of four reservoir hydro plants, ten conventional, and two wind power energy systems in each area.	No

Basu.,2019)	Yes	Nil	Yes	Yes Solar and therm al	Nil	Fuel cost reductio n and emissio n	Power balance. Transmis sion losses	Wind and thermal generator limits. reservoir volume min/max constraints, ramp rate constraints	Tie-line power flow limits.	Chaotic Fast Convergence Evolutionary Programming (CFCEP)	MATLAB	Comprises a multi- chain cascade of four reservoir hydro plants, ten conventional, one wind, and solar power energy systems in each area. A four- area, 40 units with ten generators in each area. 140 unit 12 areas and 12 generators in each area	
(Chaudhary et al.,2020)	Yes	Nil	Nil	Yes	Nil	Fuel cost reductio n and emissio n	Power balance. Transmis sion losses	Wind and thermal generator limits.	Tie-line power flow limits.	Salp Swarm algorithm(SS A)	MATLAB	4 areas with 4 generators each, the second has forty units divided into 4 areas and third has 2 areas with 20 generators each, the fourth has two area networks that consist of forty units with 20 units in each area, and three wind thermal have 110MW each	No
(Sakthivel et al., 2021)	Nil	Nil	Nil	Yes	Nil	Fuel cost reductio n and emissio n	Power balance. Transmis sion losses	thermal generator limits.	Tie-line power flow limits	Multi- Objective Squirrel Search Algorithm (MOSSA).	MATLAB	10 units and three areas, another with 40 units and four areas, and a 140-unit Korean power system.	
Ahmed et al.,2022	Yes	Yes	Nil	Yes	Nil	Fuel cost reductio n and	Power balance.	Wind, thermal, and solar	Tie-line power flow limits.	Crow Search	MATLAB	10 units allocated on three areas, Area1 has 4 committed units,	No

						emission	Transmission losses	generator. min/max constraints, ramp rate constraints, Prohibited Operating Zones (POZs), tie-line constraints		Optimization algorithm (CSOA)		Area 2 has 3 conventional units, and Area 3 has 3 as well. This test system has 3 different case studies. Test system II has 40 generating units, and 10 generators in each area. Power demand differs in each area. Test system III, consists of 140 units across the country, where 1–40 units are thermal (mostly coal powered), 41–91 are gas powered plants, 92–111 are nuclear powered plants, and 112–140 They are oil-powered plants. Test system IV has 5 thermal units integrated with two wind turbines and two solar PV systems.	
(Lotfi.,2023)	Yes	Nil	Nil	Yes	Nil	Fuel cost reduction and emission	Power balance. Transmission losses	Wind and thermal generator. min/max constraints. Ramp rate, multi-Fuel option, and Prohibited zones for thermal units.	Tie-line power flow limits.	Modified Grasshopper Optimization (MGO) algorithm	MATLAB	two systems with a 10-unit, 3-zone test system and a 40-unit 3-zone test system,	No

(Alli.,2024)	Yes	Nil	Nil	Yes	Nil	Fuel cost reduction and emission	Power balance. Transmission losses	Wind, and thermal generator. min/max constraints. Ramp rate and prohibited zones of thermal generators	Tie-line power flow limits.	Semi-Definite Programming (SDP)		Two area, six-unit system with three generators in each. Two-area system with 40 generating units, 20 generators in each area. Two-area system with 40 generating units in each area, three of the conventional units are replaced by identical wind power units of 110MW each.	No
Wang et al.,(2025)	Yes	Yes	Nil	Yes	Nil	Fuel cost reduction and emission	Power balance. Transmission losses	Wind, thermal and solar generator. min/max constraints,	Tie-line power flow limits.	Fractional order refined comprehensive learning (FORCL) LSHADE	MATLAB	Test system having 3-areas with 10-units. Test system II, has 4 areas and 40 generating units, 10 units in each area, Test System III, includes a practical provincial power system of China having 46-units.	No

2.5 Outcomes from analysis of the literature

Numerous articles have been reviewed from 1945 to 2026 for single-area wind-thermal, from 2005 to 2025 for single-area hybrid systems, and from 1992 to 2025 for the multi-area wind-thermal economic dispatch problem. Tables 2.3, 2.6, and 2.9 provide the review summaries for these articles. The review emphasises two crucial topics: the algorithm used for addressing a particular type of dispatch problem and the formulation of wind-thermal problems under system inequality and equality constraints.

2.5.1 Examination of the problem formulation applied for solving both single-area and multi-area economic dispatch problems with single and multi-criteria.

The objective function defines the single- and multi-area dispatch problem. For thermal generators, a quadratic function with valve-point loading has been adopted from many recent works, as it's a more realistic approach than a linear-quadratic function. For wind turbine generators, direct, overestimation, and underestimation cost functions have been utilized. The direct one applies to the wind farm, as per ownership. For assessing the emission cost function, a second-order quadratic function, an exponential function, and a linear-quadratic equation can be used. The total area power demand is obtained based on load, transmission losses (tie-line capacity restriction), nonlinear restrictions (prohibited zones), and the max/min output power of thermal and wind generators. The objective function of the multi-area wind-thermal economic dispatch problem is the summation of fuel, wind, and environmental costs, subject to constraints.

2.5.2 Examination of techniques and algorithms applied in solving single-area and multi-area economic dispatch problems with single-and multi-criteria.

The economic dispatch research is evolving towards the implementation of heuristic optimisation methods such as Evolutionary Iteration Particle Swarm optimisation(EIPSO) (Lee, 2007), Gravitational Acceleration Enhanced Particle Swarm Optimisation(GAEP SO)(Jiang et al., 2015), Hybrid Particle Swarm Optimisation (HPSO) (Niu&Wei,.2013), Series Particle Swarm(PSO-DE) Differential Evolution Optimisation(Pandit, Chaudhary, et al., 2015b), Dynamic controlled Particle Swarm Optimisation(DCPSO)(Jadoun et al., 2015), Fuzzified Particle Swarm Optimisation(FPSO) (Wang & Singh, 2007), (Somasundaram & Swaroopan, 2011), and Differential Evolution Particle Swarm Optimisation(DEPSO)(Ghasemi et al., 2016) used as a tool to solve the power system optimisation problems. These optimisation methods are indicated in Figures 2.9, 2.12, and 2.15. Observing from these Figures that the grouping of several optimization techniques is commonly employed to find global optima and reduce the computational time required to solve the entire dispatch problems. A more frequently employed optimisation technique is particle swarm

optimisation. This approach is applied to a wind-thermal economic emission dispatch problem in a multi-area, multi-objective system, where wind is considered an alternative power generation resource, with the relative reduction coefficient of power generation cost and the relative minimization coefficient of emissions. The multi-objective problem is transformed into a single objective using a weighting factor via separation and mutation, a method validated by various researchers in the literature.

2.6 Conclusion

The formulations of the multi-area economic dispatch problem have been discussed. The multi-area economic dispatch problem is formulated with a tie-line real-power controller, and the goal function can be formulated as a single criterion or a multi-criterion, depending on the research purpose. In addition, the multi-area economic dispatch problem is solved by various approaches and algorithms. Heuristic optimization approaches are employed (DEPSO), Differential Evolution Particle Swarm Optimization (Ghasemi et al., 2016). This means that a review is held regarding computation times to determine optimal solutions for different types of economic dispatch problems. The review shows that the MAWTEED problem involves many variables, nonlinear equations, and high dimensionality, resulting in very complex calculations. (Soroudi & Rabiee, 2013). The Optimality Condition Decomposition (OCD) (Krishnamurthy & Tzoneva, 2016; Soroudi & Rabiee, 2013) would allow the problem to be decomposed into a two-level subproblem. Distributed and parallel computing can minimize computation time when algorithms are distributed and parallelized. MAWTEED can be solved using the Lagrange Decomposition Coordinating Method, which is one of the best means of parallelizing a solution, as it decomposes the comprehensive problem into sub-problems whose solutions add up to the comprehensive solution. Thus, optimality is reached.

CHAPTER THREE

WIND-THERMAL ECONOMIC EMISSION DISPATCH(WTEED) PROBLEM USING LAGRANGE'S ALGORITHM

3.1 Introduction

Generation of electricity from fossil fuels pollutes the environment by releasing pollutants such as sulfur dioxide (SO₂), Nitrogen oxides (NO_x), and carbon dioxide (CO₂). The objective of the wind-thermal economic emission dispatch problem in electrical power system generation is to meet the power system equality and inequality constraints while dispatching electrical power to the committed conventional and wind generating units to meet load demand over a specific period. Wind power facilities are crucial to electricity production. These Distributed Energy Resources (DERs) offer an opportunity to substantially reduce production costs and atmospheric pollution.

In this chapter, fuel cost and pollutant reductions are covered, with transmission losses accounted for using the B matrix. The fuel cost and emission quadratic models are expressed without including valve-point loading effects. Both wind and conventional generating unit constraints are considered. The Lagrange's methods, algorithms, and software for the solution of Wind-Thermal Economic Combined Emission Dispatch (WTEED) problems are developed in this Chapter.

The Wind-Thermal Economic Emission Dispatch problem is first formulated in this chapter. The obtained models are then used to develop software to optimize this power dispatch problem. Three experimental IEEE 30-bus systems: 6-unit, 10-unit, and 40-unit are applied to test the developed algorithm.

Different numbers of available wind-generating units are utilised on a cluster of wind farms. Later, the results obtained with the proposed algorithm are compared with those of the existing heuristic algorithm.

3.2 WTEED problem formulation

3.2.1 Wind-thermal economic emission formulation for a single area dispatch problem

The problem formulation for the wind-thermal economic dispatch problem employing a single criterion function is presented. The goal of the Wind-Thermal Economic Emission Dispatch (WTEED) is to reduce the overall operating costs and emissions of the entire generation system, subject to specific operational constraints. The overall cost for conventional and wind generators can be expressed mathematically as (Ghasemi et al., 2016).

$$F(P_g, P_w) = \sum_{i=1}^{N_G} F_i(P_{gi}) + \sum_{j=1}^{N_F} \sum_{k=1}^{N_W} W_{j,k}(P_{w_{j,k}}) \quad (3.1)$$

where, N_G is the quantity of electrical generators, N_F is the number of wind power farms, N_w is the quantity of wind generators, P_{gi} is the active power for electrical generators, and $F(P_g, P_w)$ is the total expense of all generating units. The wind generating units' output power is denoted by the final term in equation (3.1), $W_{j,k}(P_{w_{j,k}})$. The cost function for conventional generating units is given by $F_i(P_{gi})$. It is expressed as in equation (2) and is developed using a quadratic function without a valve-point loading effect (Kothari & Dhillon, 2012). Figure 3.1 demonstrates how the thermal cost function can be represented with or without valve-point loading. The thermal generator loading is illustrated using arrows, as in Figure 3.1.

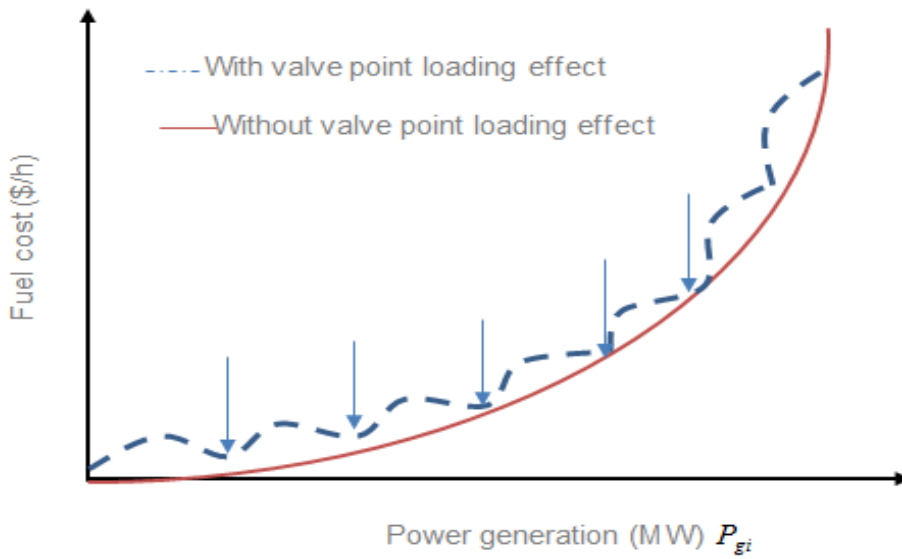


Figure 3.1: Conventional cost curve with or without valve-point loading effect.

$$F_i(P_{gi}) = a_i + b_i P_{gi} + c_i P_{gi}^2 \quad (3.2)$$

Where the fuel cost co-efficient of the i^{th} generators are represented by a_i , b_i , and c_i respectively. Equation (3.3) provides a further representation of the wind power production (A. Ghasemi et al., 2016).

$$W_{j,k}(P_{w_{j,k}}) = \phi_{D_{j,k}} P_{E_{j,k}} + \phi_{OE_{j,k}} \times (P_{A_{j,k}} - P_{E_{j,k}}) + \phi_{UE_{j,k}} \times (P_{E_{j,k}} - P_{A_{j,k}}) \quad (3.3)$$

where $P_{E_{j,k}}$, and $P_{A_{j,k}}$ are the expected and actual/available wind power output of the turbine j in a wind farm k in [MW], $\phi_{D_{j,k}}$, $\phi_{OE_{j,k}}$, and $\phi_{UE_{j,k}}$ are the direct, overestimation, and underestimation cost coefficients of the turbine j in a wind farm k [\$/MWh].

3.2.1.1 The emission cost function formulation

Industrial advancement has caused a significant increase in pollutants to the atmosphere.

When coal is used in the thermal plant utilities, harmful gaseous pollutants such as carbon oxides(CO_2), sulphur oxides(SO_2), and nitrogen oxides(NO_x) are discharged. The Green Power committee suggests using low-emission sources to address the economic dispatch problem. Therefore, there is a need for improved control techniques that can achieve lower pollution levels at a realistic fuel cost. Pollutants such as CO_2 , SO_2 and NO_x . The emissions by conventional generators should be incorporated in the optimisation objective function. Wind generators are not exposed to emissions, and the output power of the wind turbines depends on the wind velocity, so the emission cost for these generators is zero. The total emission of these impurities is the sum of the quadratic cost function and the emission values, multiplied by the exponential function of the valve-point loading effect. This can be expressed mathematically as (Abdelaziz et al., 2016)

$$E_T = \sum_{i=1}^{N_E} E_i(P_i) = \sum_{i=1}^{N_E} (\alpha_i + \beta_i P_i + \gamma_i P_i^2) \quad (3.4)$$

where E_T is the total emission in [kg/h], and the emission coefficients are $\alpha_i, \beta_i, \gamma_i$, for generating units in [kg/h].

(a) Constraints for inequality and equality

(b) Constraints for real power balance

The total of the power demand and transmission line losses equals the output power of the thermal and wind generation units. It can be indicated mathematically as shown in equation (3.5).

$$\sum_{i=1}^{N_G} P_{gi} + \sum_{k=1}^{N_W} P_{wh_{j,k}} = P_D + P_{Loss} \quad (3.5)$$

where, P_D and P_{Loss} are the power system overall load demand, and transmission line losses. Transmission losses in electric power systems are primarily caused by the distribution of electric power over lengthy distances or in vast areas with relatively low load density. Transmission losses must be incorporated into the formulation of the wind-thermal dynamic economic dispatch problem. In (Huang et al., 2018) The transmission loss formula, subsequently termed George's formula, is given by the first quadratic term in equation (3.6). The equation is also known as the loss formula or the B-coefficient technique. A linear term and a constant are added to the quadratic expression to get an improved transmission loss equation (Huang et al., 2018), and is termed Kron's formula and is given in equation (3.6) (Zhang et al., 2019). The B-coefficient technique allows coordination of power losses by arranging each plant's output to increase economy for a specified load.

$$P_L = \sum_{m=1}^{N_G+N_W} \sum_{m'=1}^{N_G+N_W} P_m B_{mm'} P_{m'} + \sum_{m=1}^{N_G+N_W} B_{0m} P_m + B_{00} \quad (3.6)$$

where the wind-thermal generator index is given by m and m' and power loss coefficients given by $B_{mm'}$, B_{0m} and B_{00} respectively.

The following inequality constraints are applicable to the objective function.

Inequality Constraints

Generation capacitor for conventional and wind power constraints

Equations (3.7) and (3.8) provide the operational output power of each generating unit, which is constrained by its minimum and maximum operating capacities.

$$P_{gi}^{min} \leq P_{gi} \leq P_{gi}^{max}, i = 1, 2, \dots, N_g \quad (3.7)$$

$$0 \leq P_{j,h} \leq P_{R,j,h} \quad j = 1, 2, \dots, N_w \quad (3.8)$$

where the maximum and minimum output power of the i^{th} thermal is represented by P_{gi}^{max} and P_{gi}^{min} , and the rated power of j^{th} wind output generator given by $P_{R,j,h}$.

3.2.1.2 Probability distribution function for wind power

Representing short-term wind speeds is crucial for monitoring wind energy potential. PDFs are mainly used to describe wind speed interpretations. The appropriateness of numerous PDFs has been studied in various regions worldwide. The selection of the PDF is crucial in wind energy investigation because wind power is formulated as a clear function of wind speed distribution parameters.

A PDF that better fits the wind speed data reduces uncertainty in approximations of wind power output. The Weibull two-parameter PDF and the Rayleigh PDF are the most frequently used probabilities in wind speed data analysis. Many have modelled wind speed using Weibull distributions to formulate the wind-thermal economic dispatch problem. Weibull PDFs offer significant advantages over other probability distributions. Among its significant advantages, it requires only two parameters to estimate, and its probability density distribution is positively skewed, favouring moderate wind speeds.

The PDF can be represented using the Weibull Probability Density Function (WPDF) (Masters, 2004) and is given in Equation (3.9).

$$f(V) = \frac{k}{c} \left(\frac{V}{c}\right)^{k-1} e^{-(V/c)^k} \quad 0 \leq V < \infty \quad (3.9)$$

Where k is the shape parameter (dimensionless), and c is the scale parameter (in [m/s]) at a particular location. Equation (3.10) presents the Cumulative Distribution function (CDF) based on equation (3.9) above.

$$F(V) = P(v \leq V) = \int_{v=0}^{V=x} \left(\frac{k}{c} \left(\frac{v}{c}\right)^{k-1} e^{-(v/c)^k}\right) dv = 1 - \exp\left(-\left(\frac{V}{c}\right)^k\right) \quad (3.10)$$

The n^{th} instant for any probability density function $f(V)$ is described by Equation (3.11) according to the PDF(Masters, 2004).

$$\bar{V}^n = \int_{V_{min}}^{V_{max}} f(V)dV = C^n \Gamma\left(\frac{n}{k} + 1\right), n = 1, 2 \dots \quad (3.11)$$

where Equation (3.12) represents the Gamma function Γ and is given as

$$\Gamma(\beta) = \int_0^{\infty} x^{\beta-1} \exp(-x) dx \quad (3.12)$$

By using equations (3.9)-(3.12), the probability distribution of wind power can be derived. The link between the wind generation's output power and wind speed is now expressed for each power unit by using a straightforward linear piecewise function, and is provided in equation (3.13)(Leon-Garcia, 2008).

$$\begin{cases} P_w = 0, & v < v_c \text{ or } v > v_f \\ P_w = P_R \frac{v-v_c}{v_r-v_c}, & v_c \leq v \leq v_r \\ P_w = P_R, & v_r \leq v \leq v_f \end{cases} \quad (3.13)$$

where the power delivered and rated power by a wind turbine in [MW] are given by P_w and P_R , and cut-in, rated, and cut-out/ furling wind speed in [m/s] are known by v_c, v_r and v_f respectively. A continuous or a discrete probability function can be utilized to represent the wind power curve(Qu et al., 2016; Xian Liu & Xu, 2010). Equation (3.13) above illustrates that the wind speed in a continuous probability function ranges between the cut-in and the rated wind speed. Equation (3.14) determines the PDF in the continuous range using the Weibull distribution function in equation (3.9).

$$f_{P_w}(p_w) = \frac{kh_w v_c}{P_{RC}} \left[\frac{\left(1 + \frac{h_w}{P_R}\right) v_c}{c} \right]^{k-1} \exp \left\{ - \left[\frac{\left(1 + \frac{h_w}{P_R}\right) v_c}{c} \right]^k \right\}, v_c \leq v \leq v_r \quad (3.14)$$

where the intermediary parameter h_w is known by: $h_w = \frac{v_r - v_c}{v_c}$.

The wind speed is between the rated and furling wind speed for the discrete probability function, and has a constant zero output power, i.e., below the cut-in and cut-out wind speed as shown in equation (3.13) above. The mathematical expression of the two events $P_w = 0$ and $P_w = P_R$ are illustrated in equations (3.15) and (3.16) separately(Ghasemi et al., 2016).

$$\begin{aligned} Pr(P_w = 0) &= Pr(V < v_c) + Pr(V \geq v_f) \\ &= 1 - \exp \left[- \left(\frac{v_c}{c} \right)^k \right] + 1 - Pr(V < v_f) = 1 - \exp \left[- \left(\frac{v_c}{c} \right)^k \right] + 1 - F(V) \\ &= 1 - \exp \left[- \left(\frac{v_c}{c} \right)^k \right] + 1 - [1 - \exp \left[- \left(\frac{v_f}{c} \right)^k \right]] \\ &= 1 - \exp \left[- \left(\frac{v_c}{c} \right)^k \right] + \exp \left[- \left(\frac{v_f}{c} \right)^k \right] \end{aligned} \quad (3.15)$$

$$\begin{aligned}
Pr(P_w = P_R) &= Pr(v_R \leq V \leq v_F) \\
&= Pr(V \leq v_F) - Pr(V \geq v_R) \\
&= 1 - \exp[-(v_F/c)^k] - [1 - \exp[-(v_R/c)^k]] \\
&= \exp[-(v_R/c)^k] - \exp[-(v_F/c)^k]
\end{aligned} \tag{3.16}$$

The Cumulative Distribution Function (CDF) of wind power is represented by both continuous and discrete probabilities accordingly. The succeeding equation (3.17) characterises the CDF of the output power stochastic variable P_w (Qu et al., 2016; Xian Liu & Xu, 2010).

$$\begin{cases} 0 & P < 0 \\ 1 & P \geq P_R \\ 1 - \exp\left\{-\left[\left(1 + \frac{hw}{P_R}\right)\frac{v_c}{c}\right]^k\right\} + \exp\left\{-\left[\frac{v_F}{c}\right]^k\right\}; & 0 \leq P < P_R \end{cases} \tag{3.17}$$

The system operator may overestimate or underestimate exact availability of wind power output from wind generating systems since the current wind speed is a random variable at all times. Underestimation and overestimation must be included in consideration in the cost function due to wind power output that is typically nonlinear. Equation (3.18) provides a mathematical representation of these two concepts that were previously discussed in equation (3.3). The overestimation and underestimation of wind power generators is specified by equations (3.18)-(3.19) and (3.20)-(3.21), respectively (A. Ghasemi et al., 2016). The overestimation is given by equation (3.18)

$$C_{r,w,i}(P_{w_i} - P_{W_{i,av}}) = k_{r,i}(P_{w_i} - P_{W_{i,av}}) = k_{r,i} \int_0^{w_i} (P_{w_i} - P_w) f_{P_w}(w) dw \tag{3.18}$$

where the reserve cost coefficient for the i^{th} wind power generator, $k_{r,i}$, P_{w_i} is the forecasted wind power, $P_{W_{i,av}}$ is the available/generated stochastic wind power and $f_{P_w}(w)dw$ is the probability distribution function for a stochastic variable P_w . Now, by utilising the link established in equation (3.17). Equation (3.19) illustrates the further modification of the overestimation equation (3.18).

$$\begin{aligned}
E(Y_{oe,j,t}) &= w_{j,t} \left[1 - \exp\left(-\frac{v_{c,j,t}}{c_{j,t}}\right)^{k_{j,t}} + \exp\left(-\frac{v_{F,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
&\quad + \left(\frac{P_{R,j,t}v_{c,j,t}}{v_{R,j,t}-v_{c,j,t}} + w_{j,t} \right) \left[\exp\left(-\frac{v_{c,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
&\quad + \left(\frac{P_{R,j,t}c_{j,t}}{v_{R,j,t}-v_{c,j,t}} \right) \left[\Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) - \Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) \right]
\end{aligned} \tag{3.19}$$

Underestimation analysis is performed by using the same approach as overestimation evaluation. Equation (3.20) represents the underestimation of wind power.

$$C_{p,w,i}(P_{W_{i,av}} - P_{w_i}) = k_{p,i}(P_{W_{i,av}} - P_{w_i}) = k_{p,i} \int_0^{w_i} (P_w - P_{w_i}) f_{P_w}(w) dw \tag{3.20}$$

Where the reserve cost coefficient for the i^{th} wind power generator, $k_{p,i}$. Equation (3.21) illustrates a further modification of the underestimation equation (3.20).

$$\begin{aligned}
E(Y_{ue,j,t}) = & (P_{R,j,t} - w_{j,t}) \left[\exp\left(-\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{F,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
& + \left(\frac{P_{R,j,t}v_{C,j,t}}{v_{R,j,t}-v_{C,j,t}} + w_{j,t} \right) \left[\exp\left(-\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}} - \exp\left(-\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}} \right] + \\
& + \left(\frac{P_{R,j,t}c_{j,t}}{v_{R,j,t}-v_{C,j,t}} \right) \left[\Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{1,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) - \Gamma\left(1 + \frac{1}{k_{j,t}}, \left(\frac{v_{R,j,t}}{c_{j,t}}\right)^{k_{j,t}}\right) \right]
\end{aligned} \tag{3.21}$$

3.3 Optimisation of a single area dispatch problem with multi-criteria

WTEED is a multi-criteria optimisation problem with two different goals. One is to reduce the wind and thermal economic dispatch problems overall fuel cost. To reduce the power systems total emission while conforming to the equality and inequality conditions specified in equations (3.4)–(3.8). The max-max price penalty factor stated in equations (3.22) is employed to transform the multi-objective optimisation into a single objective function (Hetzer et al., 2008; Liu & Xu, 2010b). Equations (3.2) and (3.4) represent the fuel cost and emission function, respectively, for the wind-thermal dispatch problem.

$$h_i = \frac{\alpha_i + b_i P_{gimax} + c_i P_{gimax}^2}{\alpha_i + \beta_i P_{gimax} + \gamma_i P_{gimax}^2} \tag{3.22}$$

The price penalty factor is used to transform the bio-objective wind-thermal economic dispatch problem, as illustrated in equation (3.22) above. In this particular case, the maximum fuel cost function divided by the maximum emission function equals the penalty factor. Now, depending on how the optimisation approach is applied, this can alternatively be used as max/min, min/min, or min/max. Equation (3.23) describes how the function of Lagrange, based on a Lagrange multiplier λ , is implemented to solve the optimisation problem.

$$L = F_T + \lambda(P_D + P_{Loss} - \sum_{i=1}^{N_G} P_{gi} - \sum_{k=1}^{N_W} P_w) \tag{3.23}$$

where

$$F_T = a_i P_{gi}^2 + b_i P_{gi} + c_i + h_i(d_i P_{gi}^2 + e_i P_{gi} + f_i) \tag{3.24}$$

3.4 The algorithm applied in solving the single-area WTEED problem

The LaGrange algorithm is one of the best methods for solving optimization problems involving coupled structures. A large-scale linked problem can be converted into a two-stage dual problem with a master problem and subproblems, using Lagrange multipliers to relax global constraints. A suboptimal, viable solution close to the dual optimal point is expected to be recognized as a valid solution to the primal problem

based on the sharp bound provided by the Lagrange dual optimum. In a parallel framework, the subproblems can be resolved quickly and easily because they are significantly smaller than the main problem. The dual fitness function is optimized in the master problem stage by updating the Lagrange multipliers. The performance of LR processes is strongly influenced by the methodologies used to initialize and update the Lagrange multipliers.

The LR method is applied to determine the optimal value of the WTEED problem. Dynamic programming's dimensionality challenge can be addressed by temporarily relaxing coupling constraints while focusing on each unit separately (Bhattacharya & Chattopadhyay, 2010). Therefore, reducing fuel expenses and pollution are two issues that the LR strategy can help with. The LaGrange technique solution approach is as follows.

Equation (3.25) is the result of adding the emission and demand limitations to the initial cost function and applying Lagrange multipliers.

$$L = F_T + \lambda(P_D + P_{Loss} - \sum_{i=1}^{N_G} P_{gi} - \sum_{k=1}^{N_W} P_w) \quad (3.25)$$

where

$$F_T = a_i P_{gi}^2 + b_i P_{gi} + c_i + h_i(d_i P_{gi}^2 + e_i P_{gi} + f_i) \quad (3.26)$$

Equation (3.27) is obtained by integrating the loss equation (3.6) into equation (3.25).

$$L = a_i P_{gi}^2 + b_i P_{gi} + c_i + h_i(d_i P_{gi}^2 + e_i P_{gi} + f_i) + \lambda \left(P_D + \sum_{m=1}^{N_G+N_W} \sum_{m'=1}^{N_G+N_W} P_m B_{mm'} P_{m'} + \sum_{m=1}^{N_G+N_W} B_{om} P_m + B_{00} - \sum_{i=1}^{N_G} P_{gi} - \sum_{k=1}^{N_W} P_w \right) \quad (3.27)$$

The condition necessary for optimality for the solution of the problem (3.27) is:

$$\text{According to } P_{gi}, \frac{\partial L}{\partial P_{gi}} = 0, i = \overline{1, N_g} \quad (3.28)$$

$$\text{According to } P_w, \frac{\partial L}{\partial P_w} = 0, k = \overline{1, N_w} \quad (3.29)$$

$$\text{According to } \lambda, \frac{\partial L}{\partial \lambda} = 0 \quad (3.30)$$

The conditions necessary for optimality for conventional generators, given in equation (3.26), are computed as follows:

$$\frac{\partial L}{\partial P_{gi}} = 2a_i P_{gi} + b_i + h_i(2d_i P_{gi} + e_i) + \lambda \left(2 \sum_{j=1}^{N_g} B_{ij} P_j + B_{oi} - 1 \right) = 0 = i = \overline{1, n} \quad (3.31)$$

This can be reduced to the following:

$$\frac{\partial L}{\partial P_{gi}} = (2a_i + h_i 2d_i)P_{gi} + 2\lambda B_{ii}P_{gi} + h_i e_i + b_i + \dots$$

$$\lambda \left(2 \sum_{\substack{j=1 \\ j \neq i}}^{N_g} B_{ij}P_j + B_{oi} - 1 \right) = 0, i = \overline{1, n} \quad (3.32)$$

By reducing equation (3.32), we have the following equation (3.33)

$$\frac{\partial L}{\partial P_{gi}} = \left(\frac{a_i + h_i d_i}{\lambda} + B_{ii} \right) P_{gi} + \sum_{\substack{j=1 \\ j \neq i}}^n B_{ij}P_j + \frac{1}{2} \left(\frac{h_i e_i + b_i}{\lambda} + B_{oi} - 1 \right) = 0, i = \overline{1, n} \quad (3.33)$$

The matrix representation of equation (3.33) is as follows:

$$\begin{bmatrix} \frac{a_1 + h_1 d_1}{\lambda} + B_{11} & B_{12} & B_{1n} \\ B_{21} & \frac{a_2 + h_2 d_2}{\lambda} + B_{22} & B_{2n} \\ B_{n1} & B_{n2} & \frac{a_{1n} + h_n d_n}{\lambda} + B_{nn} \end{bmatrix} \begin{bmatrix} P_1 \\ P_2 \\ P_3 \\ \vdots \\ P_n \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \left[1 - \left(\frac{b_1 + h_1 e_1}{\lambda} \right) - B_{o1} \right] \\ \left[1 - \left(\frac{b_1 + h_1 e_1}{\lambda} \right) - B_{o2} \right] \\ \left[1 - \left(\frac{b_1 + h_1 e_1}{\lambda} \right) - B_{on} \right] \end{bmatrix} \quad (3.34)$$

The following straightforward matrix form can be used to represent equation (3.34).

$$BP = D \quad (3.35)$$

Equation (3.35) in MATLAB can be used to find the matrix-vector P given the known value of the Lagrange multiplier.

$$P = B/D \quad (3.36)$$

Equation (3.27) provides the necessary conditions for wind generator optimality and can be derived as follows: Equation (3.37) represents the total wind power.

$$\frac{\partial L}{\partial P_w} = \lambda \left(2 \sum_{\substack{j=1 \\ j \neq i}}^{N_w} B_{ij}P_j + B_{oi} - \frac{\partial}{\partial P_w} (OE + UE + d_i P_w) \right) = 0, i = \overline{1, n} \quad (3.37)$$

Additionally, equation (3.37) can be represented as follows in matrix form:

$$\begin{bmatrix} B_{11} & B_{12} & B_{13} \\ \vdots & \vdots & \vdots \\ B_{n1} & B_{n2} & B_{nn} \end{bmatrix} \begin{bmatrix} P_1 \\ \vdots \\ P_{nw} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} \frac{\partial}{\partial P_w} (C_p \cdot UE + C_r \cdot O \cdot E + d_i P_w) - B_{o1} \\ \vdots \\ \frac{\partial}{\partial P_w} (C_p \cdot UE + C_r \cdot O \cdot E + d_i P_w) - B_{onw} \end{bmatrix} \quad (3.38)$$

The conditions necessary for optimality for LaGrange multiplier λ in equation (3.27), the coefficients are found as follows:

$$\frac{\partial L}{\partial \lambda} = (P_D + P_{Loss} - \sum_{i=1}^{N_G} P_{gi} - \sum_{k=1}^{N_W} P_w) = 0 = \Delta \lambda \quad (3.39)$$

The gradient of the functional cap L according to lambda is not represented by the Lagrange multiplier's necessary requirements for optimality. The gradients' optimality conditions must be met. Because equation (3.39) cannot be solved analytically, the gradient method must be implemented as follows.

$$\lambda^{(k+1)} = \lambda^k + \alpha \Delta \lambda^k, \lambda \neq 0 \quad (3.40)$$

where the steps of the gradient procedure, α and $\Delta\lambda^k$ is computed using equation (3.40). The gradient approach always begins with an initial guess of a Lagrange multiplier. Upon the value of $\frac{\partial L}{\partial \lambda} = 0$, The solution value for the Lagrange variable is obtained. It determines the energy that the generators must produce as a solution to equations (3.34) and (3.38). Every gradient method step's resultant solution must fit the constraint's domain in the manner that is stated below:

$$P_i^k = \begin{pmatrix} P_{i,min}^k & \text{if } P_i^k < & P_{i,min} \\ P_i^k & \text{if } P_{i,min}^k \leq & P_i^k < P_{i,max} \\ P_{i,min}^k & \text{if } P_i^k > & P_{i,max} \end{pmatrix} \quad (3.41)$$

Equation (3.42) below provides the condition for terminating the gradients and iterations.

$$\Delta\lambda^k \leq \varepsilon, \text{ and } k = \text{iter Max} \quad (3.42)$$

where, $\varepsilon > 0$ is a smaller number and the maximum number of iterations, *iter Max*. The algorithm of the approach is given as follows:

- The Lagrange multiplier's initial value λ^0 and the optimality conditions value ε are given.
- Matrix B^0 and D^0 are formed in equation (3.34)
- Equation (3.36) is resolved and $P^0 = B^0/D^0$ is determined
- Wind power is calculated using equations (3.18–3.21). In MATLAB, the trapezoidal method is used to calculate wind power.
- The total power produced by combined wind and thermal generators is calculated by adding the optimum power calculation from equations (3.36) and (3.18-3.21).
- The attained vector of P^0 is fitted to the limits equation (3.41).
- $\Delta\lambda^0$ is computed with Equation (3.39), where P^0 is added.
- The condition (3.41) is examined. If it is satisfied, the process stops. But if it is not, the better value of $\lambda \rightarrow \lambda^1$ is computed with Equation (3.40).
- Computation of the better $P_i \rightarrow P_i^1$ is done following step 5, and the procedure repeats itself until the conditions of Equation (3.42) are satisfied.

The optimal solution is utilised to compute the total cost of generation and emission pollutants employing equations (3.2) and (3.4). Figure 3.2 below shows the algorithm's flow chart.

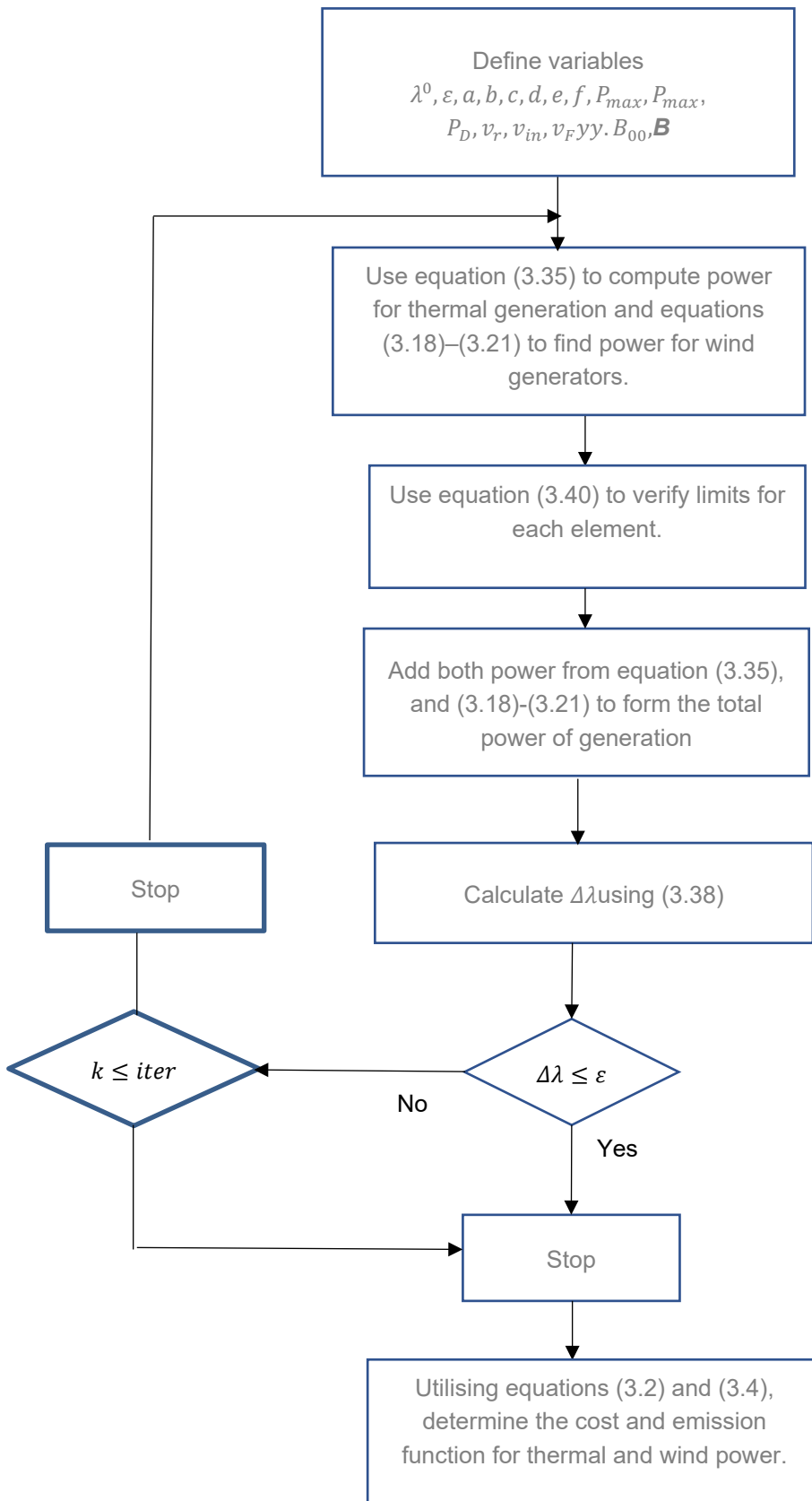


Figure 3.2: Flow diagram of the bi-criteria dispatch problem algorithm solution.

3.5 Description of the Test Systems

The power system comprises six conventional generators and a wind turbine cluster. A line diagram of a basic interconnected power system is illustrated in Figure 3.3. Then, it can be estimated that the six thermal units produce 270 MW and the wind turbines generate 125 MW. On the other hand, interconnected transmission lines enable power to be delivered from one location to another. The simplified power system model in Figure 3.3 highlights the research's focus on the wind-thermal economic dispatch problem. During the day, the power consumption fluctuates between 125 and 300 MW. Tables 3.1-3.3 provide all the necessary information for the WTEED problem. Table 3.4 presents the solution to the wind-thermal economic dispatch problem.

Table 3.1: IEEE 30 Bus System data for 6 thermal systems.

Generator Number	Generator Limits [MW]		Fuel cost coefficients			Emission coefficients		
	P_{\min}	P_{\max}	a_i [\$/MW ² h]	b_i [\$/MWh]	c_i [\$/h]	d_i [\$/kg ² h]	e_i [\$/kgh]	f_i [\$/h]
1	50	200	0.00375	2.00	0.00	0.0126	-0.90	22.983
2	20	80	0.01750	1.70	0.00	0.0200	-0.10	25.313
3	15	50	0.06250	1.00	0.00	0.0270	-0.01	25.505
4	10	35	0.00834	3.25	0.00	0.0291	-0.005	24.900
5	10	30	0.02500	3.00	0.00	0.0290	-0.004	24.700
6	12	40	0.02500	3.00	0.00	0.0271	-0.0055	25.300

Table 3.2: Transmission line coefficients

B_{0i}			B					
0.000003	0.000021	-0.00056	0.000218	0.000103	0.000009	0.000010	0.000002	0.000027
0.000034	0.000015	0.000078	0.000103	0.000181	0.000004	0.000015	0.000002	0.000030
$B_{00} = 0.000014$			0.000009	0.000004	0.000417	-0.000131	-0.000153	0.000107
			0.000010	0.000015	0.000131	0.000221	0.000094	0.000050
			0.000002	0.000002	-0.000153	-0.000094	-0.000243	-0.000001
			0.000027	0.000030	0.000107	0.000050	-0.000001	0.0003458

Table 3.3: Wind-speed data

v_{in} Cut-in wind-speed	v_r Rated wind-speed	v_o Cut-out wind speed	w_r Rated Power	C_{pw} Underestimation	C_{rw} Overestimation	d_w direct cost
5	15	45.	0.8	100	310	0

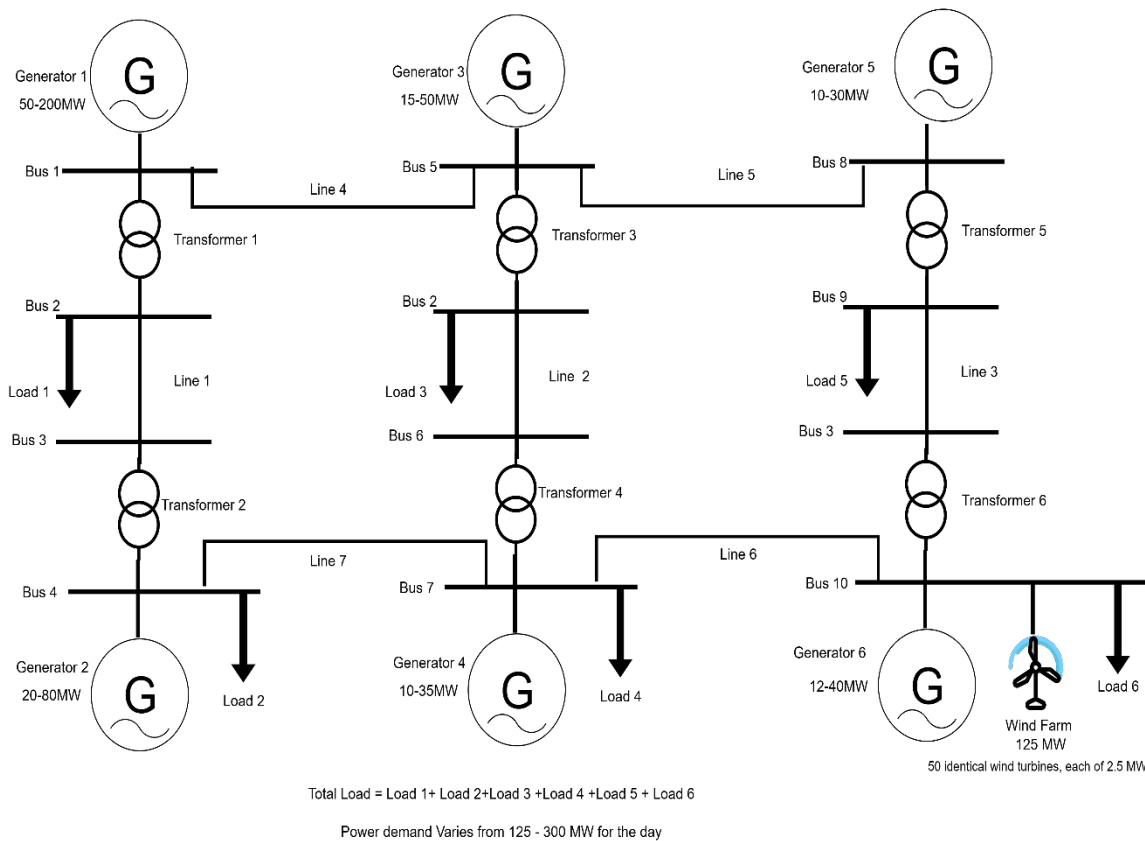


Figure 3.3: Wind-thermal economic dispatch power system model with six generators.

3.5.1 Test System 1: IEEE30 bus system with 6 units

A cluster consists of turbines situated in a geographic area, represented by a group of identical turbines in a large wind farm. The fuel cost coefficients are based on the ones reported in (Damodaran & Kumar, 2014; Krishnamurthy & Tzoneva, 2012), and, for wind power, (Liu, 2010; Mishra & Shaik, 2024a; Xian Liu & Xu, 2010). The WTEED problem is solved for a load demand of 283.4 MW, using a wind farm comprising 50 identical 2.5-MW wind turbines, for a total installed wind farm capacity of 125 MW. (Kumari & Pal, 2022). Different power demand values are simulated to test the system's behavior under varying demand. The solution to the single-area WTEED problem is shown in Table 3.4. The software is provided in Appendix A1, and the MATLAB script is named WTEED_case6units.m.

Table 3.4: The WTEED using LMM with different power demand for a 6-unit system

PD [MW]	125	150	175	200	225	250	283.4
P1 [MW]	5	5	6.65	9.54	12.44	15.35	19.24
P2 [MW]	28.29	30.37	32.32	34.17	36.03	37.89	40.37
P3 [MW]	14.5	20.87	26.85	32.54	38.24	43.96	51.63
P4 [MW]	50.68	57.51	63.91	69.98	76.06	82.15	90.31
P5 [MW]	13.72	19.98	25.85	31.42	37.01	42.61	50.11
P6 [MW]	13.15	16.9	20.4	23.71	27.02	30.32	34.72
P7 [MW]	118.28	118.28	118.28	118.28	118.28	118.28	118.28
PL [MW]	1.32	1.63	1.97	2.36	2.79	3.26	3.96
F _c [USD/h]	25,391	29,234	33,164	37,160	41,167	45,183	50,562.51
E _r [kg/h]	22.26	21.62	21.05	20.55	20.17	19.89	19.69
CEED [kg/h]	28,361	33,066	37,966	43,039	48,265	53,644	61,070

Table 3.4 shows the real power of the thermal (P1–P7) units, wind (P7) generators, transmission losses (P_L) in [MW], fuel cost (F_C) for thermal generators) in MW, total emissions (E_T) in kg/h, and CEED in kg/h.

3.5.1.1 WTEED problem discussion and results for the six-unit system

This system uses 50 available wind turbines to provide 118.28 MW to solve the power dispatch problem. The Lagrange multiplier algorithm employs the following parameters. The tolerance value epsilon is 0.01, the tolerance value of delta-lambda epsilon is 0.1, the initial guess value of lambda is 200, and the total number of iterations m is 100.

The proposed method for a six-unit system is applied and compared with different optimisation algorithms found in the literature, including the Genetic Algorithm (GA) (Zhang et al., 2019), the Particle Swarm Optimization (PSO), the Gravitational Search Algorithm (GSA), and the hybrid optimization algorithm Gravitational acceleration Enhanced Particle Swarm Optimization Algorithm (GAEPSO) (Jiang et al., 2015). Table 3.5 presents the comparison of simulation results.

Table 3.5: LMM-based WTEED in comparison to other optimisation techniques.
PD = 283.4 [MW]

Algorithm	PSO [MW]	GSA [MW]	GAEPSO [MW]	GA [MW]	GPSOA Without Wind	Proposed LMM [MW]
P1 [MW]	2	14.45	20.75	36.62	11.29	19.24
P2 [MW]	30.06	53.46	30.09	42.58	29.95	40.37
P3 [MW]	28.24	23.87	34.63	30.31	52.66	51.63
P4 [MW]	31.29	6	35.06	31.36	101.69	90.31
P5 [MW]	40.32	25.48	34.53	53.44	52.68	50.11
P6 [MW]	41.61	22.67	32.93	43.52	35.95	34.72
Pw [MW]	110.2	137.71	95.47	45.57	--	118.28
P_L [MW]	---	---	---	---	---	3.96
F_C [USD/h]	62,497	58,846	57,219	66,582	60,029	50,562.51
% Deviation F_C [\$/h] Compared to Developed LMM	5.27	3.78	3.08	6.83	4.10	4.27
E_T [kg/h]	20.43	21.33	20.49	19.72	22.21	19.69
% Deviation E_T [kg/h] Compared to Developed LMM	0.922	1.99	0.99	0.038	3.007	3.007

Compared with the LMM algorithm, the fuel cost values for the PSO, GSA, GAEPSO, GA, and GPSOA algorithms are 5.27, 3.78, 3.08, 6.83, and 4.27, respectively. Compared to other optimisation algorithms, the LLM method reduces fuel usage by 3–6% when wind power is incorporated in the economic emission dispatch. Additionally, the resultant NOx emissions are 0.922, 1.99, 0.99, 0.038, and 3.01, respectively, compared to the proposed algorithm. The effectiveness of the Lagrange algorithm in reducing emissions when wind power is added to conventional generation decreased by 1–3%. The optimization algorithm required only 84 iterations to find the optimal

solution to the WTEED problem. The calculated value of lambda is 214.9919, compared to the initial guess of 200. Figures 3.4 and 3.5 below represent the fuel cost and emissions.

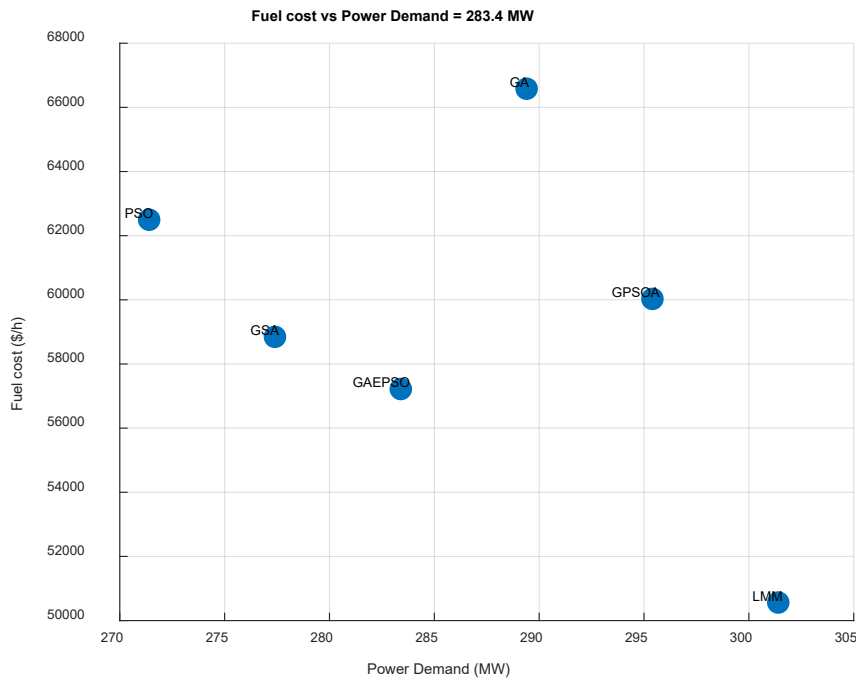


Figure 3.4: Fuel cost and emissions for various algorithms applied to a 6-unit system

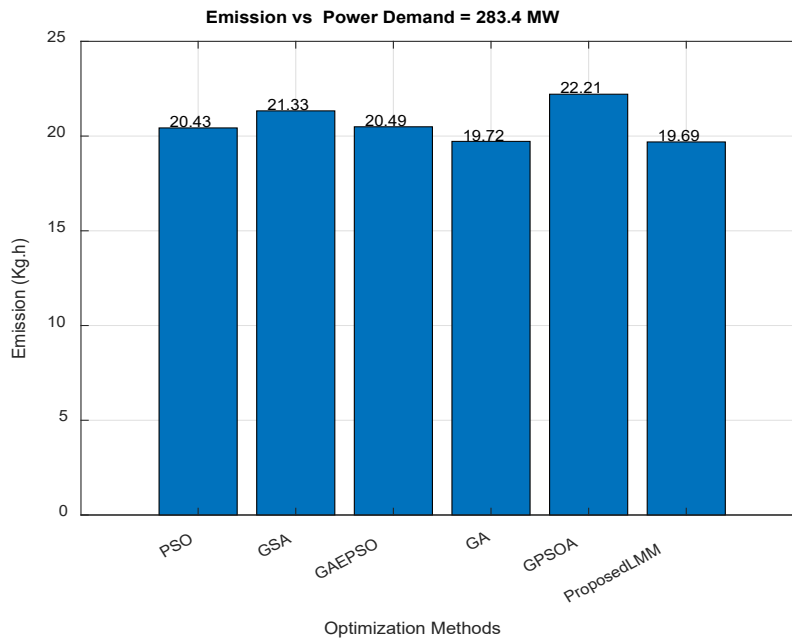


Figure 3.5: Comparison of the Fuel cost and emission analysis for different optimization algorithms applied to a 6-unit system.

3.5.2 Test System 2: IEEE30 bus system with 10-units.

This study of the WTEED power system problem includes 10 thermal generators and 1 wind turbine cluster. The cluster consists of turbines situated in a specific geographic area, represented by a group of identical turbines in a large wind farm. The fuel cost, emission, and loss coefficients are based on those reported in (Basu, 2011a). The wind parameters are adopted from (Liu, 2010; Mishra & Shaik, 2024a; Xian Liu & Xu, 2010), as in Test System I above. The study focuses on 2000 MW power demand. (Secui et al., 2024a). Various power demand values are used to test the system's response to changes in power demand. The solution of the WTEED problem is shown in Table 3.6. The software is provided in Appendix A2, and the MATLAB script file is named WTEED_case10units. m.

Table 3.6: Various power demands applied to a 10-unit generator for LMM WTEED problem

PD [MW]	650	800	1000	1200	1500	2000
P1 [MW]	16.9077	43.2946	55.0000	55.0000	55.0000	55.0000
P2 [MW]	20.4349	45.0263	59.3561	69.8398	80.0000	80.0000
P3 [MW]	47.0000	47.0000	60.9549	71.9979	87.5874	111.9414
P4 [MW]	20.0000	44.1126	59.4937	70.7465	86.6321	111.4487
P5 [MW]	50.0000	50.0000	50.0000	50.0000	67.6960	111.5112
P6 [MW]	70.0000	70.0000	70.0000	70.0000	78.8096	134.2497
P7 [MW]	60.0000	62.8499	106.5857	138.5827	183.7531	254.3184
P8 [MW]	70.0000	70.0000	114.6430	152.1590	205.1205	287.8573
P9 [MW]	135.0000	135.0000	175.7180	229.6450	305.7741	424.7033
P10 [MW]	150.0000	150.0000	173.2323	228.4474	306.3949	428.1648
P11 [MW]	24.028	100.116	100.116	100.116	100.116	100.116
PL [MW]	13.3715	17.4007	25.1010	36.5356	56.8851	99.3099
F _c \$/h	37,639.687359	41,146.509	50,742.1419	60,746.3	76,945.943152	107,422.761421
E _T [kg/h]	1399.058217	1333.454716	1501.85983	1803.17	2440.652768	3910.593584
CEED [kg/h]	63,739.681832	66,384.319239	80,126.5769	97,793.9	131,033.780343	203,261.325452

Table 3.6 shows the real power of the thermal (P1–P11) units, wind (P11) generators, and transmission losses (P_L) in MW, fuel cost F_C for thermal generators, total emissions (E_T) in kg/h, and CEED in kg/h.

3.5.2.1 WTEED problem results and discussion for Ten-Unit System

The Lagrange method is implemented to solve the economic emission dispatch problem with wind power, using 10 conventional units and 50 available wind turbines on a wind farm consisting of 50 identical wind turbines. The following parameters are used for the Lagrange multiplier method. The initial value of lambda is 200, the total number of iterations m is 3000, the tolerance value (epsilon) is 0.01, and the tolerance value of delta-lambda epsilon is 0.1. The Lagrange multiplier method is compared with

the Salp Swarm Algorithm (SSA), Grey Wolf Optimization (GWO), Moth–Flame Optimization (MFO), Whale Optimization Algorithm (WOA), Search and Rescue Algorithm (SAR), and Genetic Algorithm (GA) (Mishra & Shaik, 2024a). The optimization algorithm took 1013 iterations to find the optimal solution of the WTEED problem. The optimized lambda value is 151.2992, compared to the initial guess of 200. The proposed algorithm has a lower fuel cost and is observed to be superior to all other optimization algorithms, as shown in Table 3.7.

Table 3.7: LMM-based WTEED in comparison to other optimisation techniques.
PD = 2000[MW]

Algorithm	MFO	WOA	SAR	GA	Proposed LMM
P1 [MW]	37.16	46.96	53.49	34.17	55.0000
P2 [MW]	25.84	68.61	77.10	63.49	80.0000
P3 [MW]	120	69.24	64.41	95.75	111.9414
P4 [MW]	93.90	129.21	83.05	121.67	111.4487
P5 [MW]	160	50	158.73	145.83	111.5112
P6 [MW]	240	226	239.50	229.86	134.2497
P7 [MW]	244.61	298.21	275.88	281.21	254.3184
P8 [MW]	286.25	337.93	332.28	307.35	287.8573
P9 [MW]	470	390.40	409.12	391.63	424.7033
P10 [MW]	404.92	468	388.56	410.56	428.1648
P11 [MW]	30	30	30	30	100.116
F _c [USD]	116,690.8	114,678.8	114,106.19	115,802.24	107,422.761421
% Deviation F _c [\$ /h] Compared to Developed LMM	2.07	1.63	1.508477	1.876913	1.876
F _{CT} [\$ /h]	239,158.6	244,987.2	226,506.78	231,903.60	110,572.517314
PL [MW]	83.70	84.44	82.81	83.9	99.310
E _T [kg/h]	4080	4220	4103.3	4390	3910.593584
% Deviation E _T [kg/h] Compared to Developed LMM	1.060036	1.90273	1.202327	2.897008	2.887784
CEED[[kg/h]]	239,158.6	244,987.2	226,506.78	231,903.60	203,261.325452

Compared with the LMM algorithm, the fuel cost obtained with the MFO, WOA, SAR, and GA algorithms are 2.07%, 1.63%, 1.5%, and 1.89%, respectively. The proposed method outperforms other algorithms by 1-2% in solving the wind-thermal economic emission dispatch problem. Compared with the developed LM algorithm, the resulting NOx emissions are 1.06%, 1.9%, 1.2%, and 2.89%, respectively. Compared with other optimisation techniques, the LM approach has successfully reduced pollution levels by 1-2.89%.

Figures 3.6 and 3.7 below provide a graphic representation of fuel cost and emissions.

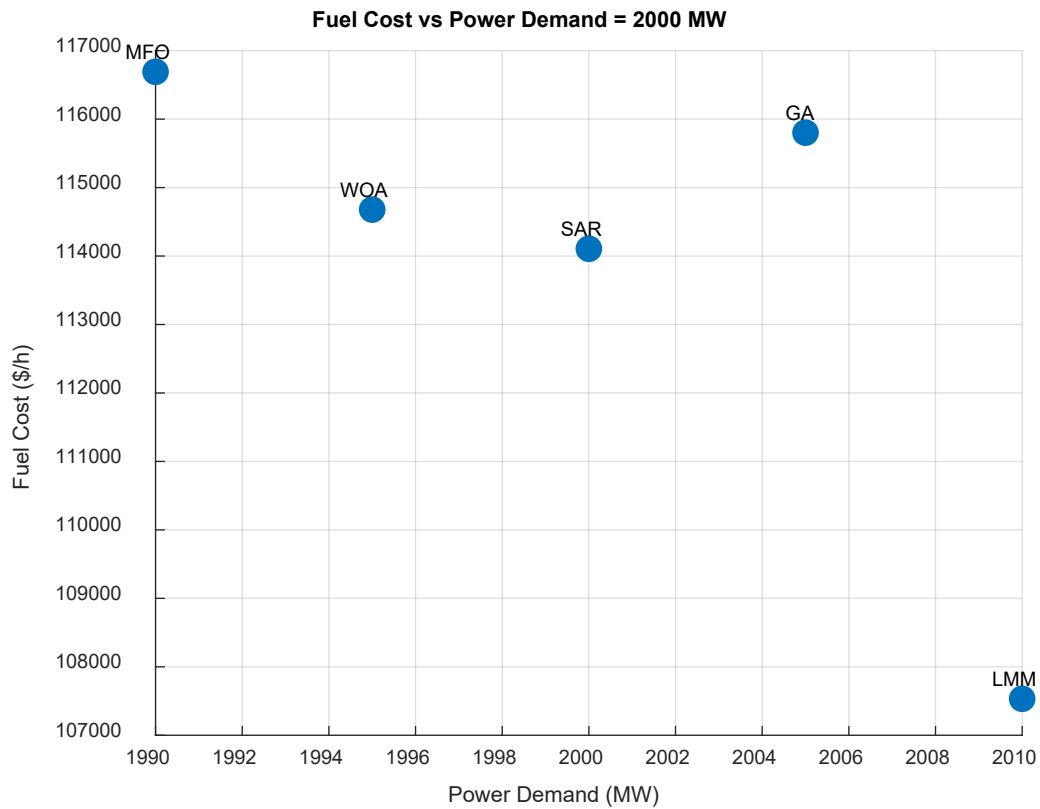


Figure 3.6: Values of fuel cost and power demand for various algorithms employing a 10-unit system in comparison to the developed algorithm

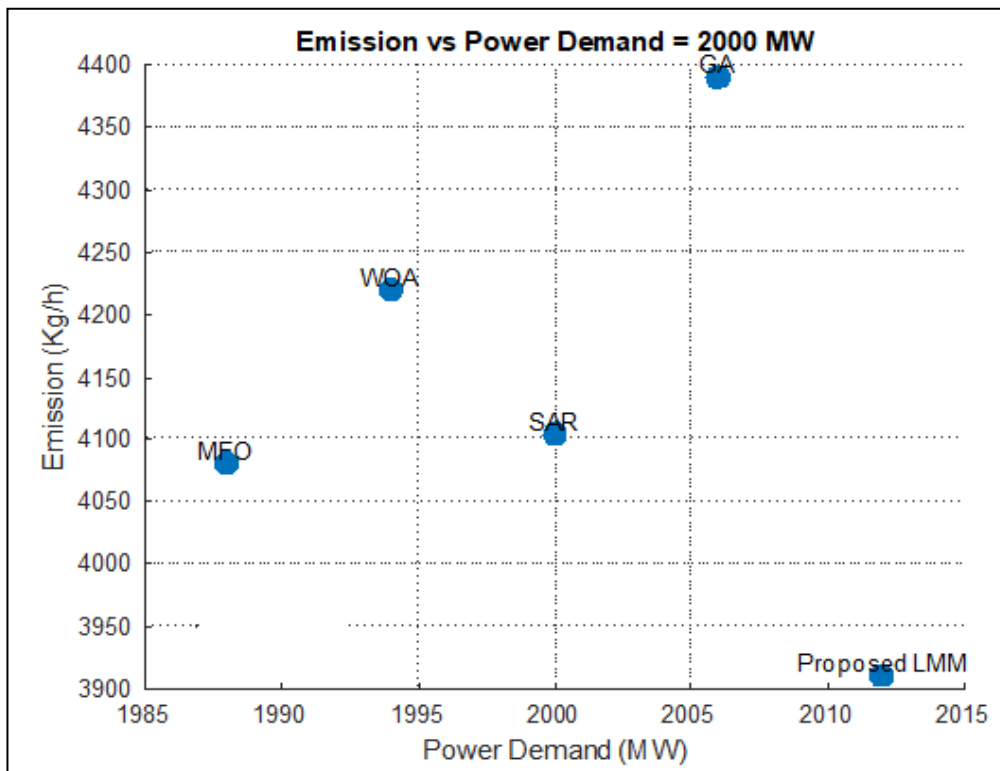


Figure 3.7: Values of emission and power demand for various algorithms employing a 10-unit system in comparison to the developed algorithm

The fuel cost and emission values are further compared to the statistical values of different algorithms, as presented in Table 3.8.

Table 3.8: Developed LMM compared with various algorithms for the ten-unit system
(Secui et al., 2024a)

Algorithm	Fuel cost (\$/h)	Fuel cost (%) Deviation	Emission (kg/h)	Emission (%) Deviation
DE	111,500.000	0.931205	3923.40	0.081736
QPSO	119,005.3030	2.557665	4032.38	0.76663
GQPSO	112,424.7444	1.137603	4011.9244	0.639511
SGO	111,497.6302	0.930674	3932.243252	0.138022
MSGO	111,497.6301	0.930674	3932.243252	0.138022
LMM	107,422.761421	1.297564	3910.593584	0.352784

In Table 3.8, fuel cost and emissions for different algorithms used to solve the thermal economic problem are compared with those of the proposed LMM. It is found that the LMM is 1.29% and 0.353% better at minimizing fuel and emissions.

3.5.3 Test System 3: IEEE30 bus system with 40-units

The test system consists of a 40-unit thermal power generator with a power demand of 10,500 MW, accounting for power losses without valve-point loading. The simulation data for power limits, fuel cost coefficients, emission coefficients, and B-loss coefficients used in this test system are identical to those used in (Secui et al., 2024a), also presented in Tables 3.9 and 3.10(a-b) respectively.

Table 3.9: IEEE 30 Bus System data for 40 thermal systems

Generating Unit [MW]	Generator Limits		Fuel cost coefficients			Emission coefficients		
	P _{min}	P _{max}	a _i [\$/ (MWh) ²]	b _i [\$/MWh]	c _i [\$/h]	α _i [t/(MWh) ²]	β _i [t/MWh]	γ _i [t/h]
1	36	114	0.0069	6.73	94.705	0.048	-2.22	60
2	36	114	0.0069	6.73	94.705	0.048	-2.22	60
3	60	120	0.02028	7.07	309.54	0.0762	-2.36	100
4	80	190	0.00942	8.18	369.03	0.054	-3.14	120
5	47	97	0.0114	5.35	148.89	0.085	-1.89	50
6	68	140	0.01142	8.05	222.33	0.0854	-3.08	80
7	110	300	0.00357	8.03	287.71	0.0242	-3.06	100
8	135	300	0.00492	6.99	391.98	0.031	-2.32	130
9	135	300	0.00573	6.6	455.76	0.0335	-2.11	150
10	130	300	0.00605	12.9	722.82	0.425	-4.34	280
11	94	375	0.00515	12.9	635.2	0.0322	-4.34	220
12	94	375	0.00569	12.8	654.69	0.0338	-4.28	225
13	125	500	0.00421	12.5	913.4	0.0296	-4.18	300
14	125	500	0.00752	8.84	1760.4	0.0512	-3.34	520
15	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
16	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
17	220	500	0.00313	7.97	647.85	0.0151	-2.68	220
18	220	500	0.00313	7.95	649.69	0.0151	-2.66	222
19	242	550	0.00313	7.97	647.83	0.0151	-2.68	220
20	242	550	0.00313	7.97	647.81	0.0151	-2.68	220
21	254	550	0.00298	6.63	785.96	0.0145	-2.22	290
22	254	550	0.00298	6.63	785.96	0.0145	-2.22	285
23	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
24	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
25	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
26	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
27	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
28	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
29	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
30	47	97	0.0114	5.35	148.89	0.085	-1.89	50
31	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
32	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
33	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
34	90	200	0.0001	8.95	107.87	0.0012	-3.48	65
35	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
36	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
37	25	110	0.0161	5.88	307.45	0.095	-1.98	100
38	25	110	0.0161	5.88	307.45	0.095	-1.98	100
39	25	110	0.0161	5.88	307.45	0.095	-1.98	100
40	242	550	0.00313	7.97	647.83	0.0151	-2.68	220

Table 3.10(a): The B-coefficients $B_{ij} \times 10^4$ (-6), $B_{0i} \times 10^4$ (-4), and B_{00} for 40-unit system

Unit	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
1	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
2	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
3	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
4	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
5	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
6	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1
7	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
8	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
9	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
10	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
11	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
12	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1
13	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
14	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
15	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
16	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
17	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
18	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1
19	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
20	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
21	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
22	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
23	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
24	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1
25	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
26	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
27	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
28	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
29	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
30	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1
31	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
32	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
33	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
34	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
35	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6
36	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1

37	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12
38	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14
39	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9
40	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1
B _{oi}	-3.	-1.	7.	0.	2.	-6.	-3.	-1.	7.	0.	2.	-6.	-3.	-1.	7.	0.	2.	-6.	-3.	-1.
	908	297	047	591	161	635	908	297	047	591	161	635	908	297	047	591	161	635	908	297

Table 3.10(b): The B-coefficients B_{ij}×10⁻⁶, B_{0i}×10⁻⁴, and B₀₀ for 40-unit system

Unit	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
1	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
2	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
3	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
4	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
5	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
6	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8
7	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
8	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
10	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
11	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
12	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8
13	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
15	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
16	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
17	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
18	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8
19	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
20	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
21	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
22	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
23	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
24	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8
25	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
26	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
27	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
28	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
29	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
30	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8

31	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
32	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
33	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
34	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
35	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5	-6	-10	-6
36	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2	-1	-6	-8
37	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1	-5	-2	17	12	7	-1
38	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1	-6	-1	12	14	9	1
39	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0	-10	-6	7	9	31	0
40	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24	-6	-8	-1	1	0	24
B_{oi}	7. 047	0. 591	2. 161	-6. 635	-3. 908	-1. 297	7. 047	0. 591	2. 161	-6. 635	-3. 908	-1. 297	7. 047	0. 591	2. 161	-6. 635	-3. 908	-1. 297	7.047	0.591

The cluster consists of turbines located within a geographic area, represented by a group of identical turbines in a large wind farm, as shown in Test System One. Various power demand values are given to test the system's behavior in response to changes in power demand. The solution of the WTEED problem is shown in Table 3.11 below.

Table 3.11: Various power demands applied to a 40-unit generator for the LMM WTEED problem

PD [MW]	10,500	11,000	11,200	11,300
P1 [MW]	114.0000	114.0000	114.0000	114.0000
P2 [MW]	114.0000	114.0000	114.0000	114.0000
P3 [MW]	120.0000	120.0000	120.0000	120.0000
P4 [MW]	190.0000	190.0000	190.0000	190.0000
P5 [MW]	97.0000	97.0000	97.0000	97.0000
P6 [MW]	140.0000	140.0000	140.0000	140.0000
P7 [MW]	300.0000	300.0000	300.0000	300.0000
P8 [MW]	300.0000	300.0000	300.0000	300.0000
P9 [MW]	300.0000	300.0000	300.0000	300.0000
P10 [MW]	236.1173	300.0000	300.0000	300.0000
P11 [MW]	279.1346	369.8932	375.0000	375.0000
P12 [MW]	277.8458	369.5691	375.0000	375.0000
P13 [MW]	383.4729	500.0000	500.0000	500.0000
P14 [MW]	422.9295	500.0000	500.0000	500.0000
P15 [MW]	421.4242	500.0000	500.0000	500.0000
P16 [MW]	421.4242	500.0000	500.0000	500.0000
P17 [MW]	500.0000	500.0000	500.0000	500.0000
P18 [MW]	500.0000	500.0000	500.0000	500.0000
P19 [MW]	550.0000	550.0000	550.0000	550.0000
P20 [MW]	550.0000	550.0000	550.0000	550.0000
P21 [MW]	550.0000	550.0000	550.0000	550.0000
P22 [MW]	550.0000	550.0000	550.0000	550.0000
P23 [MW]	550.0000	550.0000	550.0000	550.0000
P24 [MW]	550.0000	550.0000	550.0000	550.0000
P25 [MW]	550.0000	550.0000	550.0000	550.0000
P26 [MW]	550.0000	550.0000	550.0000	550.0000
P27 [MW]	17.9820	23.6373	101.6061	142.1987
P28 [MW]	17.9820	23.6373	101.6061	142.1987
P29 [MW]	17.9820	23.6373	101.6061	142.1987
P30 [MW]	97.0000	97.0000	97.0000	97.0000
P31 [MW]	190.0000	190.0000	190.0000	190.0000
P32 [MW]	190.0000	190.0000	190.0000	190.0000
P33 [MW]	190.0000	190.0000	190.0000	190.0000
P34 [MW]	90.0000	90.0000	90.0000	90.0000
P35 [MW]	90.0000	90.0000	90.0000	90.0000
P36 [MW]	90.0000	90.0000	90.0000	90.0000
P37 [MW]	110.0000	110.0000	110.0000	110.0000
P38 [MW]	110.0000	110.0000	110.0000	110.0000
P39 [MW]	110.0000	110.0000	110.0000	110.0000
P40 [MW]	550.0000	550.0000	550.0000	550.0000
P41 [MW]	150.386	150.386	150.386	150.386
F _C [USD/h]	133,540.341	143,551.62517	159,778.38	175,659.5
P _L [MW]	1038.682	1152.8	1197.2	1218.984
E _T [kg/h]	105,263.403	136,510.06316	190,426.05	244,979.8
CEED [kg/h]	254,190.3053	283,453.10221	317,220.20	350,503.7

In Table 3.11 above, the real power of the thermal (P1–P40) units, wind (P41) generators, and transmission losses (P_L) in MW, fuel cost (F_C) for thermal generators, total emissions (E_T) in kg/h, and CEED in kg/h.

3.5.3.1 WTEED problem results and discussions for Forty-Unit System

This is a fourth-generation unit system used to evaluate the effectiveness of the Lagrange multiplier method relative to other optimization methods for minimizing fuel costs and atmospheric emissions. The following parameters are used for the Lagrange multiplier method. The initial value of lambda is 8.9914, the total number of iterations m is 35,000, the tolerance value (epsilon) is 0.01, and the tolerance value of delta-lambda epsilon is 0.1. The Lagrange multiplier method is compared with different heuristic algorithms, i.e., PSO, GSA, GAEPSO(Jiang et al., 2015) and MSGO(Secui et al., 2024a). The comparison is made based on the best cost and lowest emissions. The summary of the comparison between the Lagrange method and the mentioned heuristic algorithms is given in Table 3.12.

Table 3.12: The WTEED problem with Lagrange compared with other optimization algorithms for an IEEE 40-unit system for PD = 10,500 MW

Method	MGSO Without Wind Power	MSGO	PSO	GSA	GAEPSO	Proposed LMM 150 MW Wind Power	Proposed LMM 1100 MW Wind Power
P1 [MW]	114.000000	549.9997828	114.0000	105.5679	106.3768	114.0000	114.0000
P2 [MW]	113.999999	549.9997818	104.0000	88.2574	113.2637	114.0000	114.0000
P3 [MW]	120.000000	119.9988116	120.0000	105.9739	108.5784	120.0000	108.3202
P4 [MW]	189.999995	179.7374211	169.3671	150.3464	188.6623	190.0000	165.3147
P5 [MW]	96.999999	96.99883835	97.0000	82.0595	77.0086	97.0000	97.0000
P6 [MW]	140.000000	105.4022758	124.2630	119.5704	132.6636	140.0000	130.6214
P7 [MW]	300.000000	299.9999742	299.6931	248.5154	288.3156	300.0000	285.1828
P8 [MW]	300.000000	285.7135868	297.9093	276.3936	235.0264	300.0000	300.0000
P9 [MW]	299.999998	287.9519754	297.2578	244.2866	285.7760	300.0000	300.0000
P10 [MW]	279.599683	204.8086989	130.0007	262.1424	264.6783	236.1273	166.9658
P11 [MW]	168.799860	243.6012566	298.4210	293.2579	312.0426	279.1439	214.3810
P12 [MW]	94.0000003	243.6003501	298.0264	264.5149	112.8675	277.8553	212.4040
P13 [MW]	484.039161	394.2851366	433.5590	432.2395	486.8320	383.4865	289.4015
P14 [MW]	484.039166	394.2799802	421.7360	391.8179	341.2265	422.9446	318.7482
P15 [MW]	484.039164	394.2841752	422.7884	422.8119	428.9123	421.4392	317.4792
P16 [MW]	484.039178	484.0292251	422.7841	414.8810	436.8761	421.4392	317.4792
P17 [MW]	489.279372	489.2692227	439.4078	428.5659	426.2216	500.0000	462.7621
P18 [MW]	489.279372	399.5209877	409.4132	422.1613	442.5531	500.0000	464.5057
P19 [MW]	511.279600	506.0067276	439.4111	440.9423	454.6218	550.0000	506.5800
P20 [MW]	511.279490	421.5364187	429.4155	435.9092	491.0606	550.0000	506.5812
P21 [MW]	526.732209	433.5530376	439.4421	451.8724	450.2265	550.0000	550.0000
P22 [MW]	550.000000	514.2353651	439.4587	436.1765	406.2236	550.0000	550.0000
P23 [MW]	523.279384	433.5329212	429.7822	437.2970	464.5563	550.0000	550.0000
P24 [MW]	523.279383	433.5268561	439.7697	442.0350	444.5589	550.0000	550.0000

P25 [MW]	524.239856	433.5342317	430.1191	445.9564	455.3451	550.0000	550.0000
P26 [MW]	523.815577	433.7489257	440.1219	429.3785	468.2267	550.0000	550.0000
P27 [MW]	10.000020	10.05540017	28.9738	124.0932	103.8549	17.9826	13.9471
P28 [MW]	10.000113	10.24418652	29.0007	117.8668	146.2286	17.9826	13.9471
P29 [MW]	10.000007	10.0022597	28.9828	94.5359	148.8421	17.9826	13.9471
P30 [MW]	87.800155	89.80426078	97.0000	89.6485	96.7263	97.0000	97.0000
P31 [MW]	190.000000	189.998884	172.3348	153.1318	189.2261	190.0000	175.9692
P32 [MW]	190.000000	189.9955403	172.3327	159.0102	86.6516	190.0000	175.9692
P33 [MW]	190.000000	189.9978565	172.3262	148.7814	89.2264	190.0000	175.9692
P34 [MW]	200.000000	199.9994215	200.0000	176.4061	93.9663	90.0000	90.0000
P35 [MW]	199.999999	199.9994151	200.0000	170.0710	102.2234	90.0000	90.0000
P36 [MW]	164.799870	199.998299	200.0000	181.6662	168.2261	90.0000	90.0000
P37 [MW]	110.000000	110.0000000	100.8441	96.8108	78.2663	110.0000	110.0000
P38 [MW]	109.999999	109.9997758	100.8346	94.3094	107.8912	110.0000	110.0000
P39 [MW]	110.000000	109.9962344	100.8362	82.4816	98.0368	110.0000	110.0000
P40 [MW]	550.000000	509.5675741	439.3868	456.2560	442.4562	550.0000	506.5800
P41 [MW]	-	1100	66.2736	83.099	151.9009	150.294	1100
F _c [\$ /h]	136,454.336	126,645.1342	133,995.061	142,675.36	158,269.6617	133,541.733580	121,045.419972
% Deviation F _c [\$ /h] Compared to Developed LMM	2.992	1.13	2.54	4.17	6.66	2.454	3.313174 (Average)
P _L [MW]	958.620621	962.815076	-	-	-	1038.679	1063.127
E _T [kg/h]	347,578.490	239,155.7318	352,766.822	366,190.13	156,826.1213	105,267.750200	75,880.539978
% Deviation E _T [kg/h] Compared to Developed LMM	32.08	25.91371319	32.29	32.83	17.39	8.11	24.77 (Average)

Compared with the LMM (1100 MW) algorithm, the fuel costs for the MGSO (without wind), MGSO, PSO, GSA, GAEP SO, and LMM (150 MW) algorithms are 2.99%, 1.33%, 2.54%, 4.17%, 6.66%, and 2.454%, respectively. When solving the WTEED problem, the developed solution outperforms existing algorithms by 1–6%. Compared with the proposed LM method, the resulting NO_x emissions are 32.08%, 25.91%, 32.29%, 32.83%, 17.39%, and 8.11%, respectively. Compared with other optimisation techniques, the LM approach has successfully reduced pollution levels by 1–32%.

The fuel cost and emission figures for several algorithms used to solve the thermal economic problem with the developed LMM are compared in Table 3.13. The LMM is found to reduce fuel and emissions by 0.59% and 22.163%, respectively.

Table 3.13: Developed LMM compared with various algorithms for the 40-unit system (Secui et al., 2024a)

Algorithm	Fuel cost (\$/h)	Fuel cost (%)Deviation	Emission (kg/h)	Emission (%) Deviation
PSO	123,607.9479	0.523706	193,313.7047	21.8119754
DE	123,804.0394	0.56333	193,953.9668	21.87886
SCA	125,895.2706	0.981987	210,484.9674	23.50221
SGO	123,289.7874	0.45928	193,311.54075	21.81175
MGSO	123,161.8867	0.433334	193,311.54075	21.81175
LMM	121,045.419972	0.592327	75,880.5399	22.16331

The optimal solution to the WTEED problem emerged after 72 iterations of the optimisation procedure. Compared to the initial estimate of 8.9914, the optimised lambda value is 33.9059. In addressing the WTEED problem, the LM algorithm performed better than alternative optimisation algorithms. Additionally, Table 3.13 demonstrates that improving power generation from renewable energy sources can dramatically reduce emissions and fuel cost. Figures 3.8 and 3.9 graphically represent the correlations between fuel cost [USD/h], power demand [MW], and emissions for various optimisation strategies

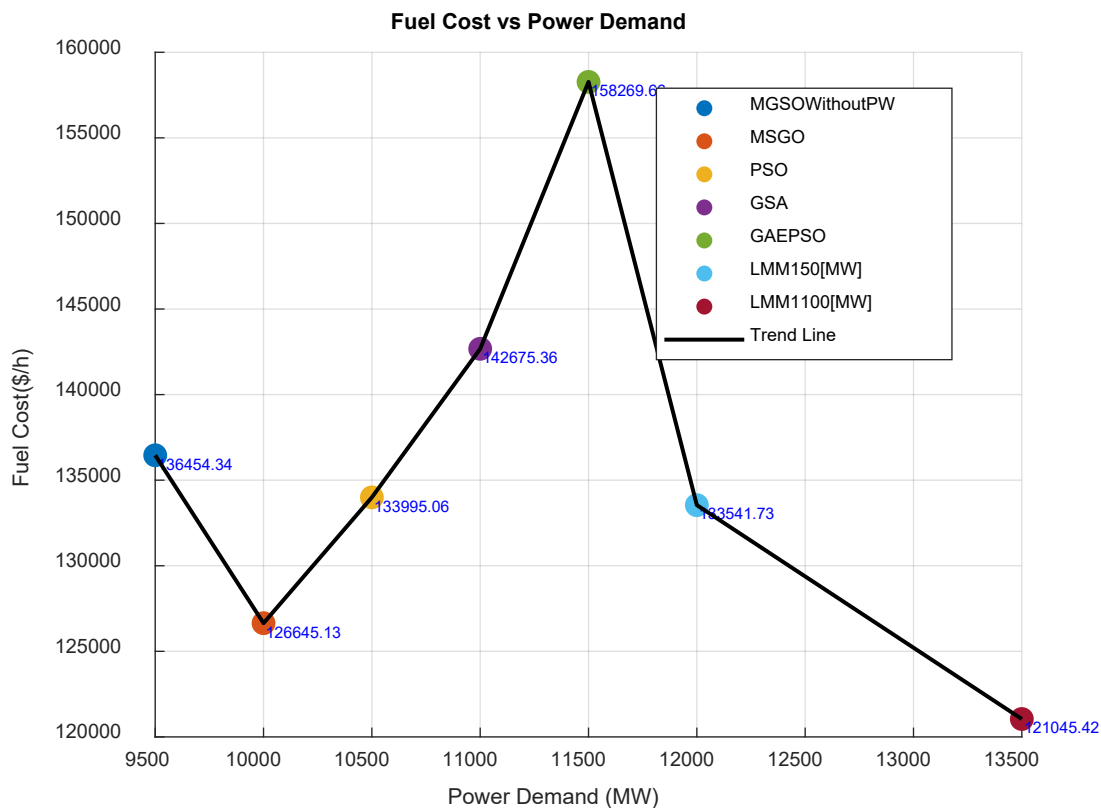


Figure 3.8: Values of Fuel cost and power demand for various algorithms using a 40-unit system in relation to the developed algorithm

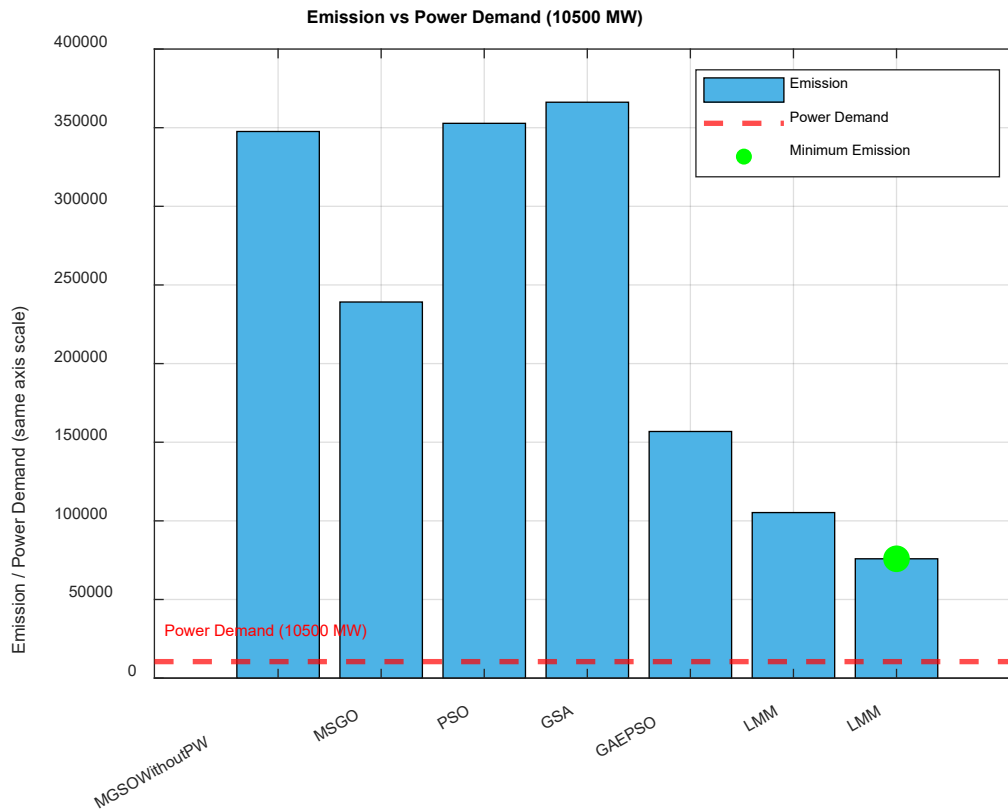


Figure 3.9: Values of emission and power demand for various algorithms using a 40-unit system in relation to the developed algorithm.

3.4 Conclusions

This chapter employs the Lagrange multiplier method to provide a successful solution to the wind-thermal economic emission dispatch problem. Fuel and emission costs are minimised in the bi-objective problem for economic emission dispatch optimisation. It also addresses transmission line losses, emissions, and inequality constraints. Three test systems, 6-unit, 10-unit, and 40-unit, are implemented to evaluate the effectiveness of the algorithm. Compared to other algorithms, the fuel cost and emissions for 6-unit systems are 3-6% and 1-3% lower, respectively. Additionally, compared with other optimisation techniques, the 10-unit system's fuel cost and emissions are 1-2% and 1-2.89%, respectively. Lastly, fuel consumption and emissions for the bigger system have been decreased by 1-6% and 1-32%, respectively.

Across all test systems, the Lagrange optimisation approach effectively converges to an optimal solution by selecting the best initial values for the lambda parameters. The resulting computational times for the 6-unit, 10-unit, and 40-unit models were 11.042308s for 84 iterations, 11.657372s for 1013 iterations, and 16.145170s for 72 iterations. In comparison, the optimal values for the 6-unit, 10-unit, and 40-unit systems are found to fall within the expected values reported in the literature for fuel cost, emissions, and total generation in the WTEED problem. It can also be seen that,

irrespective of load demand or the types of generators used, if the initial guess of λ is chosen carefully, the Lagrange multiplier always finds an optimal solution quickly and precisely. Furthermore, the results of the LM algorithm have been contrasted with those of other heuristic algorithms documented in the recent literature. Compared with heuristic approaches documented in the literature, the conventional LM algorithm may readily achieve optimal results in reducing fuel consumption and pollution. Considering straightforward, convex scenarios, Lagrange's classical methods are effective and precise. Chapter 4: Solving the Wind-Thermal Economic Emission Dispatch (WTEED) problem using Particle Swarm Optimisation (PSO) and comparing the results of heuristic and classical optimisation techniques.

CHAPTER FOUR

WIND-THERMAL ECONOMIC EMISSION DISPATCH(WTEED) PROBLEM USING PARTICLE SWARM OPTIMIZATION(PSO)

4.1 Introduction

This chapter solves the problem of WTEED using the PSO. Many researchers have solved the WTEED using PSO. In the work of (Mishra & Shaik, 2024b; Secui et al., 2024b; Zhang et al., 2019)The problem for WTEED is solved by minimizing both the fuel cost and emission using the price penalty factor h . Several price factors are used in solving the economic emission dispatch problem(Krishnamurthy & Tzoneva, 2012). In this chapter, a min-min penalty factor is adopted. The impact of varying wind power on the solution of the WTEED problem is compared across different IEEE 30-bus systems with 6-unit, 10-unit, and 40-unit generators. All three case studies are compared with the existing literature solution values using the developed PSO algorithm. The PSO algorithm is also compared with the classical Lagrange multiplier method developed in Chapter 3 for solving the WTEED problem.

A description of the PSO algorithm is presented in 4.2. In 4.3, the PSO method for solving the CEED problem is developed. The application of the PSO method and its comparison with the Lagrange method for IEEE power systems models are illustrated in 4.4. Sections 4.5 and 4.6 present the discussion and conclusions.

4.2 PSO algorithm

Kennedy and Eberhart developed the particle swarm optimisation technique in 1995. It is an optimisation based on how the swarm's species behaves. It provides a population-based search strategy in which species, referred to as particles, navigate an open, multidimensional space and change their positions over time.

Based on both its own and the other particle's experiences, the particle positioned itself in the solution space utilising the best position that both of them had encountered. Based on past experiences, the swarm follows the nearby particle. Every particle in the swarm travels around the search space at a specific speed that varies based on its prior experiences.

Let a particle coordinate (position) and its corresponding flight speed (velocity) in a search space denoted by p and v , respectively. The i^{th} particle is preserved as a volume less particle assumed by $p_i = (p_{i1}, p_{i2} \dots p_{id})$ and the best position as $p_i^{best} = (p_{i1}^{best}, p_{i2}^{best} \dots p_{id}^{best})$. The index of the best particle amongst others is given a name called global best g_d^{best} . The change of velocity of the i^{th} particle is given by $v_i = (v_{i1}, v_{i2} \dots v_{id})$. Equations (4.1) and (4.2) provide the immediate velocity and the

distance between p_{id}^{best} and g_d^{best} , respectively, which may be utilised to determine the updated velocity and location of each particle.

$$v^{t+1}_{id} = \omega v^t_i + c_1 rand()(p^{best}_{id} - p^t_{id}) + c_2 rand()(p^{best}_{id} - p^t_{id}) \quad (4.1)$$

$$p_{id}^{t+1}_i = p^t_{id} + v^{t+1}_{id} \quad (4.2)$$

Where

c_1 Self-assurance ranges between 1.5 and 2, and

c_2 Swarm range between 2 and 2.5.

$(p^{best}_{id} - p^t_{id})$ and $(p^{best}_{id} - p^t_{id})$ are a particle memory influence and a swarm influence.

The proper balance between global and local search can be achieved by selecting the inertia weight factor ω , to be between 0.9 and 0.4 during the search, and can be given

by the following expression:
$$\omega = \omega_{max} - \left[\frac{\omega_{max} - \omega_{min}}{iter_{max}} \right] iter$$

Where,

ω The inertia weight factor

ω_{max} and ω_{min} Maximum and minimum weighting factors

$Iter$ and $Iter_{max}$ Current and maximum iterations.

4.3 WTEED problem solution using the developed PSO algorithm

In Chapter 3, the WTEED problem is studied, formulated, and solved using LMM. The problem is formulated using the total fuel cost equation for thermal and wind power systems as given in equation (2.1). The fuel cost for conventional and wind power generators is given by equations (2.2) and (2.3). This is subject to equality and inequality constraints given in equations (2.4) and (2.6). The wind power system is further analyzed using the probability distribution function (PDF), yielding equations (2.46) and (2.51). The emission function is given by equation (2.52), and the price penalty factors (3.1)-(3.3) are used to formulate the single-objective function for the WTEED problem. The WTEED problem is solved using a heuristic optimisation algorithm, PSO, tailored to incorporate the specifics of the WTEED problem. It is needed to associate the structure of the WTEED problem with that of the velocity and position Equations (4.1) and (4.2) adopted by the PSO algorithm. This can be achieved with the following steps:

- The number of members in a distinct particle inside the swarm is equivalent to the number of generators. The active power generated by conventional and wind power producers is represented by the positions of particle members in the wind thermal economic dispatch problem.
- The velocities are parameters that represent the active power, even if they are utilized for finding within the boundaries.
- The swarm's particle population is determined to be N_p . Equations (2.1) to (2.6) and (2.46) to (2.52) provide the developed PSO algorithm for solving the combined economic dispatch problem:

Step1: Set the PSO initial values for the acceleration constants and inertia weight. The maximum number of iterations ($Iter^{max}$) and uniform random values (rand1, rand2) for c1 and c2.

Step 2: Employing the generator limit constraints in Equation (3.20), determine the minimum and maximum initial velocities, which are provided in Equation (4.3) as follows:

$$-0.5P_{pi}^{min} \leq V_{pi} \leq +0.5P_{pi}^{max}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.3)$$

Where

N_p Quantity of particles in the swarm

n The total number of generators equals the number of members in one particle.

The particle position and velocity are calculated for $(n - 1)$ generators, since the first generator is acknowledged as a slack one.

Step 3: Apply equation (4.4) to compute the initial velocity of every particle, with the exception of the slack bus generator.

$$V_{pi} = V_{pi}^{min} + rand() (V_{pi}^{max} - V_{pi}^{min}), p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.4)$$

Where

$V_{pi}^{min}, V_{pi}^{max}$ Minimum and maximum velocities previously determined

Step 4: Employ Equation (4.5) to determine the particle members' starting positions.

$$P_{pi} = P_{pi}^{min} + rand() (P_{pi}^{max} - P_{pi}^{min}), p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.5)$$

Wind power is added to equation (4.5) using equations (2.46) to (2.52) to obtain the active power for the WTEED problem. Then this is verified if they are within the given limits in equation(4.20), and is represented by the following equation(4.6)

$$\left\{ \begin{array}{l} P_{pi}^{min}, \quad P_{pi} \leq P_{pi}^{min} \\ P_{pi}^{max}, \quad P_{pi} \geq P_{pi}^{max} \\ P_{pi}, \quad P_{pi}^{min} \leq P_{pi} \leq P_{pi}^{max} \end{array} \right\}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.6)$$

The power system's buses are divided into three categories: load (PQ), generator (PV), and slack buses. Any bus connected to a generator with the greatest generating capacity is referred to as a slack bus in a power system. The system's voltage and angle are referenced by the slack bus. The slack bus's real and reactive powers are uncontrollable; the actual or reactive power necessary to balance the system's power flows is provided by the bus.

Generation scheduling is used to solve the economic dispatch problem without accounting for the actual power output of the slack bus generator. In the PSO algorithm, the slack bus serves to meet the power balance requirement specified in Equation (2.4). Step 5 outlines the process for determining the real power of the slack bus generator in the PSO algorithm.

Step 5: The slack bus generator is considered to have the most power-generating capability among dependent generators. Equation (4.7) provides the power balance constraint that may be used to calculate the initial active power P_{pd} using the bus voltage magnitude and phase angle as a reference (Krishnamurthy & Tzoneva, 2012):

$$P_{pd} + \sum_{\substack{i=1 \\ i \neq d}}^n P_{pi} = \left\{ \sum_{\substack{i=1 \\ i \neq d}}^n \sum_{\substack{j=1 \\ j \neq d}}^n P_{pi} B_{ij} P_{pj} + \sum_{\substack{j=1 \\ j \neq d}}^n P_{pj} (B_{jd} + B_{dj}) P_{pd} + B_{dd} P_{pd}^2 + \sum_{\substack{i=1 \\ i \neq d}}^n B_{io} P_{pi} + B_{do} P_{pd} + B_{oo} + P_D \right\}, p = \overline{1, N_p} \quad (4.7a)$$

Where

P_{pd} Is the power generated by the slack bus?

P_D Is the entire power demand of the power system

$\sum_{\substack{i=1 \\ i \neq d}}^n P_{pi}$ Is the power system's total active power, except for the slack bus power.

, and is

$$\text{given by } \sum_{\substack{i=1 \\ i \neq d}}^n P_{pi} = [P_{T1}, P_{T2} \dots P_{TN_T}, P_{W1}, P_{W2} \dots P_{WN_w}], \quad (4.7b)$$

Where,

P_{TN_T} Is the active power produced by thermal power generators.

P_{WN_w} Is the active power produced by wind power generators.

By using the quadratic form, Equation (4.7) can be rewritten, where the P_{pd} is the unknown variable in the equation.

$$XP_{pd}^2 + YP_{pd} + Z = 0 \quad (4.8)$$

Where

$$X = B_{dd} \quad (4.9)$$

$$\sum_{\substack{j=1 \\ j \neq d}}^n P_{pj}(B_{jd} + B_{dj}) + B_{do} - 1 \quad (4.10)$$

$$Z = \sum_{\substack{i=1 \\ i \neq d}}^n \sum_{\substack{j=1 \\ j \neq d}}^n P_{pi}B_{ij}P_{pj} + \sum_{\substack{i=1 \\ i \neq d}}^n B_{io}P_{pi} + B_{oo} + P_D - \sum_{\substack{i=1 \\ i \neq d}}^n P_{pi} \quad (4.11)$$

Equation (4.8) positive root can be determined as follows:

$$P_{pd} = \frac{-Y + \sqrt{Y^2 - 4XZ}}{2X}, \text{ where } Y^2 - 4XZ \geq 0 \quad (4.12)$$

The actual power vector is now constructed as $P_p = [P_{pd}, P_{pi}, i = 1, n, i \neq d]$ where $p = \overline{1, N_p}$

Step 6: Determine the following objective functions for the particles' starting positions.

Fuel cost function

$$F_{Cp} = \sum_{i=1}^n (a_i P_{pi}^2 + b_i P_{pi} + c_i), p = \overline{1, N_p} \quad (4.13)$$

Emission function

$$F_{Tp} = \sum_{i=1}^n (d_i P_{pi}^2 + e_i P_{pi} + f_i), p = \overline{1, N_p} \quad (4.14)$$

Combined economic emission function

$$F_{CT} = \sum_{i=1}^n (a_i P_{pi}^2 + b_i P_{pi} + c_i) + h_{pi}(d_i P_{pi}^2 + e_i P_{pi} + f_i), p = \overline{1, N_p} \quad (4.15)$$

Where the calculation of the Min-Max price penalty factor is

$$h_{pi} = \frac{a_i P_{pi,max}^2 + b_i P_{pi,max} + c_i}{d_i P_{pi,max}^2 + e_i P_{pi,max} + f_i}, p = \overline{1, N_p}, i = \overline{1, n} \quad (4.16)$$

The fuel cost values F_{Tp} of all the particles are organised in ascending order. The value at the highest point of the ascending sequence is chosen as the F_T^{best} .

Step 7: Choose the global best starting position and the best initial position as follows:

The initial particle locations in the swarm are assumed to be optimal.

$$P_p^{best} = \min P_p^{best}, p = \overline{1, N_p}, i = \overline{1, n}.$$

- The best position out of all the best particles $\min P_p^{best}$, $p = \overline{1, N_p}$ is taken as

$$G_p^{best} = \min P_p^{best}, p = \overline{1, N_p}$$

l^{th} step of the iteration process commences, where $l = l + 1$

Step 8: Applying equation (4.17) to calculate the new velocity.

$$V_{pi}^{new^l} = \omega \cdot V_{pi}^{l-1} + c1 * rand1() (P_p^{best^{l-1}} - P_{pi}^{l-1}) + c1 * rand1() (G^{best^{l-1}} - P_{pi}^{l-1}),$$

$$p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.17)$$

Check the limits on the minimum and maximum velocity values.

$$\text{If } V_{pi}^{new^l} > V_{pi}^{max^{l-1}}, V_{pi}^{new^l} = V_{pi}^{max^{l-1}} \text{ and}$$

$$\text{If } V_{pi}^{new^l} < V_{pi}^{min^{l-1}}, V_{pi}^{new^l} = V_{pi}^{min^{l-1}}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.18)$$

Step 9: Applying Equation (4.19), determine the generator's new location within the particles.

$$\text{If } P_{pi}^{new^l} = P_{pi}^{l-1} + V_{pi}^{new^l}, p = \overline{1, N_p}, i = \overline{1, n} \quad (4.19)$$

Step 10: Employ the constraint Equation (4.6) to validate the generators' new positions within the particles as follows

$$P_{pi}^{new^l} = \left\{ \begin{array}{l} P_{pi}^{min}, \quad P_{pi}^{new^l} \leq P_{pi}^{min} \\ P_{pi}^{max}, \quad P_{pi}^{new^l} \geq P_{pi}^{max} \\ P_{pi}^{new}, \quad P_{pi}^{min} \leq P_{pi}^{new^l} \leq P_{pi}^{max} \end{array} \right\}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (4.20)$$

Step 11: Determine the new real power of the slack bus generator. Utilising the formula from step 5, establish the new real power vector $P_{pd}^{new^l}$. Employing the constraint Equation (4.6), determine the slack bus generators' new position within the particles.

$$P_{pd}^{new^l} = \left\{ \begin{array}{l} P_{pd}^{min}, \quad P_{pd}^{new^l} \leq P_{pd}^{min} \\ P_{pd}^{max}, \quad P_{pd}^{new^l} \geq P_{pd}^{max} \\ P_{pd}^{new}, \quad P_{pd}^{min} \leq P_{pd}^{new^l} \leq P_{pd}^{max} \end{array} \right\} \quad (4.21)$$

Step 12: For the l^{th} iteration, the entire active power vector is:

$$P_{pd}^{new^l} = (P_{pd}^{new^l}, P_{pi}^{new^l}, i \neq d, i = \overline{1, n}), p = \overline{1, N_p} \quad (4.22)$$

Step 13: Compute the new objective functions F_T^{new} with Step 6

Step 14: Validate the new objective function F_T^{new} as explained below

$$\text{If } F_T^{new^l} < F_T^{best^{l-1}} \text{ then } F_T^{best^l} = F_T^{new^l} \text{ and } P_{pi}^{best^l} = P_{pi}^{new^l}$$

$$\text{Else If } F_T^{best^l} = F_T^{best^{l-1}} \text{ and } P_{pi}^{best^l} = P_{pi}^{best^{l-1}} \quad (4.23)$$

$$G^{best^l} = P_p^{best^l}, p = \overline{1, N_p}$$

where l is the number of iterations

The best solution G^{best} is only one for the whole system. The best solution per particle is only one $P_p^{best} = \min P_{pi}, i = \overline{1, n}$.

The best solution for the whole system is $P_p^{best} = [P_1^{best}, P_1^{best}, \dots, P_{N_p}^{best}]$. Then

$$G^{best} = \min P_p^{best^l}, p = \overline{1, N_p}$$

Step 15: Repeat steps 5-13 until the maximum number of iterations is reached. The PSO flowchart is shown in Figure 4.1 below.

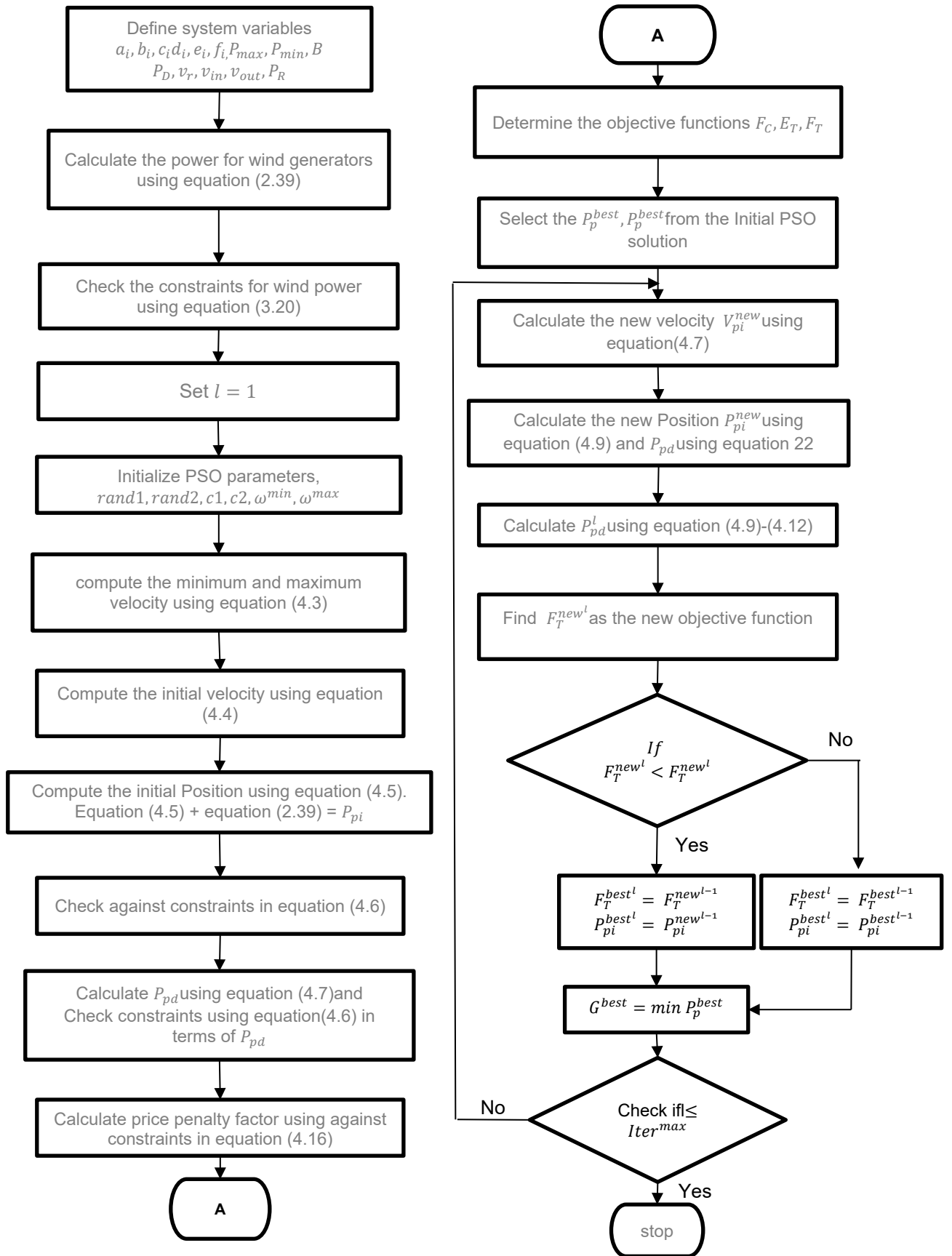


Figure 4.1: PSO algorithm for the WTEED problem solution flowchart.

4.4 Application of the PSO algorithm to solve the WTEED problem

The PSO algorithm is used to solve the WTEED problem. The problem is tested using three different case studies: the IEEE 30-bus system with 6 units, the IEEE 10-unit system, and the IEEE 40-unit system. These are discussed separately in 4.4.1, 4.4.2, and 4.4.3, respectively.

4.4.1 Test system 1: IEEE 30 bus system with six generation units

The problem of solving WTEED using the PSO algorithm is addressed using a system comprising six thermal generators and one wind turbine cluster. The fuel cost parameter are formed with the ones reported in (Krishnamurthy & Tzoneva, 2012), and (Gnanadass, 2005), and for wind power, the coefficients are those reported in (Damodaran & Sunil Kumar, 2018; Liu & Xu, 2010). The bi-objective optimisation problem is converted to a single problem by using the max-max price penalty factor as given in equations (3.1)-(3.3)(Krishnamurthy & Tzoneva, 2012). Several power demand values are presented in Table 4.1 in order to test the system's behaviour to changes in power demand. The software is provided in Appendix B1, and the MATLAB script is named WTEED_casePSO6units.m. The solution of the WTEED problem is shown in Table 4.1. The real power of the thermal (P1-P6) units, wind (Pw) generators, transmission losses (P_L) in [MW], fuel cost (F_C) for thermal generators, total emission (E_T) in [kg/h], and CEED in [Kg/h].

Table 4.1: The wind-thermal economic emission dispatch problem using PSO method with various power demands

PD[MW]	125	150	175	225	250	283.4
P1[MW]	5.00	5.00	5.00	5.00	5.00	5.00
P2[MW]	5.00	5.00	5.00	10.34	16.11	41.87
P3[MW]	5.00	5.00	5.00	5.00	5.00	10.13
P4[MW]	5.00	26.22	5.00	91.44	120.00	5.00
P5[MW]	5.00	5.00	5.00	5.13	5.00	9.92
P6[MW]	5.00	5.00	52.39	12.45	5.00	13.09
Pw[MW]	100.2	100.2	100.2	100.20	100.2	200.00
PL[MW]	1.00	1.400	2.6	4.50	6.30	4.00
Fc[\$/h]	50,820	53,0081	58,1999	62,2608	65,4475	59,5914
ET[Kg/h]	28.40	28.00	27.40	29.10	31.30	25.8

The values for transmission losses (P_L) in MW, fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h] for the WTEED problem shown in Table 4.1 above.

The wind-thermal economic emission dispatch problem using the PSO algorithm is compared with other optimization algorithm (Zhang et al., 2019). The Lagrange multiplier method developed in Chapter 3, shown in Table 4.2 below, is compared with various optimization algorithms.

Table 4.2: PSO and LMM compared to other optimisation algorithms for the WTEED problem, PD = 283.4 MW

Reference	(Jiang et al., 2019)			Developed algorithms	
Algorithm	GSA	GPSOA	GA	LMM	PSO
P1[MW]	49.21	31.65	36.62	19.76	5.00
P2[MW]	46.21	45.22	42.58	41.31	41.87
P3[MW]	36.69	42.49	30.31	51.05	10.13
P4[MW]	33.32	38.37	31.36	89.58	5.00
P5 [MW]	43.77	43.42	53.44	49.58	9.92
P6[MW]	53.51	47.62	43.52	35.09	13.09
Pw [MW]	20.69	34.63	45.57	200.200	200.20
PL[MW]	-	-	-	3.9600	4.00
Fc[\$/h]	66123.00	66134.00	66582.00	50589.00	59591.4
%Deviation of Fc for PSO in relation to the literature	2.59	2.60	2.77	4.08	3.01 Average
E _T [Kg/h]	23.17	24.26	26.18	19.6400	25.8
%Deviation of E _T for PSO in relation to the literature	2.69	1.54	0.37	6.79	2.8475 Average

The WTEED problem is solved considering a load demand of 283.4MW and a wind farm consisting of 200 identical wind turbines, each with 1.5 MW power capacity, for a total wind farm installed capacity of 200 MW.(Liu et al., 2018). The PSO algorithm is compared with Genetic Algorithm (GA), Gravitational Search Algorithm (GSA), and a hybrid Gravitational Particle Swarm Optimization Algorithm (GPSOA).

4.4.1.1 The IEEE30 bus system with 6-unit results discussion

This system has utilized 50 available wind turbines that supply the power dispatch problem with 200MW. The developed algorithm for a 6-unit system is used and compared with LMM and other optimisation algorithms as presented in Table 4.2. The fuel cost obtained for the GSA, GPSOA, GA, and LMM algorithms is 2.59%, 2.60%, 2.77%, and 4.08%, respectively, compared to the PSO algorithm. The proposed algorithm is 1–3% better than other algorithms used to solve the wind–thermal economic emission dispatch problem. The resultant NOx emissions are 2.69%, 1.54%, 0.37%, and 6.79%, 0.26%, compared to the proposed PSO algorithm. The PSO method has effectively reduced pollutant levels by 1–2.8% compared to other optimization algorithms. The table shows that fuel cost and emissions are lower with Lagrange's method than with the other methods. This can also be shown graphically, as presented in Figures 4.2 and 4.3 below. The following graphs show the relationships

between power demand, fuel cost, and emissions for the various methods presented in Table 4.2 above.

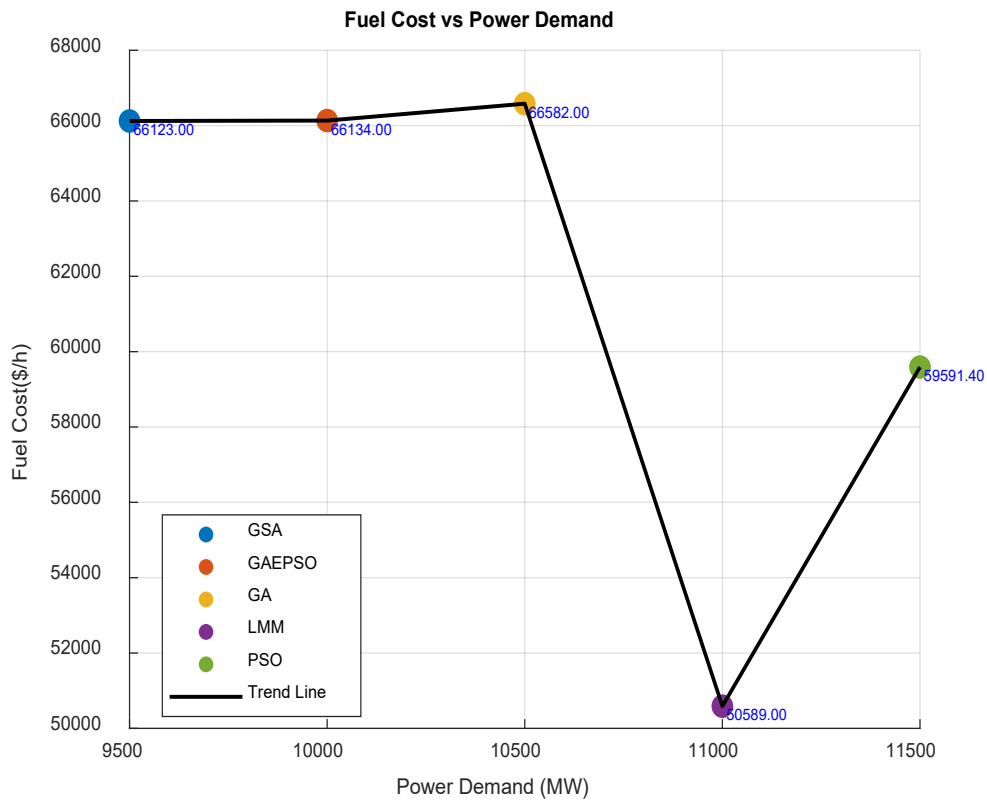


Figure 4.2: Values of fuel cost and power demand for various algorithms using a 6-unit system compared to the developed PSO

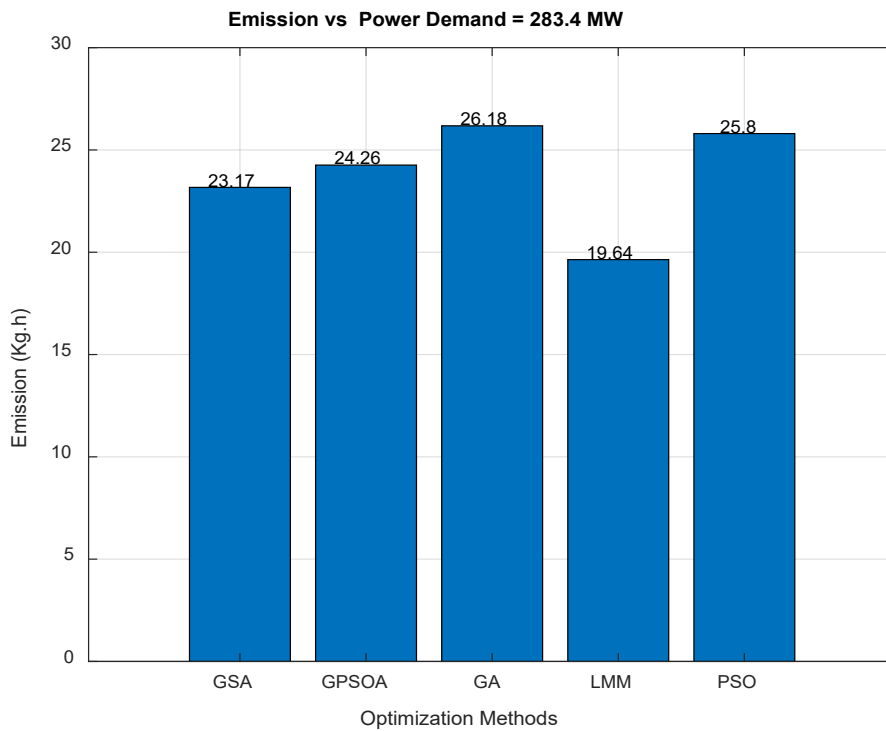


Figure 4.3: Values of emission and power demand for various algorithms using a 6-unit system compared to the developed PSO

4.4.2 Test system 2: IEEE 30 bus system with 10 generation units

This study of the WTEED power system problem using PSO includes 10 thermal generators and one wind turbine cluster. The cluster consists of wind turbines situated in a geographic area, characterised by a group of equal turbines in a large wind farm. The fuel cost, emission, and loss coefficients are constructed based on the ones reported on (Basu, 2011b). Moreover, the results are presented in Tables 3.6 and 3.7. The test system uses the same wind parameters as reported in Test System I. The multi-objective optimisation problem is converted to a single problem by using the min-max price penalty factor as in test system I. The study focuses on the 2000MW power demand as presented in (Mishra & Shaik, 2024b). Several power demand values ranging from 650 to 2000 [MW] are used to test the system's behaviour to changes in power demand. The software is provided in Appendix B2, and the MATLAB script is named WTEED_casePSO10units. m. The solution of the WTEED problem is shown in Table 4.3. The table illustrates the real power of the thermal (P1-P10) units, wind (Pw) generators, and transmission losses (P_L) in [MW], fuel cost (F_C) for thermal generators, total emission (E_T) in [kg/h], and CEED in [Kg/h].

Table 4.3: The wind-thermal economic emission dispatch problem using PSO with various power demands for 10-unit generators

PD[MW]	650	800	1000	1200	1500	2000
P1[MW]	10	10.00	10.00	26.43	14.1450	37.6848
P2[MW]	20	20.00	67.02	42.78	37.3342	70.8940
P3[MW]	47	47.00	117.63	58.55	104.4475	81.0499
P4[MW]	20	20.49	21.58	96.21	72.6856	128.5784
P5[MW]	50	122.01	90.53	92.29	87.2873	108.1157
P6[MW]	70	70.00	70.00	102.29	150.3286	146.7899
P7[MW]	60	60.00	60.00	108.19	178.7130	252.6337
P8[MW]	70	82.73	200.01	70.55	247.4480	265.0825
P9[MW]	135	135.00	135.00	229.37	323.7965	470.0000
P10[MW]	150	150.00	150.00	314.43	235.4756	441.0383
Pw[MW]	100.166	100.166	100.166	100.17	100.166	100.166
PL[MW]	15.14	17.40	21.93	41.26	51.827	102.033
Fc[\$/h]	37137.345	42392.449	52214.646	62202.01	78621.468	107838.272
E _T [Kg/h]	1427.308	1508.206	1898.959	1971.98	2553.717	3988.590
CEED[Kg/h]	-	44008.891	54113.606	64173.99	81175.186	111826.862

The optimum values of transmission losses (P_L) in MW, fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h] for the WTEED problem shown in Table 4.3 above. The WTEED problem outputs obtained using the PSO algorithm are compared with those of multiple optimization algorithms reported in (Mishra & Shaik, 2024b) and are shown in Table 4.4. The solution to the problem for WTEED is considered with a load demand of 2000MW and a wind farm consisting of 50 identical wind turbines. The developed PSO algorithm is compared with the developed Lagrange multiplier method from Chapter 3, as well as with Moth-Flame Optimisation (MFO), the Whale

Optimisation Algorithm (WOA), the Search and Rescue Algorithm (SAR), and the Genetic Algorithm (GA) (Mishra & Shaik, 2024b).

Table 4.4: PSO compared to the LM method and other optimization algorithms for the WTEED Problem applied to a 10-unit system, PD = 2000[MW]

Algorithm	MFO	WOA	SAR	GA	Developed LMM	Developed PSO
P1[MW]	37.16	46.96	53.49	34.17	107.0710	37.6848
P2[MW]	25.84	68.61	77.10	63.49	104.4629	70.8940
P3[MW]	120	69.24	64.41	95.75	108.4683	81.0499
P4[MW]	93.90	129.21	83.05	121.67	107.9097	128.5784
P5[MW]	160	50	158.73	145.83	105.2629	108.1157
P6[MW]	240	226	239.50	229.86	126.3436	146.7899
P7[MW]	244.61	298.21	275.88	281.21	244.2553	252.6337
P8[MW]	286.25	337.93	332.28	307.35	276.0585	265.0825
P9[MW]	470	390.40	409.12	391.63	407.7432	470.0000
P10[MW]	404.92	468	388.56	410.56	410.7996	441.0383
PW[MW]	30	30	30	30	100.166	100.166
Fc[\$]	116690.89	114678.84	114106.19	115802.24	107533.05	107838.272
%Deviation of Fc for PSO in relation to the literature	4.10	3.17	2.91	3.69	0.14	2.79 Average
PL[MW]	83.70	84.44	82.81	83.9	98.490	102.033
ET[T]	4080	4220	4103.3	4390	3967.871841	3988.590
%Deviation of E _T for PSO in relation to the literature	1.15	2.90	1.44	5.03	0.26	2.16 Average
CEED[\$]	239158.66	244987.20	226506.78	231903.60	111500.921	111826.862

4.4.2.1 The IEEE 30 bus system with 10 units results discussion

The PSO algorithm is applied to solve the economic emission dispatch problem with wind power, using 10 conventional generators and 50 available wind turbines across 50 identical wind farms. The fuel cost obtained for the MFO, WOA, SAR, GA, and LMM algorithms are 4.10%, 3.17%, 2.91%, 3.69%, and 0.14%, respectively, compared to the PSO algorithm. The proposed algorithm is 1–3% superior to other algorithms for solving the wind–thermal economic emission dispatch problem. The resultant NO_x emissions are 1.15%, 2.90%, 1.44%, 5.03%, and 0.26% compared to the proposed LM algorithm. The LM method has effectively reduced pollutant levels by 1–2% compared to other optimization algorithms. The table shows that fuel cost, emissions, and CEED values are lower with Lagrange's method than with the other methods. Nevertheless, the obtained solutions are not the same as Lagrange's, since PSO generates a random solution for each execution. Fuel cost, emissions, and CEED are shown graphically in Figures 4.4, 4.5, and 4.6 below.

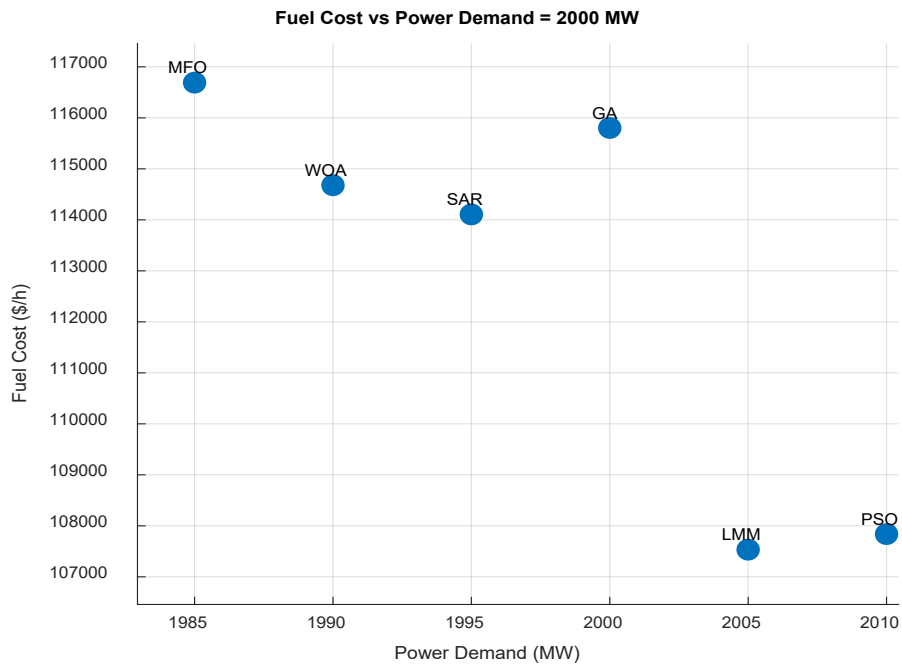


Figure 4.4: Values of fuel cost and power demand for various algorithms applied to a 10-unit system, and compared to the developed PSO algorithm

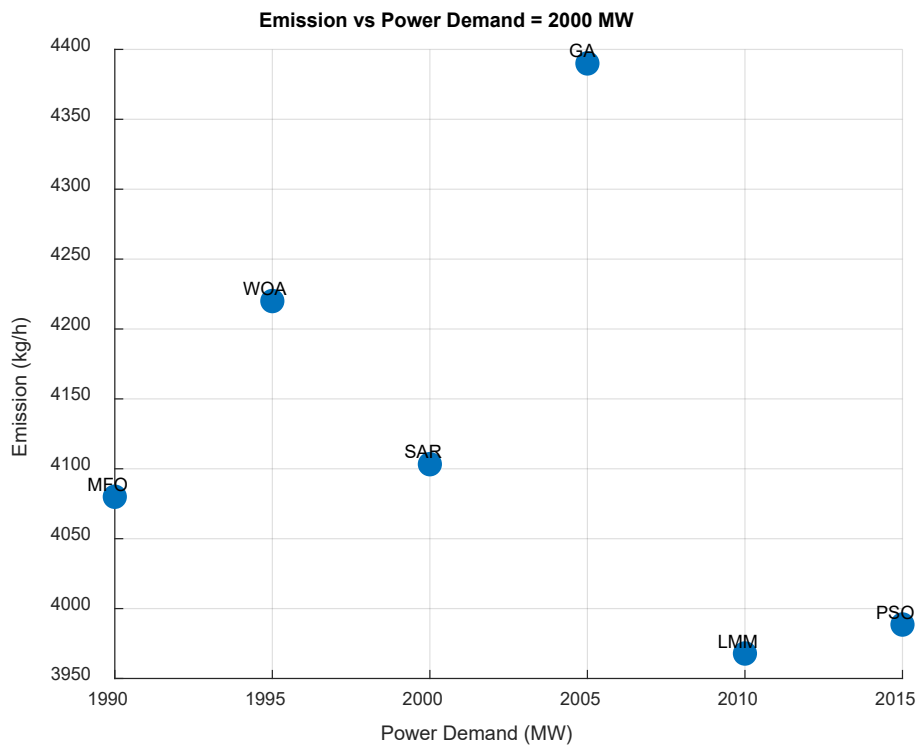


Figure 4.5: Values of emission and power demand for various algorithms applied to a 10-unit system, and compared to the developed PSO algorithm

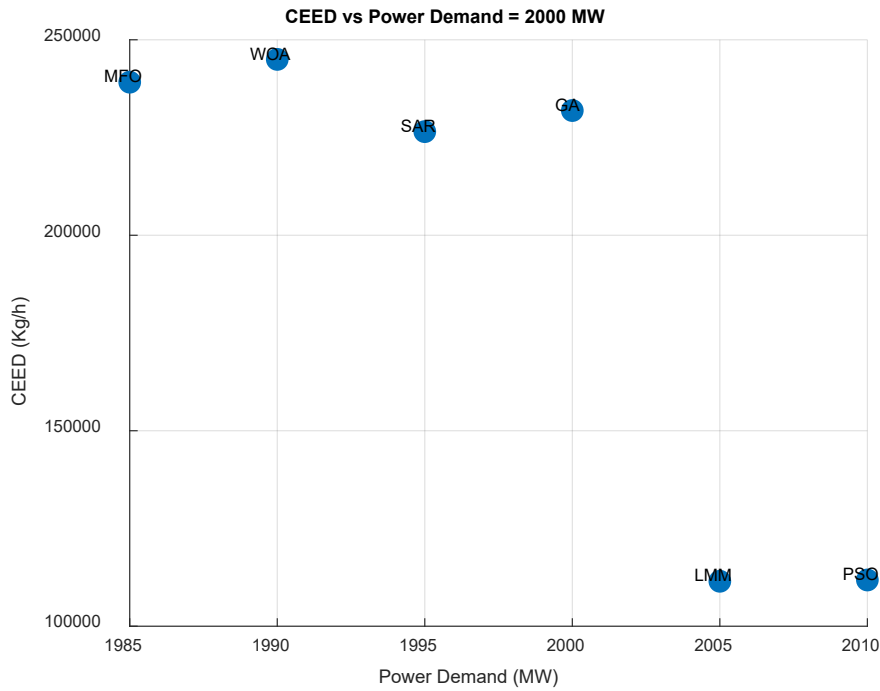


Figure 4.6: Values of CEED and power demand for various algorithms applied to a 10-unit system in relation to the developed PSO algorithm

4.4.3 Test System 3: IEEE 30 bus system with 40 generation units

The solution for the WTEED is verified using a power system with 40 thermal power generators, a power demand of 10500MW, and transmission losses, excluding VPLE. Power constraints, fuel cost coefficients, pollution coefficients, and B-loss coefficients are among the power system constraints that originate from (Secui et al., 2024b). The coefficients are illustrated in Tables 3.9 and 3.10, respectively.

As noted in test system two, the cluster consists of land-based wind turbines, including a collection of identical turbines in a sizable wind farm. Similar to test systems I and II above, the max-max price penalty factor is used to convert the bi-objective optimisation problems into a single optimisation power system problem.

The PSO algorithm is contrasted with various heuristic algorithms, i.e., (GSA, GAEPSO) (Jiang et al., 2015) and MSGO (Secui et al., 2024b) as well as with the developed Lagrange Multiplier Method. The evaluation is completed for the best cost and emission. The system response to variations in power demand can be tested using a range of power demand values. Table 4.5 illustrates the solution to the WTEED problem. The actual power values for thermal (P1–P40) units, wind (Pw) generators, fuel cost (F_C) for thermal generators, transmission losses (P_L) in [MW], total emissions (E_T) in [kg/h], and CEED in [Kg/h]. The software is provided in Appendix B3, and the MATLAB script is termed WTEED_casePSO40units.m

Table 4.5: Various power demands applied to a 40-unit generator for PSO WTEED problem

PD[MW]	10500	11000	12000	11300
P ₁ [MW]	114.0000	36	114	114
P ₂ [MW]	114.0000	114	114	114
P ₃ [MW]	120.0000	120	60	120
P ₄ [MW]	190.0000	190	80	190
P ₅ [MW]	97.0000	97	97	97
P ₆ [MW]	96.6707	68	68	68
P ₇ [MW]	223.6840	300	300	300
P ₈ [MW]	300.0000	300	300	300
P ₉ [MW]	135.0000	300	135	300
P ₁₀ [MW]	300.0000	300	130	300
P ₁₁ [MW]	375.0000	375	375	375
P ₁₂ [MW]	375.0000	375	94	375
P ₁₃ [MW]	500.0000	500	500	500
P ₁₄ [MW]	125.0000	500	500	500
P ₁₅ [MW]	500.0000	125	500	500
P ₁₆ [MW]	500.0000	500	500	500
P ₁₇ [MW]	500.0000	500	500	500
P ₁₈ [MW]	500.0000	500	500	500
P ₁₉ [MW]	550.0000	550	550	550
P ₂₀ [MW]	550.0000	242	242	242
P ₂₁ [MW]	550.0000	550	550	550
P ₂₂ [MW]	550.0000	550	254	550
P ₂₃ [MW]	254.0000	550	550	550
P ₂₄ [MW]	550.0000	254	550	550
P ₂₅ [MW]	550.0000	550	550	550
P ₂₆ [MW]	550.0000	550	550	550
P ₂₇ [MW]	150.0000	150	150	150
P ₂₈ [MW]	10.0000	150	150	150
P ₂₉ [MW]	150.0000	150	150	150
P ₃₀ [MW]	97.0000	97	47	97
P ₃₁ [MW]	190.0000	190	60	190
P ₃₂ [MW]	190.0000	60	190	190
P ₃₃ [MW]	190.0000	190	190	190
P ₃₄ [MW]	90.0000	200	200	200
P ₃₅ [MW]	200.0000	90	200	90
P ₃₆ [MW]	90.0000	90	200	200
P ₃₇ [MW]	110.0000	110	110	110
P ₃₈ [MW]	110.0000	110	110	110
P ₃₉ [MW]	110.0000	25	110	110
P ₄₀ [MW]	550.0000	550	550	550
P _w [MW]	150.249	150.249	150.249	150.249
F _c [\$/h]	157665.001	166404.803	164009.405	177272.170
P _L [MW]	1056.597	949.111	1038.643	1210.910
E _T [Kg/h]	199232.044	238948.748	211643.033	252972.712
CEED[Kg/h]	356940.591	-	-	-

4.4.3.1 The IEEE 30 bus system for 40 units results, and discussion

This is a fourth-generation unit system used to evaluate the effectiveness of the Lagrange multiplier method compared to other optimization methods for minimizing fuel cost and atmospheric emissions. Table 4.6 below shows that the fuel costs for the MGSO, GSA, GAEPSo, and LMM (1100 MW) algorithms are 1.11%, 4.09%, 6.60%, and 0.02%, respectively, compared to the PSO (1100 MW) algorithm. The proposed algorithm is 1–3% superior to other algorithms for solving the WTEED problem. The resultant NO_x emissions are 28.96%, 35.18%, 21.11%, and 0.02% compared to the

proposed PSO algorithm. The PSO method has effectively reduced pollutant levels by 1–22% compared to other optimization algorithms.

Table 4.6: PSO compared to the LM method and other optimization algorithms for the WTEED problem applied to a 40-unit system, PD = 10500[MW]

Algorithm	MSGO	GSA	GAEPSO	Developed PSO 1100[MW] wind power	Developed LMM 1100[MW] wind power
Reference	(Secui et al.,2025)	(Jiang and Wang.,2015)	Wang.,2015)		
P ₁ [MW]	549.9997828	103.9422	104.8952	114.0000	141.5002
P ₂ [MW]	549.9997818	103.9422	113.0724	113.9999	141.5002
P ₃ [MW]	119.9988116	112.2758	91.9834	119.9997	135.7827
P ₄ [MW]	179.7374211	97.2549	161.3754	189.8484	192.7574
P ₅ [MW]	96.99883835	179.8187	96.8920	97.0000	124.5002
P ₆ [MW]	105.4022758	95.0966	139.2597	71.9253	158.0745
P ₇ [MW]	299.9999742	119.5940	291.8542	299.9897	312.5901
P ₈ [MW]	285.7135868	263.8120	261.6582	256.9563	327.5002
P ₉ [MW]	287.9519754	263.0950	298.5412	300.0000	327.5002
P ₁₀ [MW]	204.8086989	269.5109	140.7686	130.0000	194.3838
P ₁₁ [MW]	243.6012566	130.8497	102.6502	236.1939	241.8042
P ₁₂ [MW]	243.6003501	102.1717	94.9653	203.5049	239.8264
P ₁₃ [MW]	394.2851366	95.9356	138.3682	500.0000	316.7899
P ₁₄ [MW]	394.2799802	129.7004	308.3268	171.2636	346.1246
P ₁₅ [MW]	394.2841752	301.7727	302.8832	175.4570	344.8558
P ₁₆ [MW]	484.0292251	301.7773	306.0256	201.6798	344.8558
P ₁₇ [MW]	489.2692227	496.6855	453.9314	485.4771	490.1056
P ₁₈ [MW]	399.5209877	490.4517	478.8826	499.9893	491.8484
P ₁₉ [MW]	506.0067276	502.7192	521.2446	549.8790	533.9051
P ₂₀ [MW]	421.5364187	510.7183	526.3789	549.9993	533.9064
P ₂₁ [MW]	433.5530376	523.3236	519.7761	548.8774	577.5002
P ₂₂ [MW]	514.2353651	524.7491	516.7892	549.9889	577.5002
P ₂₃ [MW]	433.5329212	523.4055	516.3568	549.9876	577.5002
P ₂₄ [MW]	433.5268561	522.6936	508.0922	426.8130	577.5002
P ₂₅ [MW]	433.5342317	522.6783	521.0308	550.0000	577.5002
P ₂₆ [MW]	433.7489257	518.1215	519.1626	550.0000	577.5002
P ₂₇ [MW]	10.05540017	149.7369	102.2686	10.0000	41.4425
P ₂₈ [MW]	10.24418652	131.3113	132.0367	10.0019	41.4425
P ₂₉ [MW]	10.0022597	130.7194	137.3896	10.0024	41.4425
P ₃₀ [MW]	89.80426078	92.7962	96.5634	69.3648	124.5002
P ₃₁ [MW]	189.998884	185.4022	168.7821	189.9978	203.4342
P ₃₂ [MW]	189.9955403	164.0935	176.2361	189.9999	203.4342
P ₃₃ [MW]	189.9978565	168.3946	168.7295	189.9995	203.4342
P ₃₄ [MW]	199.9994215	166.0944	129.6826	199.9999	117.5002
P ₃₅ [MW]	199.9994151	104.4641	185.6648	200.0000	117.5002
P ₃₆ [MW]	199.998299	167.3644	168.0922	199.9882	117.5002
P ₃₇ [MW]	110.0000000	89.9918	96.2245	25.0030	137.5002
P ₃₈ [MW]	109.9997758	102.7658	104.6853	93.5475	137.5002
P ₃₉ [MW]	109.9962344	108.1541	105.2245	84.0954	137.5002
P ₄₀ [MW]	509.5675741	532.2987	532.2893	549.9995	533.9051
P _w [MW]	1100	121.0666	151.9035	1100	1100
F _c [\$/h]	126645.134	142675.36	158269.6617	121107.584	121022.329581
%Deviation of F _c for PSO compared with literature	1.11	4.09	6.	2.97 Average	0.02
P _L [MW]	962.815076	-	-	1065.454	1063.149649
E _T [Kg/h]	239155.73184	366190.13	156826.1213	63713.052	75841.336841
%Deviation of E _T for PSO in relation to the literature	28.96	35.18	21.11	22.39 (Average)	4.35

Figures 4.7 and 4.8 graphically represent the relationship between fuel expenditure [\$ /h], power demand [MW], and emissions for various optimisation strategies.

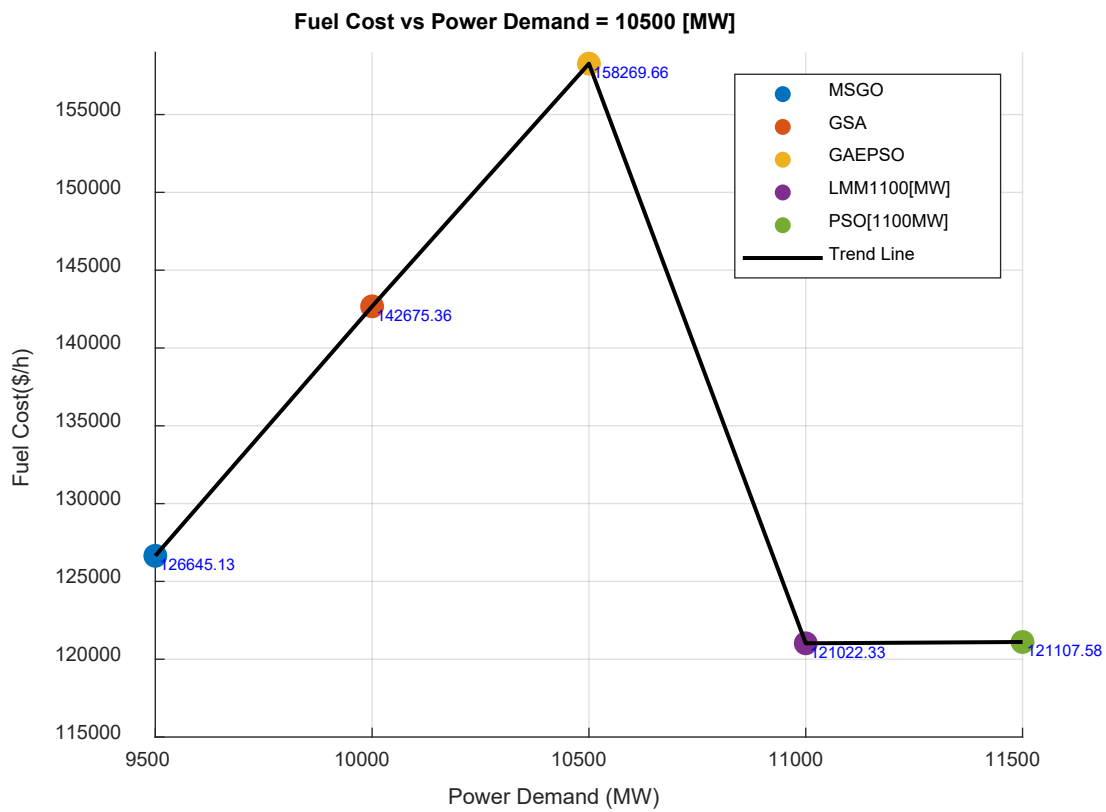


Figure 4.7: Values of fuel cost and power demand for the WTEED problem using the PSO algorithm applied to a 40-unit system

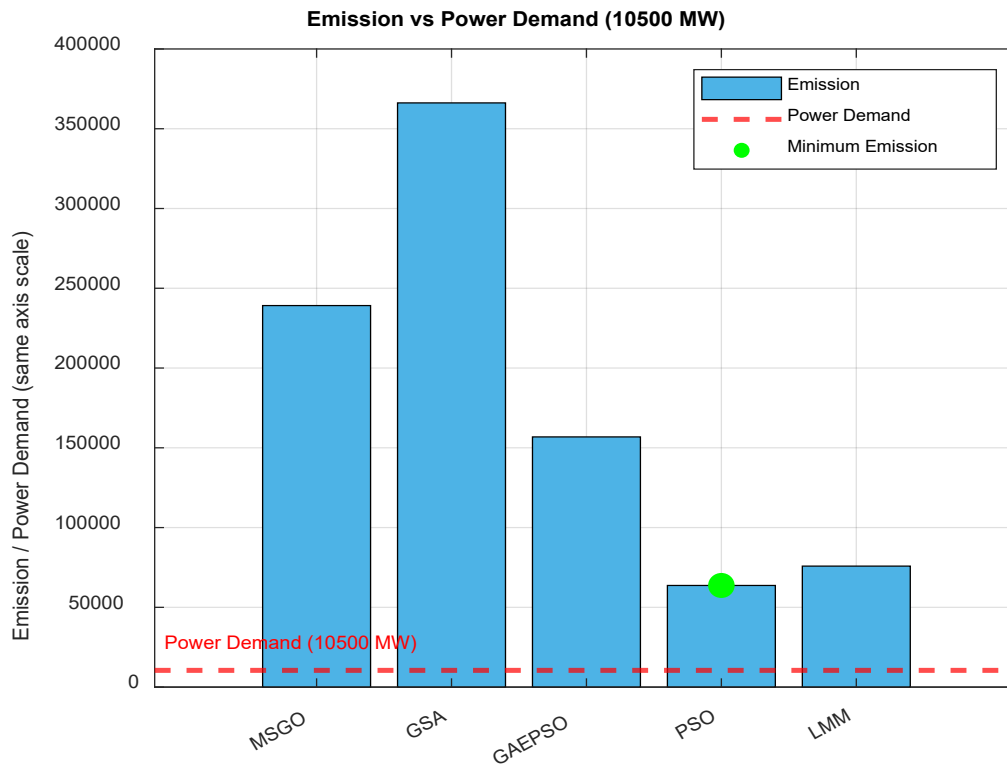


Figure 4.8: Values of fuel cost and emission for the WTEED problem using the PSO algorithm applied to a 40-unit system

4.5. Conclusion

In this chapter, a wind-thermal economic emission dispatch problem is successfully solved using the PSO method. Fuel and emission costs are minimised in the bi-objective problem of economic emission dispatch optimisation. This chapter presents the transmission line losses, emissions, and inequality limits. Three test systems, 6-unit, 10-unit, and 40-unit, are employed to evaluate the efficiency of the algorithm. Compared to other algorithms, the fuel cost and emissions for 6-unit systems are 1-3% and 1-2.8% lower, respectively. Additionally, compared with previous optimisation techniques, the 10-unit system's fuel cost and emissions are 1-3% and 1-2%, respectively. Lastly, fuel consumption and emissions for the bigger system have significantly decreased by 1-2% and 1-22%, respectively.

Lagrange's technique, which is described in Chapter 3, is compared with the developed PSO solution. Tables 4.2, 4.4, and 4.6 illustrate the fuel cost and emissions produced by the PSO algorithm compared with various alternative approaches. The number of particles in the swarm and the initial choice of the Lagrangian variable (λ) determine the PSO and Lagrange's solutions. It concludes that the PSO algorithm provides a near-global solution independent of the swarm size, whereas Lagrange's method yields a global solution independent of the initial λ .

It can be seen that the generation of random variables in each optimal solution has a significant impact on the solution to the WTEED problem across all test systems. The swarm population, iteration, solution weight, and constants c_1 and c_2 need to be carefully chosen. The 6-unit, 10-unit, and 40-unit models have the following computational times of 15.235862s, 7.024024s, and 10.978005s, respectively. In contrast, the best values for fuel cost, emissions, and total generation in the WTEED problem for the 6-unit, 10-unit, and 40-unit systems are within the expected values reported in the literature.

Based on the results described in Chapters 3 and 4, several calculations and simulations are required to thoroughly study the developed methods and their applications. The investigation will be further extended to a multi-area system in which the solution of the WTEED problem is distributed across subsystems, with a two-level hierarchical structure. In this decomposition, each area is treated as a separate problem. Since this can lead to high computational cost, future work beyond this thesis could use parallel computing within the MATLAB environment to solve the WTEED problem.

CHAPTER FIVE

MULTI-AREA WIND-THERMAL ECONOMIC EMISSION DISPATCH(MAWTEED) PROBLEM USING LAGRANGE MULTIPLIER METHOD(LMM)

5.1 Introduction

A Multi-Area Wind–Thermal Economic Emission Dispatch (MAWTEED) problem is addressed using the Lagrange multiplier approach. This optimisation is formulated as a multi-objective problem that reduces fuel cost and emissions. The inequality, quality limits, pollutants, transmission line loss, and tie-line power between areas are considered. To assess performance, the algorithm is tested on three benchmark systems: a 6-unit system with two areas, a 12-unit system with four areas, and a 40-unit system with two areas. For the 6-unit system, the fuel cost is 1-5% lower than that of other algorithms; for the 12-unit system, the fuel cost and emissions are 1-6% and 1-14% lower than those of other optimisation algorithms; and for the 40-unit system, there is a very significant reductions in fuel use by 1% and emissions by approximately 1-20%.

It appears that the Lagrange optimisation approach efficiently converges to an optimal solution by determining the best initial values of the lambda parameters across all test systems. In contrast, the optimum values for fuel cost, emissions, and total generation in the MAWTEED problem for the 6-unit, 12-unit, and 40-unit systems are within the predicted values published in the literature. Compared to heuristic methods documented in the literature, the conventional Lagrange employing decomposition coordination can easily produce optimal results for fuel and emission reduction. Lagrange's classical techniques are effective and precise for straightforward convex optimisation problems.

This chapter is further structured as follows. The problem formulation appears in Section 5.2; the development of Lagrange's decomposition coordinating method for solving the MAWTEED problem is discussed in Section 5.3, the algorithm of the Lagrange decomposition-coordinating method for solving the MAWTEED problem is presented in Section 5.4, various case studies used for multi-area WTEED problem solutions are provided in Section 5.5, and ultimately, the conclusion.

5.2 Multi-area wind-thermal economic emission dispatch problem formulation

The Multi-Area Wind-Thermal Dynamic Economic Dispatch (MAWTDEED) aims to minimise power transferred between generation areas, reduce emissions from thermal units, and control the power outputs of thermal and wind generating plants across multiple areas. This can be expressed mathematically as(Alli, 2024; Ghasemi et al., 2016; Hetzer et al., 2008; Ming Chen & Wang, 2010; Secui, 2015).

$$\text{Min } F_C = \sum_{m=1}^M \sum_{n=1}^{N_m} C_{mn}(P_{Gmn}) + C_{wmn}(P_{wmn}) \quad [\$/\text{h}] \quad (5.1)$$

Where, the number of online generators for the area m in an M area generation units denoted by n is. $C_{wmn}(P_{wmn})$ is the amount of power that the wind turbine units produce.

The MAWTEED problem can be expressed mathematically as follows:

In order for equation 5.2 to provide the operation cost for thermal generators, find the vectors of the real power P and the power transmitted over the tie lines P_T .

$$F_C(P_{mn}) = \sum_{n=1}^M \sum_{n=1}^{N_m} (a_{mn}P_{Gmn}^2 + b_{mn}P_{Gmn} + c_{mn}) \quad (5.2)$$

Where,

M Quantity of interconnected areas

N_m The quantity of generators that are part of the producing power area in area m

a_{mn}, b_{mn}, c_{mn} Price coefficient of the n^{th} generator in the m^{th} area

P_{Gmn} Real power formed by the n^{th} generator in the m^{th} area

$P_{mn} = [P_{Gm1} P_{Gm2} P_{Gm3} P_{Gm4} \dots \dots P_{wm1} P_{wm2} P_{wm3} P_{wmN_m}]$ vector of an absolute power generated in the m^{th} area and $m = \overline{1, M}$

$P = [P_1 P_2 P_3 \dots \dots P_M]^T$ Vector of the actual power generated throughout the entire power system

Equation (5.3) determines the operational cost for electricity being transmitted via the tie-lines.

$$F_T(P_T) = \sum_{m=1}^M \sum_{\substack{j=1 \\ j \neq m}}^M (q_{mj}P_{Tmj} + q_{jm}P_{Tjm}) \quad (5.3)$$

Where q_{mj} is the transmission coefficient for the cost of power transmission from area m to area j , and P_{Tmj} is the tie line power flow from area m to area j .

$P_{Tm} = [P_{Tm,m+1} P_{Tm,m+2} P_{Tm,m+3} \dots \dots P_{Tm,M}]^T$, $m = \overline{1, M-1}$ Power transfer vector between the m^{th} area and every other area.

$P = [P_{T1} P_{T2} P_{T3} \dots \dots P_{T,M-1}]^T$ Power transmission vector between all areas.

Equations (5.1), (5.2), and (5.3) are to be minimized, subject to the following limitations.

a) Lower and higher active power produced for every generator

$$P_{Gmn,\min} \leq P_{Gmn} \leq P_{Gmn,\max}, m = \overline{1, M}, n = \overline{1, N_m}$$

$$0 \leq P_{wmn} \leq P_{wmn,\text{rated}}, m = \overline{1, M}, n = \overline{1, N_m}$$

Where, $P_{Gmn,min}$ and $P_{Gmn,max}$ The lowest and highest power that can be produced by the n^{th} generator in the m^{th} area. $P_{wmn,rated}$ is the rated wind power produced by the wind power system.

b) Lowest and highest active power sent through the tie lines.

$P_{Tmj,min} \leq P_{Tmj} \leq P_{Tmj,max}$. These limits apply to both power flow directions and can be expressed as follows:

$$P_{Tmin} \leq P_{Tmj} \leq P_{Tmax}, m = \overline{1, M}, j = \overline{1, M}, j \neq m, \quad (5.4)$$

$$P_{Tmin} \leq P_{Tjm} \leq P_{Tmax}, m = \overline{1, M}, j = \overline{1, M}, j \neq m$$

Power balance constraints.

Equation (5.5) below provides the balance between production and power demand for the m^{th} area and the whole system.

$$\sum_{n=1}^{N_m} P_{mn} = P_{Dmn} + P_{Lmn} + \sum_{\substack{m=1 \\ m \neq k}}^M [P_{Tmj} - (1 - \rho_{jm}) \times P_{Tjm}], m = \overline{1, M}, \quad (5.5)$$

The output power from both thermal and wind generators is represented in this instance by P_{mn} . Equation (5.6) provides the wind output power.

$$W_{j,k}(P_{w_{j,k}}) = \phi_{D_{j,k}} P_{E_{j,k}} + \phi_{OE_{j,k}} \times (P_{A_{j,k}} - P_{E_{j,k}}) + \phi_{UE_{j,k}} \times (P_{E_{j,k}} - P_{A_{j,k}}) \quad [$/h] \quad (5.6)$$

Where

$P_{E_{j,k}}$ Estimated wind power output of the turbine j in a wind farm k [MW]

$P_{A_{j,k}}$ Accessible wind power output of the turbine j in wind farm k [MW]

$\phi_{D_{j,k}}$ Direct cost coefficient of the turbine j in wind farm k [\$/MWh]

$\phi_{OE_{j,k}}$ Overestimation cost coefficient of the turbine j in wind farm k [\$/MWh]

$\phi_{UE_{j,k}}$ Underestimation cost coefficient of the turbine j in wind farm k [\$/MWh]

Where,

$$P_{Lm} = \sum_{n=1}^{N_m} \sum_{r=1}^{N_m} (P_{mn} B_{mnr} P_{mr}) + \sum_{n=1}^{N_m} (B_{0n} P_{mn} + B_{m00}), m = \overline{1, M}, \quad (5.7)$$

$$\sum_{n=1}^{N_m} P_{mn} = P_{Dm} + \sum_{n=1}^{N_m} \sum_{r=1}^{N_m} (P_{mn} B_{mnr} P_{mr}) + \sum_{n=1}^{N_m} (B_{0n} P_{mn} + B_{m00}), + \quad (5.8)$$

$$+ \sum_{\substack{m=1 \\ m \neq k}}^M [P_{Tmj} - (1 - \rho_{jm}) \times P_{Tjm}], m = \overline{1, M},$$

Where, B_{mnr} , B_{0n} , B_{m00} , are the integrated power system transmission loss coefficients., ρ_{jm} is the fractional loss rate from area j to area m , P_{Tmj} and P_{Tjm} are a power flow from area m to area j and area j to area m . Pollutant minimisation is also considered. The mathematical expression can be given as follows.

$$F_e = \sum_{n=1}^M \sum_{n=1}^{N_m} (d_{mn} P_{mn}^2 + e_{mn} P_{mn} + f_{mn}) \quad (5.9)$$

d_{mn}, e_{mn}, f_{mn} Pollutants coefficients of the n^{th} generator in the m^{th} area. Equation (5.9b) provides the multi-area combined economic emission dispatch fuel cost.

$$F_T = \sum_{n=1}^M \sum_{n=1}^{N_m} (a_{mn} P_{mn}^2 + b_{mn} P_{mn} + c_{mn}) + h_{mn} (d_{mn} P_{mn}^2 + e_{mn} P_{mn} + f_{mn}) \quad (5.9b)$$

5.3 Solution of the MAWTEED problem using Lagrange's decomposition coordinating method.

This section presents a Lagrange decomposition-coordinating technique for solving the multi-area wind-thermal economic emission dispatch problem. The method's development is based on the Lagrange functional for the multi-area economic dispatch problem. The following describes how the Lagrange functional is constructed:

$$L = \left\{ \sum_{n=1}^M \sum_{n=1}^{N_m} (a_{mn} P_{mn}^2 + b_{mn} P_{mn} + c_{mn}) + h_{mn} (d_{mn} P_{mn}^2 + e_{mn} P_{mn} + f_{mn}) + \sum_{m=1}^M \sum_{\substack{j=1 \\ j \neq m}}^M (q_{mj} P_{Tmj} + q_{jm} P_{Tjm}) + \sum_{m=1}^M \left\{ \lambda_m \left(-\sum_{n=1}^{N_m} P_{mn} + P_{Dm} + \sum_{n=1}^{N_m} \sum_{r=1}^{N_m} (P_{mn} B_{mnr} P_{mr}) + \sum_{n=1}^{N_m} (B_{0n} P_{mn} + B_{m00}), + \sum_{m=1}^M [P_{Tmj} - (1 - \rho_{jm}) \times P_{Tjm}] \right) \right\} \right\} \quad (5.10)$$

Where $\lambda = (\lambda_1, \lambda_2, \lambda_3 \dots \lambda_M)$, are vectors of Lagrange multipliers, and h_{mn} is the price penalty factor for every area. It is essential to determine the values of P_{mn}, P_{Tmj}, P_{Tjm} and λ such that the Lagrange functional has an optimum value according to P_{mn}, P_{Tmj}, P_{Tjm} , and the maximum according to λ under the following limits.

$$P_{mn,min} \leq P_{mn} \leq P_{mn,max}, m = \overline{1, M}, n = \overline{1, N_m} \quad (5.11)$$

$$0 \leq P_{wmn} \leq P_{wmn,rated}, m = \overline{1, M}, n = \overline{1, N_m} \quad (5.12)$$

$$P_{Tmin} \leq P_{Tmj} \leq P_{Tmax}, m = \overline{1, M}, j = \overline{1, M}, j \neq m, \quad (5.13)$$

$$P_{Tmin} \leq P_{Tjm} \leq P_{Tmax}, m = \overline{1, M}, j = \overline{1, M}, j \neq m \quad (5.14)$$

The following requirements for optimality are employed to determine the optimal solution:

$$\frac{\partial L}{\partial P_{mn}} = 2a_{mn} P_{mn} + b_{mn} + h_{mn} (2d_{mn} P_{mn} + e_{mn}) + \lambda_m (2 \sum_{r=1}^{N_m} B_{mnr} P_{mr} + B_{m0n} - 1) = 0 \quad m = \overline{1, M}, n = \overline{1, N_m} \quad (5.15)$$

$$\frac{\partial L}{\partial P_{Tmj}} = q_{mj} + \lambda_m = 0 = e_{pTmj}, m = \overline{1, M}, j = \overline{1, M}, j \neq m \quad (5.16)$$

$$\frac{\partial L}{\partial P_{Tjm}} = q_{jm} - \lambda_m(1 - \rho_{jm}) = 0 = e_{pTjm}, m = \overline{1, M}, j = \overline{1, M}, j \neq m \quad (5.17)$$

$$\begin{aligned} \frac{\partial L}{\partial \lambda_m} = & -\sum_{n=1}^{N_m} P_{mn} + P_{Dm} + \sum_{n=1}^{N_m} \sum_{r=1}^{N_m} (P_{mn} B_{mnr} P_{mr}) + \sum_{n=1}^{N_m} (B_{0n} P_{mn} + B_{m00}), + \\ & \sum_{m \neq j}^M [P_{Tmj} - (1 - \rho_{jm}) \times P_{Tjm}], m = \overline{1, M}, j = \overline{1, M}, j \neq m \end{aligned} \quad (5.18)$$

The solution to the above system of equations (5.15-5.18) can be obtained in parallel using a decomposition method based on the selection of coordinating variables. These are selected to be $\lambda_m, m = \overline{1, M}$. In a two-level structure, a coordinator provides the following values for the coordinating variables:

$$\lambda_m = \lambda_m^l, m = \overline{1, M}, \quad (5.19)$$

Where l is the index of iterations. Equations (5.16) through (5.18) must be solved on the second level of the calculation framework, but equation (5.15) can be solved on the first level. The following method can be used to solve equation (5.15).

$$\begin{aligned} \frac{\partial L}{\partial P_{mn}} = & 2a_{mn}P_{mn} + b_{mn} + h_{mn}(2d_{mn}P_{mn} + e_{mn}) + \lambda_m(2 \sum_{r=1}^{N_m} B_{mnr}P_{mr} + B_{m0n} - 1) = \\ & 0, m = \overline{1, M}, n = \overline{1, N_m} \end{aligned} \quad (5.20)$$

Solution of equation 5.20 by multiplying by $1/2\lambda_m$ be

$$\begin{aligned} \left(\frac{a_{mn} + h_{mn}d_{mn}}{\lambda_m} \right) P_{mn} + \sum_{r=1}^{N_m} B_{mnr} P_{mr} = \frac{1}{2} \left(1 - \frac{b_{mn} + h_{mn}e_{mn}}{\lambda_m} - B_{m0n} \right), \\ m = \overline{1, M}, n = \overline{1, N_m} \end{aligned} \quad (5.21)$$

This can also be expressed in matrix form as:

$$\begin{aligned} \begin{bmatrix} \frac{a_{m1} + h_{m1}d_{m1}}{\lambda_m} + B_{m11} & B_{m12} & B_{mN_m1} \\ B_{m21} & \frac{a_{m2} + h_{m2}d_{m2}}{\lambda_m} + B_{m22} & B_{m2N_m} \\ B_{mN_m1} & B_{mN_m1} & \frac{a_{mN_m} + h_{mN_m}d_{mN_m}}{\lambda_m} + B_{mN_mN_m} \end{bmatrix} \begin{bmatrix} P_{m1} \\ P_{m2} \\ P_{m3} \\ \vdots \\ P_{mN_m} \end{bmatrix} = \\ \frac{1}{2} \begin{bmatrix} \left[1 - \left(\frac{b_{m1} + h_{m1}e_{m1}}{\lambda_m} \right) - B_{m01} \right] \\ \left[1 - \left(\frac{b_{m1} + h_{m1}e_{m1}}{\lambda_m} \right) - B_{m02} \right] \\ \left[1 - \left(\frac{b_{m1} + h_{m1}e_{m1}}{\lambda_m} \right) - B_{m0N_m} \right] \end{bmatrix}, m = \overline{1, M} \end{aligned} \quad (5.22)$$

The following straightforward matrix form can be used to express equation (5.22).

$$E_m P_m = D_m, m = \overline{1, M} \quad (5.23)$$

With a known value of $\lambda_m, m = \overline{1, M}$. The solution for the active power of the m^{th} area is given by

$$P_m = E_m \setminus D_m \quad (5.24)$$

The solutions of equations (5.16) and (5.17) can be found using the gradient procedure in the following way:

a) Initial values of $P_{Tmj}^{q_m}$ and $P_{Tjm}^{q_m}$ are estimated, $q_m = 1, q_m = \overline{1, k_m}$
 $P_{Tmj} = P_{Tmj}^{q_m}$ and $P_{Tjm} = P_{Tjm}^{q_m}$, where q_m is the index of the gradient process in the m^{th} area.

(b) The amended values of the tie lines' power are:

$$P_{Tmj}^{q_m+1} = P_{Tmj}^{q_m} - \alpha_{Tmj} e_{PTmj}^{q_m}, \text{ where } e_{PTmj}^{q_m} \text{ is given in equation (5.16), } m = \overline{1, M} \quad (5.25)$$

$$P_{Tjm}^{q_m+1} = P_{Tjm}^{q_m} - \alpha_{Tjm} e_{PTjm}^{q_m} \text{ where } e_{PTjm}^{q_m} \text{ is given in equation (5.17), } m = \overline{1, M}. \quad (5.26)$$

The solution is checked against the error constraints.

$e_{PTmj}^{q_m} \leq \varepsilon_1$ and $e_{PTjm}^{q_m} \leq \varepsilon_2$ where ε_1 and ε_2 , They are tiny positive numbers.

Solutions of equations (5.24), (5.25), and (5.26) depend on $\lambda_m, m = \overline{1, M}$. When the value of lambda is attained, the optimal values of P_{mn}, P_{Tmj} and P_{Tjm} are found.

A gradient technique is utilised to compute the optimal value of $\lambda_m, m = \overline{1, M}$, using the following form:

$$\lambda_m^{l+1} = \lambda_m^l + \alpha_{m\lambda} e_{m\lambda}, m = \overline{1, M}, \quad (5.27)$$

Where the steps of the gradient procedure are represented by $\alpha_{m\lambda}$. The gradient on the second level halts when $e_{\lambda} \leq \varepsilon_3, \varepsilon_3 \geq 0$. The two-level solution structure for MAWTEED is shown in Figure 5.1 below.

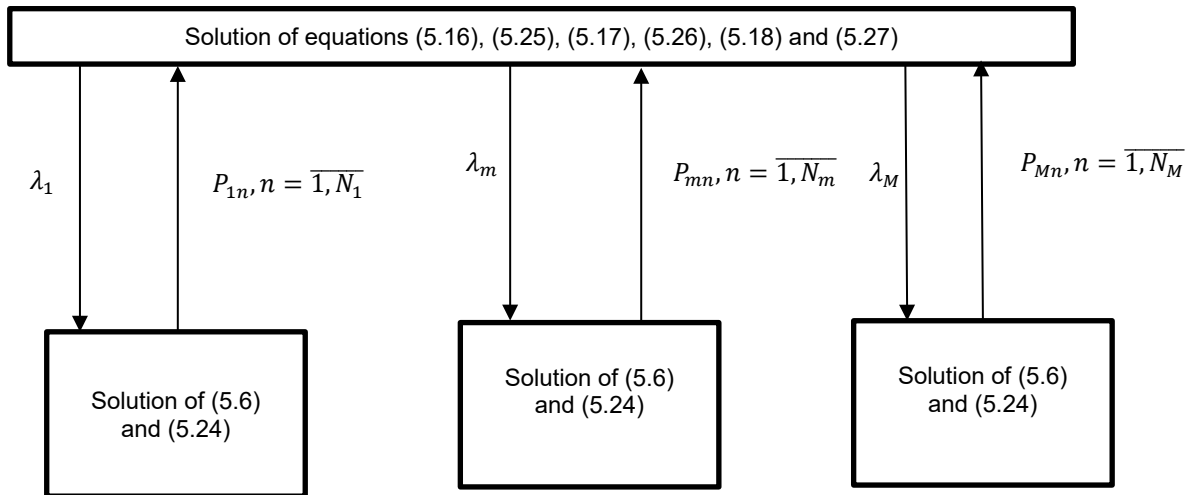


Figure 5.1: Lagrange decomposition coordinating algorithm for the solution of the MAWTEED problem in two level structure

5.4 Algorithm of the Lagrange decomposition-coordinating method for calculation of the MAWTEED problem.

Step 1. The number of iterations of the first and second levels is set, and all coefficient values are supplied $k_m, m = \overline{1, M}$.

Step 2. Start values of the coordinating variables $\lambda_m^l, m = \overline{1, M}$, are guessed.

Step 3. Beginning values of the tie lines are estimated. $P_{Tmj}^{k_m}, P_{Tjm}^{k_m}, m = \overline{1, M}, j \neq m$

Step 4. Computation on the first level is complete for every subsystem, $m = \overline{1, M}$, using equation (5.24).

Step 5. The solution of the first level $P_{mn}^l, m = \overline{1, M}, n = \overline{1, N_m}$ are verified against the limits (5.11) and (5.12) and are sent to the second level.

Step 6. On the second level

(i) Equations (5.16) and (5.25)

(ii) Equations (5.17) and (5.26)

The gradient technique stops when this condition $e_{PTmj} \leq \varepsilon_1$, and $e_{PTjm} \leq \varepsilon_2$ is achieved or the highest number of iterations $k_m, m = \overline{1, M}$, is attained.

The solution of the second level P_{Tmj}^l and $P_{Tjm}^l, m = \overline{1, M}, j = \overline{1, M}, j \neq m$ are verified under the conditions (5.13) and (5.14)

Step 7. Equations (5.18) and (5.27) are established. When the epsilon requirements are met, the gradient process ends. The related optimal solutions of the first-level problems are obtained along with the optimal value for $\lambda_m, m = \overline{1, M}$. In the aforementioned approach, the optimal solution of the MAWTEED sub-problems in the m^{th} region is obtained by performing the maximum number of iterations for one step of the gradient procedure for the optimization of λ_m , on the second level k_m . Each area may have a distinct value for k_m .

5.5 Studies of the multi-area MAWTEED problem solutions

Three benchmark models for multi-area power systems are used to test the proposed algorithm:

- (i) Two areas with 6-unit generators and three thermal generating units in each area, including the transmission line losses, tie-line power transfer between areas, and wind power of 330MW injected in area 1.

- (ii) Four areas with 3 generators in each area, including the transmission line losses, and 330MW of wind power from three wind farms supplying 110MW each.
- (iii) Two areas with 20 generating units in each area, and a wind farm of 330MW, applied in area 1.

The three benchmark representations are implemented for the two considered scenarios:

- (a) The entire power system is divided into multiple sections due to tie-line constraints.

Figure 5.2 illustrates the flowchart for Lagrange's decomposition-coordinating technique employed to determine the MAWTEED problem.

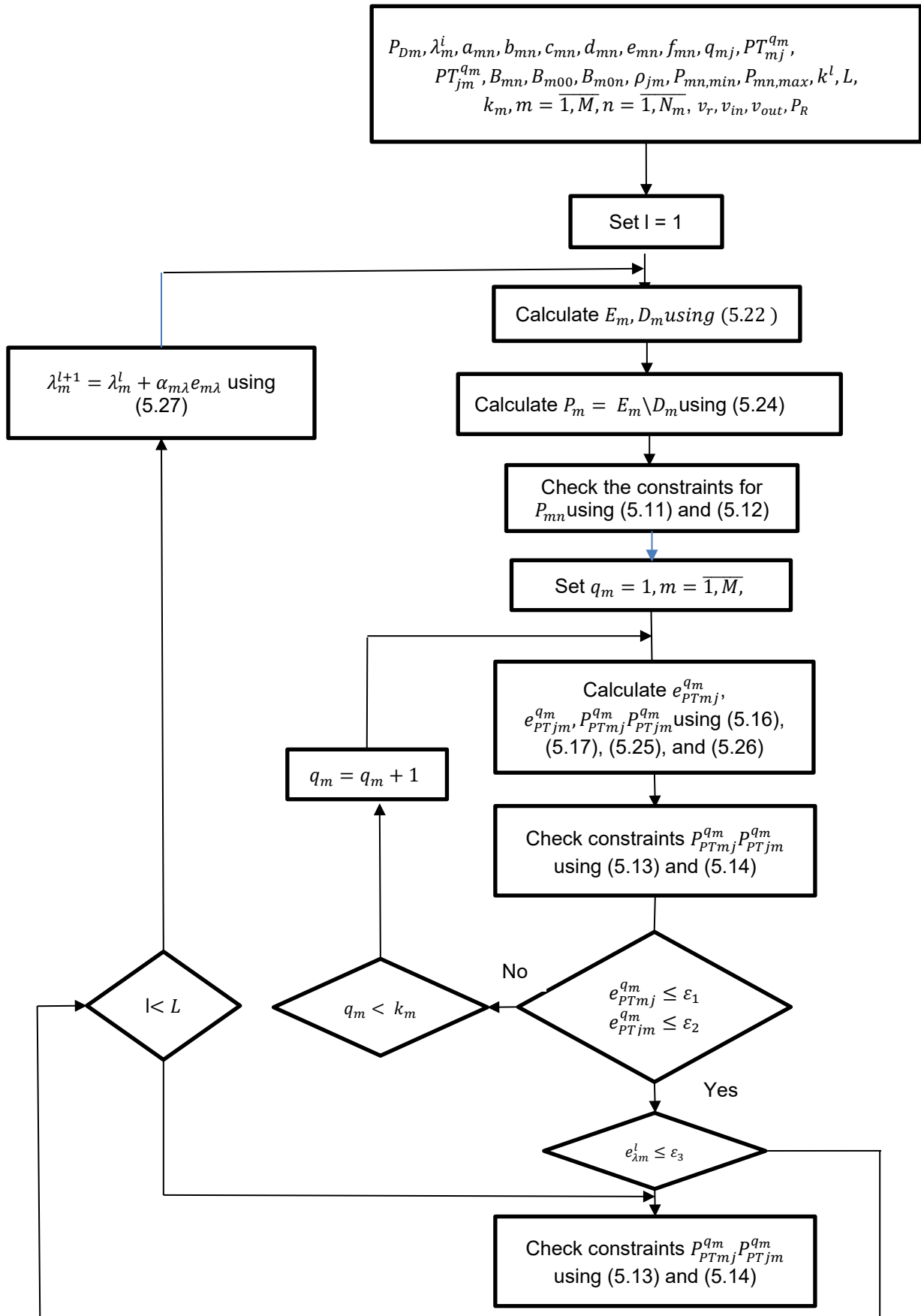


Figure 5.2: Lagrange's decomposition-coordinating algorithm flowchart for solving the MAWTEED problem

5.5.1 Test system I: IEEE30 bus system using 6-units

The test case consists of two areas with six thermal units, each with three generators. The Three-wind Park network that supplies wind power of 110MW each to the entire dispatch problem(Alli, 2024). The total power demand is 1263 [MW]. The area demand is 60% for area 1, and 40% for area 2. The demand for area 1 is 757.8 MW, and for area 2, 505.2MW. The data for the fuel cost is taken from (Basu, 2013) and B-loss coefficients (Krishnamurthy & Tzoneva, 2012). Various power demand values are presented in Table 5.1 to experiment with the system's behaviour to changes in power demand. The MATLAB script file is called MAWTEED_case6units.m, and the software is provided in Appendix C1.

Table 5.1: The MAWTEED problem using the Lagrange multiplier method with various power demands

PD[MW]	600	700	800	900	1000	1263
P1,1[MW]	50	50	100	160.7681	214.8556	232.7670
P1,2[MW]	50	50	50	97.5242	114.5397	120.1745
P1,3[MW]	50	50	50	81.2430	92.8587	96.7054
P2,1[MW]	91.8718	91.9027	143.2658	131.9209	131.9208	238.7650
P2,2[MW]	72.5071	72.5274	106.3055	98.8447	98.8447	169.1088
P2,3[MW]	63.0326	63.0426	79.7222	76.0380	76.0380	110.7344
Pw[MW]	292.4709	239.2799	304.3865	262.216	282.4045	313.9185
PL[MW]	3.6383	3.6393	5.7538	8.5456	11.4528	19.1629
F _c [\$/h]	5256.8085	5257.3266	6129.7873	7047.359	7716.0091	9819.9287
E _T [Kg/h]	239.2494	239.2799	313.2204	378.9017	499.4681	830.2617
CEED[Kg/h]	7827.5305	7828.3065	9328.5035	10495.02	11702.766	16427.6875
Computational time(s)						

The solution of the MAWTEED problem is shown in Table 5.1 above. The real power generators (P1,1-P1,3) and (P2,1-P2,3) units represent the thermal generators for area 1 and area 2, wind (Pw) generators represent the wind power generators for all three wind parks in [MW], fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h]. The obtained fuel cost using LMM is compared with Artificial Bee Colony Optimization (ABCO), Differential Evolution (DE), Evolutionary Programming (EP), Real-coded Genetic Algorithm (RCGA), and Semi-define Programming (SDP)(Basu, 2013), and (Alli, 2024) algorithms reported in the literature, as shown in Table 5.2 below.

Table 5.2: The MAWTEED problem using the Lagrange multiplier method is compared with other optimisation algorithms using PD = 1263[MW]

Reference	(Basu.,2013)				(Alli,2024)	Proposed
Algorithm	ABCO	DE	EP	RCGA	SDP	LMM
P1,1[MW]	500.0000	500.0000	500.0000	500.0000	311.0838	232.7670
P1,2[MW]	200.0000	200.0000	200.0000	200.0000	200.0000	120.1745
P1,3[MW]	149.9997	150.0000	149.9919	149.6328	150.0000	96.7054
P2,1[MW]	204.3358	204.3341	206.4493	205.9398	162.8737	238.7650
P2,2[MW]	154.9954	154.7048	154.8892	155.8322	159.5473	169.1088
P2,3[MW]	67.2915	67.5770	65.2717	65.2209	101.7656	110.7344
Pw [MW]	-	-	-	-	-	313.9185
P _L [MW]	13.6224	13.6159	13.6021	13.6257	-	19.1629
F _c [\$/h]	12255.39	12255.42	12255.43	12256.23	10722	9819.9287
%Deviation of F _c for LMM in relation with the literature	5.51625	5.51631	5.51633	5.51795	2.19568	4.8525 Average
E _T [Kg/h]	-	-	-	-	-	830.2617
CEED[Kg/h]	-	-	-	-	-	16427.6875
Computational time(s)						

Figure 5.3 represents the relationship between fuel cost [\$/h] and power demand [MW] for various optimisation strategies, as described in Table 5.2 above.

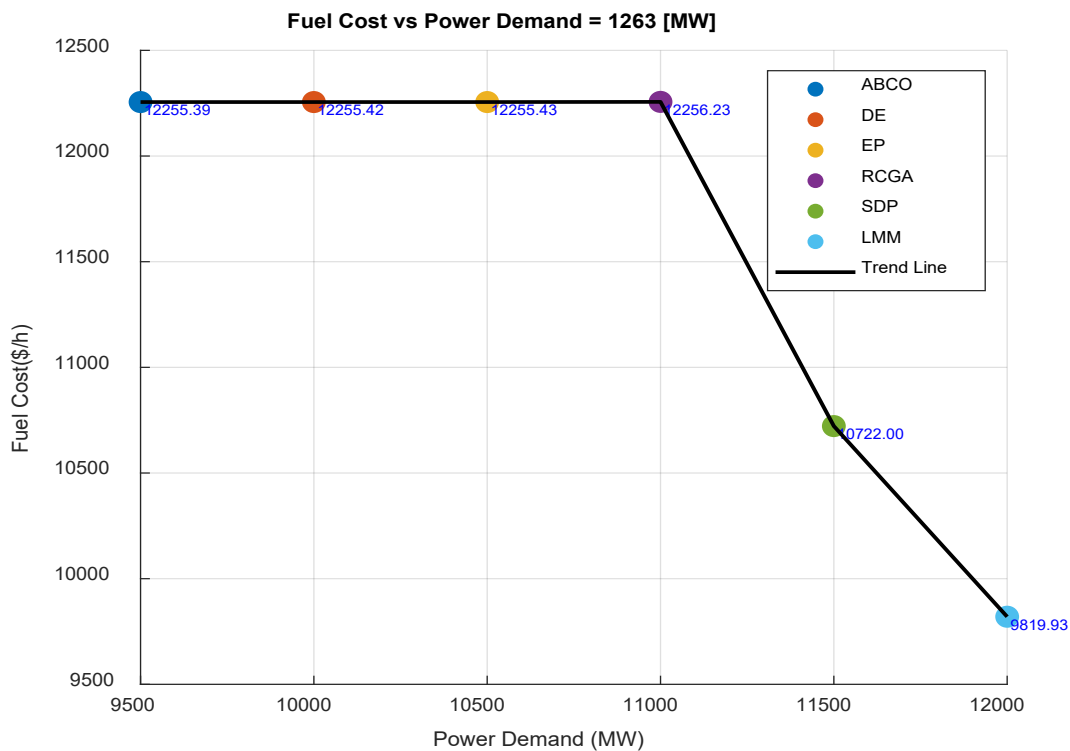


Figure 5.3: Fuel cost versus power demand for different optimisation methods using the LM algorithm for a 6-unit system

5.5.1.1 The MAWTEED problem results and discussion for the 6-Unit System

This system utilises three wind farm networks, which supply 330 [MW] to the power dispatch problem. The following parameters are used for the Lagrange multiplier method. The initial value of lambda is [50 50], the total number of iterations m is 100, the tolerance value epsilon is 0.01, and the tolerance value of delta-lambda epsilon is 0.1. The proposed algorithm for a 6-unit multi-area system is compared with other optimization algorithms in the literature, namely, Artificial Bee Colony Optimization (ABCO), Differential Evolution (DE), Evolutionary Programming (EP), Real-coded Genetic Algorithm (RCGA), and Semi-define Programming (SDP)(Basu, 2013), and (Alli, 2024). The comparison is of the simulation results shown in Table 5.2 above.

The fuel cost results for the ABCO, DE, EP, RCGA, and SDP algorithms are 5.52%, 5.52%, 5.52%, 5.52%, and 2.19%, respectively, compared to the LMM algorithm. When using the LLM algorithm, there is a 1–5% benefit in fuel consumption when wind power is added to the economic emission dispatch as compared to other optimisation algorithms. The optimisation algorithm required only 57 iterations to find the optimal solution to the MAWTEED problem. The optimised value of lambda is [16.8244 24.5375], compared to the initial guess of [50 50].

5.5.2 Test System 2: IEEE30 bus system using 12-unit system

This test system consists of a standard IEEE 30-bus system with four areas, 12 thermal generators (3 in each area), and a three-wind-park network that supplies 110MW of wind power to the entire dispatch problem. The total power demand is 2090 [MW]. The area demand is considered to be 500 [MW] for area 1, 410 [MW] for area 2, 580 [MW] for area 3, and 600 [MW] for area 4. The fuel cost and wind parameters are formed based on the ones stated in (Krishnamurthy et al., 2017) and (Alli, 2024). In Table 5.3, varying power demand is used to test the system's behaviour. The MATLAB script file is called MAWTEED_case12units.m, and the software is accessible in Appendix C2.

Table 5.3: The MAWTEED problem using the LM Method with several power demands for 12-unit generators.

PD[MW]	1500	1600	1700	1800	1900	2090
P1,1[MW]	37.7323	35	89.1836	112.8288	139.8413	87.5974
P1,2[MW]	130.0000	130	141.0986	179.4117	223.0174	138.5237
P1,3[MW]	125.0000	125	135.5624	172.9403	215.4290	133.0488
P2,1[MW]	84.8628	84.5174	80.6747	81.0847	79.5809	86.1913
P2,2[MW]	109.2794	108.8269	103.7930	104.3300	102.3600	110.0000
P2,3[MW]	125.0000	125.0000	125.0000	125.0000	125.0000	125.0000
P3,1[MW]	90.3138	90.3498	87.1977	88.6285	86.1077	146.1331
P3,2[MW]	125.3639	125.4012	122.1359	123.6182	121.0065	182.9771
P3,3[MW]	106.9614	107.0043	103.2550	104.9568	101.9586	173.4331
P4,1[MW]	65.4137	94.2511	90.0618	91.0632	88.7304	141.6098
P4,2[MW]	73.5199	104.8905	100.3432	101.4305	98.8973	156.0605
P4,3[MW]	114.5042	171.0612	162.8729	164.8311	160.2685	262.9685

Pw[MW]	299.0776	317.9222	325.9862	309.0305	307.4669	329.2499
PL[MW]	14.3517	17.8147	18.7403	22.7079	27.4143	33.6248
F _c [\$/h]	69451.7517	76514.9109	77470.6989	82461.9824	86268.2387	106977.016
E _T [Kg/h]	587.7043	646.6456	650.3996	748.8189	877.4164	1120.2618
CEED[Kg/h]	106859.1545	119055.4491	119408.165	128990.227	138137.2521	181987.099

The solution of the MAWTEED problem is shown in Table 5.3 above. The real power generators (P1,1-P1,3), (P2,1-P2,3), (P3,1-P3,3), and (P4,1-P4,3) units represent the thermal generators for area 1, area 2, area 3, and area 4. Wind (Pw) generators represent the wind power generators for all three wind parks in [MW], fuel cost (F_c), total emission (E_T) in [kg/h], and CEED in [Kg/h]. The obtained fuel cost and emission using LMM is compared with Lagrange's Decomposition-Coordinating Method (LDCM), Particle Swarm Optimisation (PSO), and Simplex-Particle Swarm Optimisation (SPSO)(Chopra et al., 2018) Algorithms found in the literature are shown in Table 5.4 below.

Table 5.4: Lagrange multiplier method compared with other optimisation algorithms for MAWTEED problem, PD = 2090[MW]

Algorithm	LDCM	PSO	SPSO	LMM (Krishnamurthy,2011)	Proposed LMM
	(Chopra et al., 2018)				
P1,1[MW]	131.45	160.9	165	182.7879	87.5974
P1,2[MW]	209.49	163.3	260	302.6497	138.5237
P1,3[MW]	202.25	289.4	265	287.4964	133.0488
P2,1[MW]	150	109.6	150	130.5891	86.1913
P2,2[MW]	110	117.1	75	110.0000	110.0000
P2,3[MW]	191.63	184.4	175	147.6606	125.0000
P3,1[MW]	175	171.5	175	142.9309	146.1331
P3,2[MW]	215	197.5	160	181.2219	182.9771
P3,3[MW]	236.38	198.3	280	168.9267	173.4331
P4,1[MW]	164.09	230	175	126.3394	141.6098
P4,2[MW]	180.2	144.8	160	140.9621	156.0605
P4,3[MW]	306.18	211.5	280	236.9631	262.9685
Pw[MW]	-	-	-	-	329.2499
F _c [\$]	144058.2	136598.3	134557.6	125883.5243	106977.016
%Deviation of F _c for LMM in relation with the literature	7.38565	6.08052	5.70945	4.05962	5.80881
PL[MW]	61.82	48.22	43.804	68.5286	33.6248
ET[T]	1923.7	3713.93	1473.935	1684.6603	1120.2618
%Deviation of E _T for LMM in relation to the literature	13.1972	26.8263	6.81662	10.0609	14.2253
CEED[\$/h]	266400.92	277258.2	232500.67	225665.1721	181987.099
%Deviation of CEED for LMM in relation with the literature	9.41303	10.3726	6.09349	5.35727	7.8091

The relationships between fuel cost [\$/h], Emission [Kg/h], and CEED with power demand [MW] are shown graphically in Figures 5.4, 5.5, and 5.6 for different optimisation algorithms.

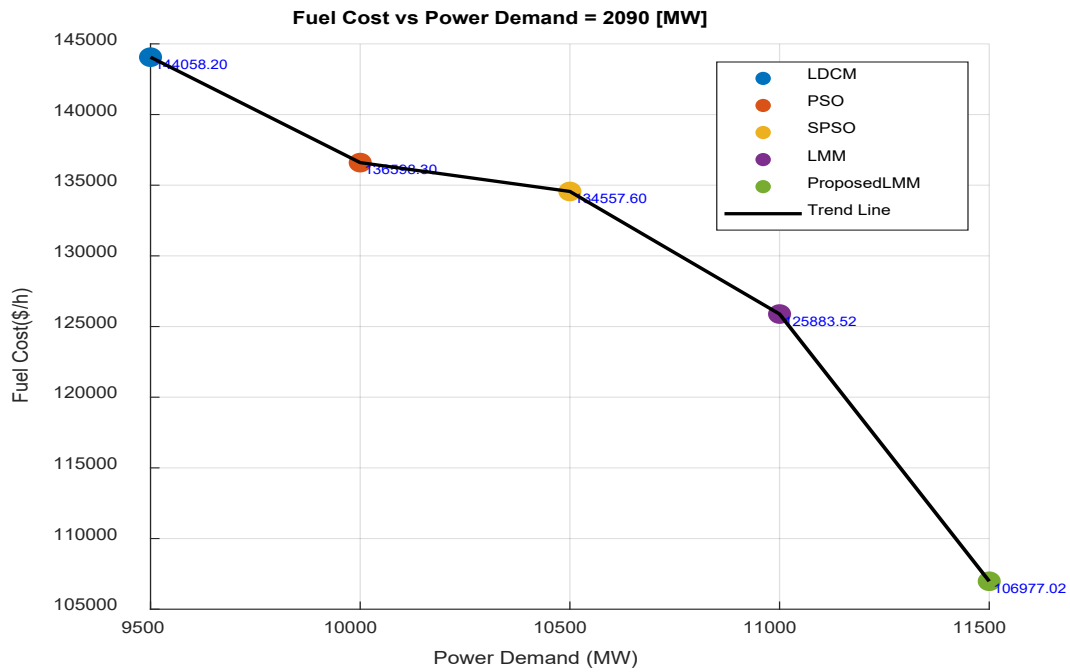


Figure 5.4: Fuel cost versus power demand for different optimisation methods using the LM algorithm for a 12-unit system

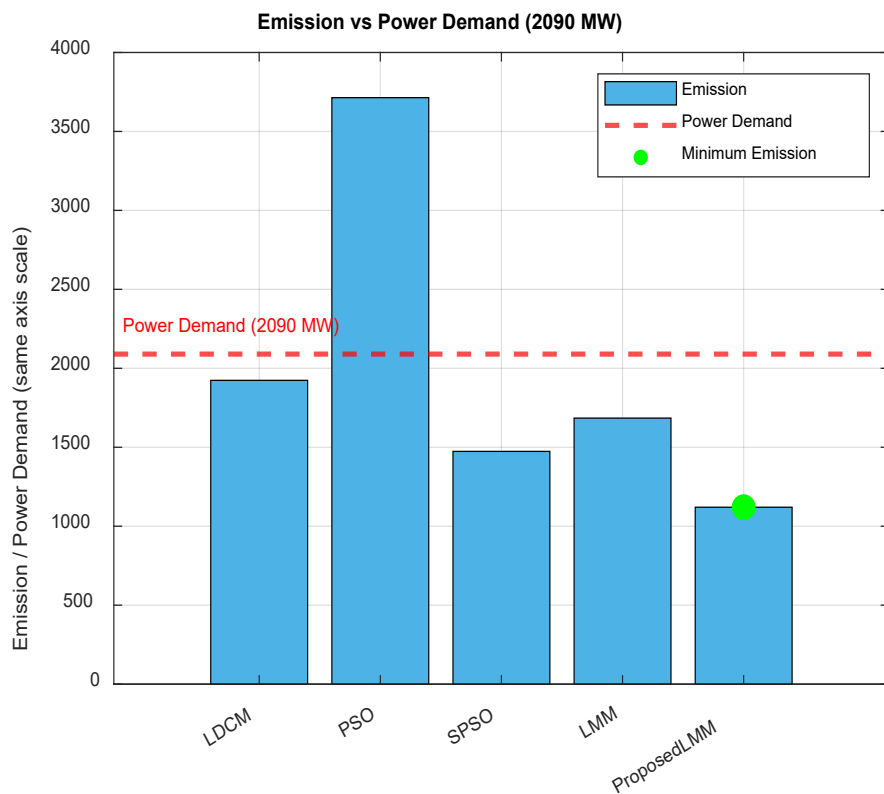


Figure 5.5: Emission versus power demand for different optimisation methods using the LM algorithm for a 12-unit system

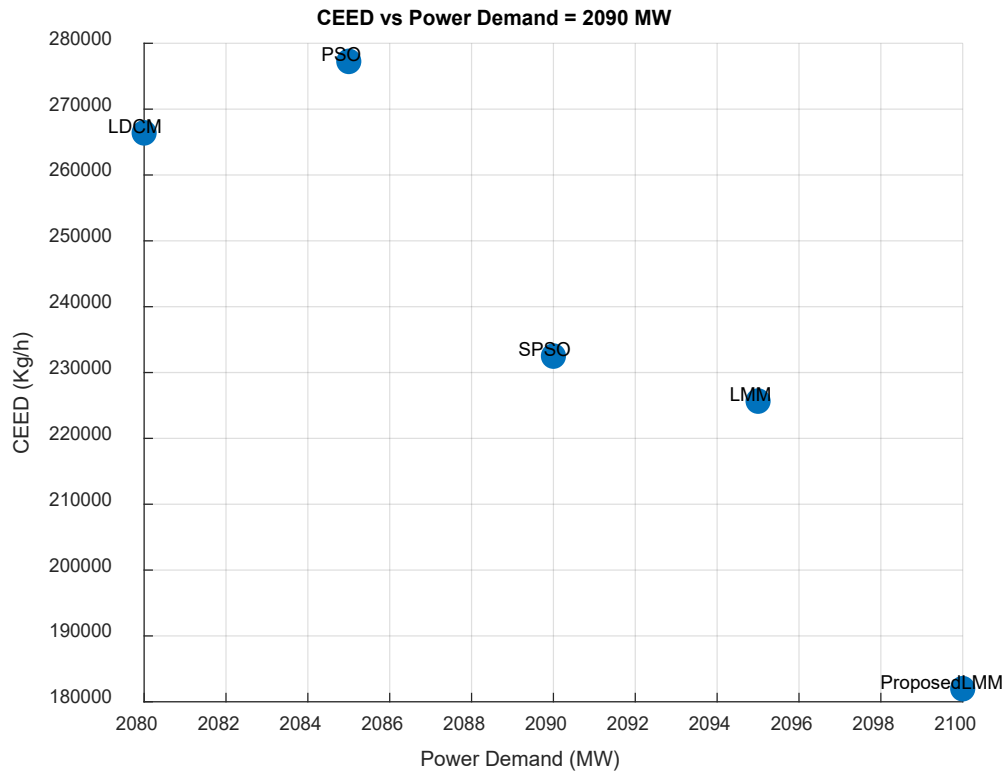


Figure 5.6: CEED versus power demand for different optimisation methods using the LM algorithm for a 12-unit system

5.5.2.1 The MAWTEED problem results, and discussion for the 12-Unit System

The Lagrange method is implemented to solve the multi-area economic emission dispatch problem with wind power, utilizing three wind-farm networks of 110MW each. The following parameters are used for the Lagrange multiplier method. The initial value of lambda is [100 100 100 100], the total number of iterations m is 3000, the tolerance value (epsilon) is 0.01, and the tolerance value of delta-lambda epsilon is 0.1. The Lagrange multiplier method is compared with Lagrange’s Decomposition-Coordinating Method (LDCM), Particle Swarm Optimisation (PSO), and Simplex-Particle Swarm Optimisation (SPSO)(Chopra et al., 2018). The fuel cost results for the LDCM, PSO, SPSO, and LMM algorithms are 7.39%, 6.08%, 5.71%, and 4.06%, respectively, compared to the proposed LMM algorithm. When using the LLM algorithm, there is a 1–6% benefit in fuel consumption when wind power is added to the economic emission dispatch as compared to other optimisation algorithms. The resultant NOx emissions are 13.197%, 26.83%, 6.82%, and 10.06% lower than those of the proposed LM algorithm. The LM method has effectively reduced pollutant levels by 1–14% compared to other optimization algorithms.

The optimization algorithm took 87 iterations to find the optimal solution of the MAWTEED problem. The optimized lambda values are [79.1408, 105.8244, 192.1400, 212.6355], compared to the initial guess of [100, 100, 100, 100]. The proposed

algorithm demonstrates reduced fuel costs and lower emissions, proving to be more effective than all other optimisation algorithms.

5.5.3 Test System 3: IEEE30 bus system using 40 generating units

The MAWTEED problem is solved using the Lagrange algorithm on a standard IEEE 30-bus two-area system with 40 thermal generators (20 in each area) and a three-wind park network supplying 110MW each to the entire dispatch problem. The total power demand is considered as 10500MW. The area demand is considered as 7500 MW for area 1 and 3000 MW for area 2, respectively. The fuel cost and wind parameters are formed based on the ones reported in (Krishnamurthy & Tzoneva, 2016) and (Alli, 2024) and are shown in Tables 5.5 and 5.6.

Table 5.5: Wind-speed data

v_{in} Cut-in wind speed	v_r Rated wind-speed	v_o Cut-out wind speed	w_r Rated Power	C_{pw} Underestimation	C_{rw} Overestimation	d_w direct cost
5	15	45.	330	5	5	0

Table 5.6: IEEE 30 Bus System data for 40 thermal systems

Generating Unit [MW]	Generator Limits		Fuel cost coefficients			Emission coefficients		
	P_{min}	P_{max}	a_i [\$/ (MWh) ²]	b_i [\$/MWh]	c_i [\$/h]	α_i [t/(MWh) ²]	β_i [t/MWh]	γ_i [t/h]
1	36	114	0.0069	6.73	94.705	0.048	-2.22	60
2	36	114	0.0069	6.73	94.705	0.048	-2.22	60
3	60	120	0.02028	7.07	309.54	0.0762	-2.36	100
4	80	190	0.00942	8.18	369.03	0.054	-3.14	120
5	47	97	0.0114	5.35	148.89	0.085	-1.89	50
6	68	140	0.01142	8.05	222.33	0.0854	-3.08	80
7	110	300	0.00357	8.03	287.71	0.0242	-3.06	100
8	135	300	0.00492	6.99	391.98	0.031	-2.32	130
9	135	300	0.00573	6.6	455.76	0.0335	-2.11	150
10	130	300	0.00605	12.9	722.82	0.425	-4.34	280
11	94	375	0.00515	12.9	635.2	0.0322	-4.34	220
12	94	375	0.00569	12.8	654.69	0.0338	-4.28	225
13	125	500	0.00421	12.5	913.4	0.0296	-4.18	300
14	125	500	0.00752	8.84	1760.4	0.0512	-3.34	520
15	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
16	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
17	220	500	0.00313	7.97	647.85	0.0151	-2.68	220
18	220	500	0.00313	7.95	649.69	0.0151	-2.66	222
19	242	550	0.00313	7.97	647.83	0.0151	-2.68	220
20	242	550	0.00313	7.97	647.81	0.0151	-2.68	220
21	254	550	0.00298	6.63	785.96	0.0145	-2.22	290
22	254	550	0.00298	6.63	785.96	0.0145	-2.22	285
23	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
24	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
25	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
26	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
27	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
28	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
29	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
30	47	97	0.0114	5.35	148.89	0.085	-1.89	50
31	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
32	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
33	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
34	90	200	0.0001	8.95	107.87	0.0012	-3.48	65
35	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
36	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
37	25	110	0.0161	5.88	307.45	0.095	-1.98	100
38	25	110	0.0161	5.88	307.45	0.095	-1.98	100
39	25	110	0.0161	5.88	307.45	0.095	-1.98	100
40	242	550	0.00313	7.97	647.83	0.0151	-2.68	220

Varying power demand is used to test the system's behaviour, as shown in Table 5.7. The software is in Appendix C3, with the MATLAB script file named MAWTEED_case40units.m. The real power generators (P1,1-P1,20) units represent the thermal generators for area 1, generators from (P2,1-2,20) represent generators for area 2, and wind (Pw) generators represent wind power generators, all in [MW], fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h].

Table 5.7: The MAWTEED problem using the Lagrange multiplier method with various power demands for a 40-unit system

PD[MW]	8000	8500	9000	9500	10000	10500
P1,1[MW]	62.6342	111.4095	93.4401	111.8273	114.0000	114.0000
P1,2[MW]	62.6342	111.4095	93.4401	111.8273	114.0000	114.0000
P1,3[MW]	60	83.8286	69.4501	84.1629	88.8032	120.0000
P1,4[MW]	58.1447	127.9018	105.9376	128.4125	135.5010	184.4384
P1,5[MW]	68	97.0000	89.7009	97.0000	97.0000	97.0000
P1,6[MW]	128.6335	100.0267	82.0652	100.4443	106.2409	140.0000
P1,7[MW]	135	224.8212	189.3844	225.6452	237.0816	300.0000
P1,8[MW]	135	251.8268	207.4993	252.8575	267.1632	300.0000
P1,9[MW]	130	255.1525	209.8292	256.2063	270.8334	300.0000
P1,10[MW]	94	130.0000	130.0000	130.0000	130.0000	194.2785
P1,11[MW]	94	164.3456	134.9710	165.0286	174.5085	239.9567
P1,12[MW]	125	161.8368	132.1500	162.5270	172.1078	238.2515
P1,13[MW]	125	216.7120	174.0377	217.7042	231.4763	326.5568
P1,14[MW]	125	238.2467	190.9862	239.3455	254.5978	359.8966
P1,15[MW]	125	238.5932	191.8553	239.6799	254.7634	358.8979
P1,16[MW]	220	238.5932	191.8553	239.6799	254.7634	358.8979
P1,17[MW]	220	360.8711	301.0534	362.2620	381.5668	500.0000
P1,18[MW]	242	362.0568	301.9115	363.4552	382.8657	500.0000
P1,19[MW]	242	392.7521	325.9265	394.3058	415.8723	550.0000
P1,20[MW]	62.6342	392.7530	325.9272	394.3068	415.8732	550.0000
P2,1[MW]	550	420.5658	550.0000	547.5998	550.0000	477.1028
P2,2[MW]	550	420.1264	550.0000	546.9982	550.0000	476.5912
P2,3[MW]	550	422.2360	550.0000	548.1981	550.0000	478.2959
P2,4[MW]	550	422.2360	550.0000	548.1981	550.0000	478.2959
P2,5[MW]	550	400.6600	550.0000	518.2773	550.0000	453.0060
P2,6[MW]	550	400.6600	550.0000	518.2773	550.0000	453.0060
P2,7[MW]	15.4979	10.0000	15.3898	12.6284	28.4012	11.0158
P2,8[MW]	15.4979	10.0000	15.3898	12.6284	28.4012	11.0158
P2,9[MW]	15.4979	10.0000	15.3898	12.6284	28.4012	11.0158
P2,10[MW]	97	96.9774	97.0000	97.0000	97.0000	97.0000
P2,11[MW]	187.3504	420.5658	186.5573	166.2908	190.0000	477.1028
P2,12[MW]	187.3504	420.1264	186.5573	166.2908	190.0000	476.5912
P2,13[MW]	187.3504	422.2360	186.5573	166.2908	190.0000	478.2959
P2,14[MW]	90	422.2360	90.0000	90.0000	90.0000	478.2959
P2,15[MW]	90	400.6600	90.0000	90.0000	90.0000	453.0060
P2,16[MW]	90	400.6600	90.0000	90.0000	90.0000	453.0060
P2,17[MW]	110	10.0000	110.0000	110.0000	110.0000	11.0158
P2,18[MW]	110	10.0000	110.0000	110.0000	110.0000	11.0158
P2,19[MW]	110	10.0000	110.0000	110.0000	110.0000	11.0158
P2,20[MW]	550	96.9774	550.0000	458.4336	550.0000	97.0000
Pw[MW]	312.3995	312.4521	305.7285	303.5730	298.7680	282.5545
F _c [\$/h]	90408.3823	96712.8847	100631.4254	106292.5497	112214.6744	120069.1486
P _L [MW]	-	-	-	-	-	-
E _T [Kg/h]	42120.6871	43703.4949	49528.3791	54644.3179	63073.0950	79614.2253
CEED[Kg/h]	150011.2334	152808.9588	170151.9779	180787.3657	197097.3539	214795.2613

This study presents a comparison of the wind-thermal multi-area economic emission dispatch problem using the Lagrange algorithm in relation to other optimisation algorithms., Salp Swarm Algorithm(SSA), Flower Pollination Algorithm(FPA), and Backtracking Search Algorithm(BSA) (Alli, 2024), and Hybridizing Sum-Local Search Optimize (HLSO)(Chaudhary et al., 2020), and are given in Table 5.8.

Table 5.8: Lagrange algorithm compared with other optimization algorithms for MAWTEED applied to the IEEE 40-unit system for PD = 10500[MW]

Algorithm	SSA	FPA	BSA	HLSO	Developed LMM 330[MW] wind power
Reference	(Alli.,2024)			(Chaudhary,2020)	
P1,1[MW]	113.9998	97.4000	97.3999	110.8012	114.0000
P1,2[MW]	113.9996	179.7331	179.7331	113.9997	114.0000
P1,3[MW]	120	87.7999	87.7999	120.0	120.0000
P1,4[MW]	179.73331	105.3999	105.3999	179.7331	184.4384
P1,5[MW]	96.0324	300	259.5996	95.551	97.0000
P1,6[MW]	140	284.5997	284.5996	140.0	140.0000
P1,7[MW]	300	295.3663	284.5997	300.0	300.0000
P1,8[MW]	284.5995	279.5997	204.7997	284.5997	300.0000
P1,9[MW]	284.6002	94	94	284.5997	300.0000
P1,10[MW]	269.9999	94	94	270.0	194.2785
P1,11[MW]	168.7999	214.7598	304.5195	94.0	239.9567
P1,12[MW]	350.0002	394.2794	394.2793	300.0	238.2515
P1,13[MW]	394.2794	394.2794	394.2793	304.5195	326.5568
P1,14[MW]	394.2793	394.2794	394.2793	394.2797	359.8966
P1,15[MW]	304.5197	489.2794	489.2794	484.0395	358.8979
P1,16[MW]	484.0391	399.5196	489.2793	484.0391	358.8979
P1,17[MW]	489.2794	511.2794	511.2794	489.2794	500.0000
P1,18[MW]	489.2796	511.2794	511.2793	489.2796	500.0000
P1,19[MW]	511.2794	511.2794	523.2794	549.9998	550.0000
P1,20[MW]	511.2793	511.2794	523.2794	511.2791	550.0000
P2,1[MW]	523.2795	523.2794	523.2794	523.2792	477.1028
P2,2[MW]	343.7598	523.2794	523.2793	523.2791	476.5912
P2,3[MW]	254	523.2794	523.2794	523.2794	478.2959
P2,4[MW]	523.2794	523.2794	523.2794	523.2794	478.2959
P2,5[MW]	523.2793	10	10	523.2795	453.0060
P2,6[MW]	523.2793	10	10	254.0	453.0060
P2,7[MW]	109.9999	10	10	10.0001	11.0158
P2,8[MW]	109.9999	87.7999	87.7999	10	11.0158
P2,9[MW]	110	190	190	10	11.0158
P2,10[MW]	87.7998	190	190	87.7997	97.0000
P2,11[MW]	159.733	190	190	188.5959	477.1028
P2,12[MW]	159.733	200	196.9619	159.7331	476.5912
P2,13[MW]	159.7331	164.7999	164.7998	159.733	478.2959
P2,14[MW]	90	164.7999	164.7998	164.8002	478.2959
P2,15[MW]	164.8	110	109.9997	164.7998	453.0060
P2,16[MW]	164.8	110	89.1141	164.7998	453.0060
P2,17[MW]	72.296	110	109.9997	89.1143	11.0158
P2,18[MW]	89.114	511.2794	511.2793	89.114	11.0158
P2,19[MW]	89.114	550	549.9992	89.1134	11.0158
P2,20[MW]	242	550	550	242.0001	97.0000
Pw[MW]	-	-	-	-	282.5545
Fc[\$/h]	120857.2447	130573.2847	130580.7421	125100.2621	120069.1486
%Deviation of Fc for LMM in relation with the literature	0.16356	2.09544	2.09687	1.02605	1.34548 (average)
P _L [MW]					-
E _T [Kg/h]					79614.2253
CEED[Kg/h]	-	-	-	-	214795.2613

The relationship between the fuel cost [\$/h] and the power demand [MW] is shown graphically in Figure 5.7 for different optimization algorithms.

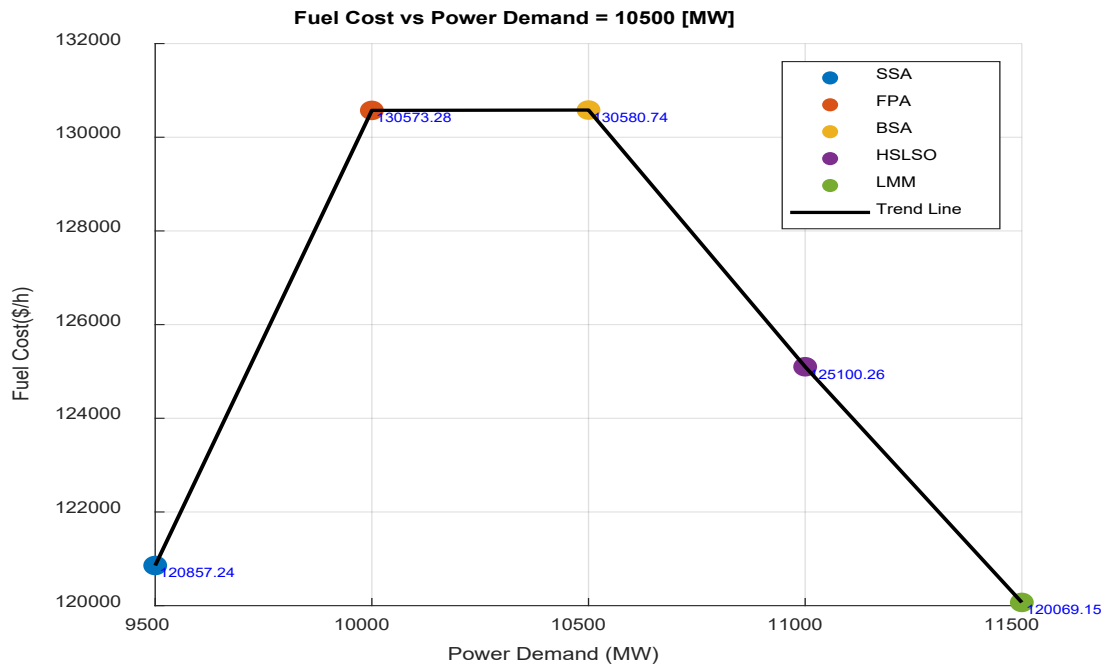


Figure 5.7: Values of fuel cost and power demand for the MAWTEED problem using the LM algorithm for a 40-unit system

As illustrated in Table 5.9, the fuel cost and emission values are compared with the statistical values of various algorithms.

Table 5.9: LMM Comparison with various algorithms(Ahmed et al., 2022)

Algorithm	Fuel cost (\$/h)	Fuel cost (%)Deviation	Emission (Kg/h)	Emission (%)Deviation
ABC	126 480.56	1.30023	209 285.74	22.4423
EMA	125 910.69	1.1874	210 238.19	22.5328
NSGA-II	125 830.00	1.17138	210 950.00	22.6001
SSA-WSA	125 760.05	1.15749	206 705.97	22.194
MOSSA	125 591.29	1.12394	205 965.40	22.1219
CSOA	124 330.50	0.8718	116 560.5	9.41668
Developed LMM	120069.1486	1.13537	79614.2253	20.218

The best fuel [\$/h] and emission [Kg/h] values for different optimization algorithms are compared with the LMM algorithm, as shown in Table 5.11 above. The best emission values are plotted against power demand[MW] as illustrated in Figure 5.8 below.

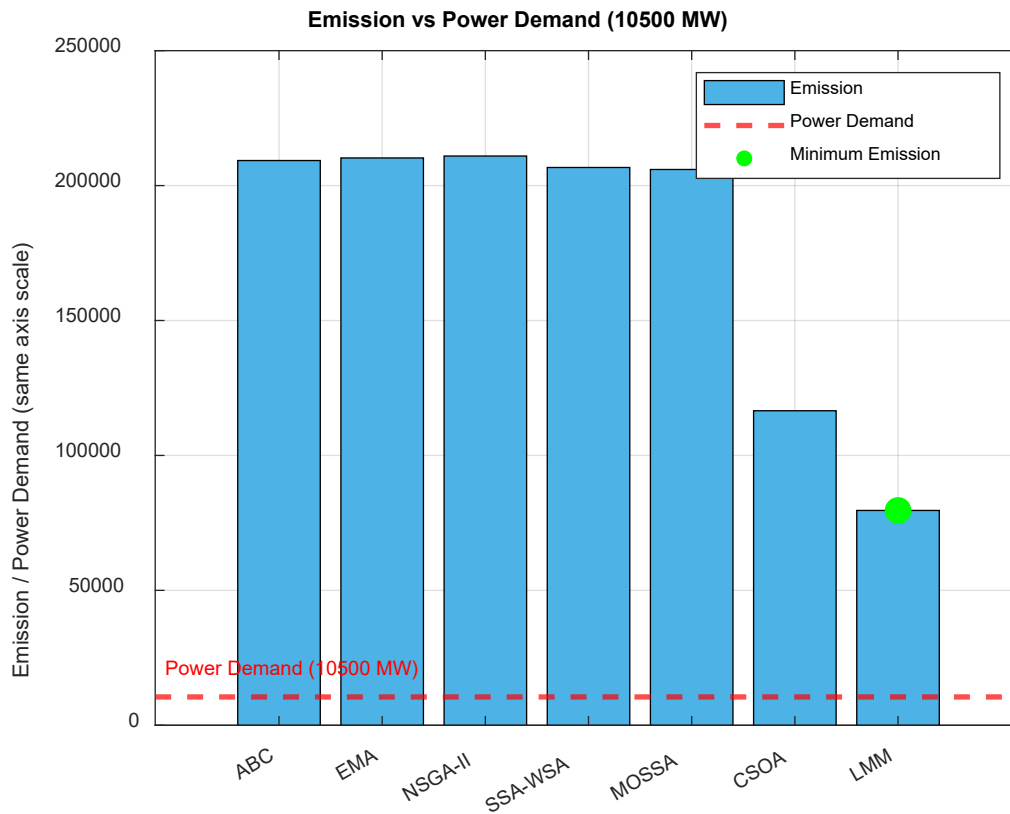


Figure 5.8: Values of emission and power demand for the MAWTEED problem using the LM algorithm for a 40-unit system

5.5.3.1 The MAWTEED problem results, and discussion for a 40-Unit System

This is a fourth-generation unit system used to evaluate the effectiveness of the Lagrange multiplier method relative to other optimization methods for minimizing fuel costs and atmospheric emissions. The following parameters are used for the Lagrange multiplier method. The initial value of lambda is [50 50], the total number of iterations m is 10000, the tolerance value (epsilon) is 0.01, and the tolerance value of delta-lambda epsilon is 0.1. The Lagrange multiplier method is compared with different heuristic algorithms, i.e., Salp Swarm Algorithm(SSA), Flower Pollination Algorithm(FPA), and Backtracking Search Algorithm(BSA)(Alli, 2024), and Hybridizing Sum-Local Search Optimize (HLSO)(Chaudhary et al., 2020). The comparison is made based on the best cost and lowest emissions. The summary of the comparison between the Lagrange method and the mentioned heuristic algorithms is given in Table 5.11.

The optimization algorithm took 3101 iterations to find the optimal solution of the MAWTEED problem. The calculated value of lambda after the optimization algorithm is [48.1302 22.3787], compared to the initial guess.

Table 5.11 shows that the values for fuel cost and emission minimization for LMM are 1.13537% and 20.218%, respectively, which are better than those for the MAWTEED problem.

5.6 Conclusions

In this chapter, a Multi-Area Wind–Thermal Economic Emission Dispatch problem is successfully solved using the Lagrange multiplier approach. Fuel and emission costs are minimised in the bi-objective problem of economic emission dispatch optimisation. This chapter presents the transmission line losses, emissions, and inequality limits. Three test systems, a 6-unit system with two areas, a 12-unit system with four areas, and a 40-unit system with two areas, are used to evaluate the algorithm. Compared to other methods, the fuel cost for 6-unit systems is reduced by 1–5%. Additionally, compared with previous optimisation techniques, the 12-unit system's fuel cost and emissions are 1–6% and 1–14%, respectively. Lastly, fuel consumption and emissions for the 40-unit system have decreased by 1% and 1–20%, respectively.

All test systems demonstrate that the Lagrange optimisation approach efficiently converges to an optimal solution by selecting the best initial lambda values. For fuel cost, emissions, and total generation in the MAWTEED problem, the optimal results for the 6-unit, 12-unit, and 40-unit systems are within the expected values reported in the literature. Compared to the heuristic methods described in the literature, the classical Lagrange approach utilising decomposition coordination can easily produce optimal results for fuel and emission reduction. For simple, convex cases, Lagrange's classical methods are reliable and accurate.

In chapter six, the Multi-Area Wind–Thermal Economic Emission Dispatch (MAWTEED) problem is solved using Particle Swarm Optimisation (PSO), and the MAWTEED dispatch problem solutions are compared between classical and heuristic optimisation techniques.

CHAPTER SIX

MULTI-AREA WIND-THERMAL ECONOMIC EMISSION DISPATCH(MAWTEED) PROBLEM USING PARTICLE SWARM OPTIMISATION(PSO)

6.1 Introduction

In this chapter, a Multi-Area Wind-Thermal Economic Emission Dispatch problem is solved using Particle Swarm Optimisation (PSO). Fuel and emission costs are minimised in the bi-objective problem of economic emission dispatch optimisation. This chapter presents the transmission line losses, emissions, and inequality limits. Three benchmark systems: a 6-unit system with two areas, a 12-unit system with four areas, and a 40-unit system with two areas, are used to test the PSO algorithm. Compared to other methods, the fuel cost for 6-unit systems is reduced by 1-5%. Additionally, compared with previous optimisation techniques, the 12-unit system's fuel cost and emissions are 1-6% and 1-12%, respectively. Finally, the 40-unit system shows a notable 1% reduction in fuel and a 14% reduction in emissions.

Efficient convergence of PSO is achieved through careful selection of algorithm parameters, including the inertia weight (w), cognitive coefficient (c_1), social coefficient (c_2), population size, and number of iterations. The fuel and emissions for the MAWTEED problem are affected by the random selection of PSO variables, and the resulting LMM and PSO values differ by 1% across all test systems. The optimum conditions for the 6-unit, 12-unit, and 40-unit systems, however, fall within the anticipated ranges for fuel cost, emissions, and total generation in the MAWTEED problem, as compared to the literature. Compared to the heuristic methods described in the literature, the classical Lagrange approach utilising decomposition coordination can easily produce optimal results for fuel and emission reduction. For simple, convex situations, Lagrange's classical methods are effective and accurate. On the other hand, when the objective function and constraints are nonlinear and nonconvex, the PSO algorithm can solve the MAWTEED problem more successfully than the Lagrange technique.

The chapter is further structured in the following sections. Section 6.2, Introduction to the PSO algorithm; Section 6.3, development of the PSO algorithm for the solution of the MAWTEED problem; Section 6.4, illustrates different case studies used for multi-area WTEED problem solutions.

6.2 Introduction to the PSO algorithm

Kennedy and Eberhart developed the particle swarm optimisation technique in 1995. It is an optimisation based on how the swarm's species behaves. It provides a population-based search strategy in which species, referred to as particles, navigate an open, multidimensional space and change their positions over time.

Based on both its own and the other particle's experiences, the particle positioned itself in the solution space, utilising the best position that both of them had encountered. Based on past experiences, the swarm follows the nearby particle. Every particle in the swarm travels around the search space at a specific speed that varies based on its prior experiences.

Let a particle coordinate (position) and its corresponding flight speed (velocity) in a search space denoted by p and v respectively. The i^{th} particle is preserved as a volume less particle assumed by $p_i = (p_{i1}, p_{i2} \dots p_{id})$ and the best position as $p_i^{best} = (p_{i1}^{best}, p_{i2}^{best} \dots p_{id}^{best})$. The index of the best particle amongst others is given a name called global best g_d^{best} . The change of velocity of the i^{th} particle is given by $v_i = (v_{i1}, v_{i2} \dots v_{id})$. Equations (6.1) and (6.2) provide the immediate velocity and the distance between p_{id}^{best} and g_d^{best} , respectively, which may be utilised to determine the updated velocity and location of each particle.

$$v_{id}^{t+1} = \omega v_{id}^t + c_1 rand() (p_{id}^{best} - p_{id}^t) + c_2 rand() (g_d^{best} - p_{id}^t) \quad (6.1)$$

$$p_{id}^{t+1} = p_{id}^t + v_{id}^{t+1} \quad (6.2)$$

Where

c_1 Self-confidence ranges between 1.5 and 2, and

c_2 Swarm range between 2 and 2.5.

$(p_{id}^{best} - p_{id}^t)$ and $(g_d^{best} - p_{id}^t)$ are a particle memory influence and a swarm influence.

The proper balance between global and local search can be achieved by selecting the inertia weight factor ω , to be between 0.9 and 0.4 during the search, and can be given

$$\omega = \omega_{max} - \left[\frac{\omega_{max} - \omega_{min}}{iter_{max}} \right] iter$$

by the following expression:

Where,

ω	The inertia weight factor
ω_{max} and ω_{min}	Maximum and minimum weighting factors
$Iter$ and $Iter_{max}$	Current and maximum iterations.

6.3 PSO algorithm developed for the solution of the MAWTEED problem

In Chapter 5, the Multi-Area Wind-Thermal Economic Emission Dispatch (MAWTEED) problem is formulated and solved using the Lagrange Multiplier Method (LMM). The

problem is articulated using the total fuel cost equation for thermal and wind power systems as given in equation (5.1). The fuel cost for conventional and wind power generators is given by equations (5.2) and (5.6). This is subject to equality and inequality constraints given in equations (5.5), (5.7), (5.8), and (5.11-5.14). The wind power system is further analysed using the probability density function (PDF), yielding equations (2.46) and (2.51). The emission function is given by equation (5.9), and the price penalty factors (5.9b) are used to formulate the bio-objective problem into a single objective function for the MAWTEED problem. The MAWTEED problem is solved using a tailored PSO heuristic optimization algorithm. It is needed to associate the structure of the MAWTEED problem with that of the velocity and position Equations (6.1) and (6.2) adopted by the PSO algorithm. This can be achieved with the following steps:

In the wind thermal economic dispatch problem, the active power generated by conventional and wind power generators is represented by the positions of particle members; the number of generators is equal to the number of members in a particular particle in the swarm.

The velocity values are parameters that indicate the active power, even though they are used to search within the boundaries.

It is anticipated that the quantity of particles in the swarm is N_p . Equations (5.1) to (5.9b) provide the developed PSO algorithm for solving the multi-area combined economic emission dispatch problem:

Step1: Provide the initial values for the acceleration constants, inertia weight, and other PSO parameters. Considering $c1$ and $c2$, the uniform random variables are $rand1$, $rand2$, and the maximum number of iterations $Iter^{max}$.

Step 2: Compute the lowest and highest initial velocities using the generator limit restrictions in Equations (5.11) and (5.12), and are presented in Equation (6.3) as follows:

$$-0.5P_{mpi}^{min} \leq V_{mpi} \leq +0.5P_{mpi}^{max}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.3)$$

Where

N_p Number of particles in the swarm

n The total number of generators equals the number of members in a single particle.

The particle position and velocity are calculated for $(n - 1)$ generators, since the first generator is acknowledged as a slack one.

Step 3: Compute the initial velocity of all members of the particles excluding the slack bus generator, using equation (6.4)

$$V_{mpi} = V_{mpi}^{min} + rand() (V_{mpi}^{max} - V_{mpi}^{min}), p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.4)$$

Where

$V_{mpi}^{min}, V_{mpi}^{max}$ Previously computed lowest and highest velocities

Step 4: Compute the initial Position of the particle members using Equation (6.5)

$$P_{mpi} = P_{mpi}^{min} + rand() (P_{mpi}^{max} - P_{mpi}^{min}), p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.5)$$

Wind power is added to equation (6.5) using equation (5.6) to obtain the active power of the MAWTEED problem in each area. Then this is verified if they are within the given limits in equation(5.12) and is represented by the following equation(6.6)

$$\left\{ \begin{array}{l} P_{mpi}^{min}, \quad P_{mpi} \leq \quad P_{mpi}^{min} \\ P_{mpi}^{max}, \quad P_{mpi} \geq \quad P_{mpi}^{max} \\ P_{mpi}, \quad P_{mpi}^{min} \leq P_{mpi} \leq P_{mpi}^{max} \end{array} \right\}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.6)$$

The power system's buses are divided into three categories: load (PQ), generator (PV), and slack buses. Any bus connected to a generator with the greatest generating capacity is referred to as a slack bus in a power system. The system's voltage and angle are referenced by the slack bus. The slack bus's real and reactive powers are uncontrollable; the actual or reactive power necessary to balance the system's power flows is provided by the bus.

Generation scheduling is used to solve the economic dispatch problem without accounting for the actual power output of the slack bus generator. In the PSO algorithm, the slack bus serves to meet the power balance requirement specified in Equation (2.4). Step 5 outlines the process for determining the real power of the slack bus generator in the PSO algorithm.

Step 5: The slack bus generator is considered to have the most power-generating capability among dependent generators. Equation (6.7a) provides the power balance constraint that may be used to calculate the initial active power P_{mpd} using the bus voltage magnitude and phase angle as a reference(Krishnamurthy & Tzoneva, 2012):

$$P_{mpd} + \sum_{i \neq d}^n P_{mpi} = \left\{ \sum_{i \neq d}^n \sum_{j \neq d}^n P_{mpi} B_{ij} P_{pj} + \sum_{j \neq d}^n P_{mpj} (B_{jd} + B_{dj}) P_{mpd} + B_{dd} P_{mpd}^2 + \sum_{i \neq d}^n B_{io} P_{mpi} + B_{do} P_{mpd} + B_{moo} + P_{Dm} \right\}, p = \overline{1, N_p} \quad (6.7a)$$

Where

P_{mpd} Is the power generated by the slack bus for each area.

P_{Dm} Is the total power demand for each area

$\sum_{i \neq d}^n P_{mpi}$ Is the total active power of the power system, without the slack bus power, and is known by. $\sum_{i \neq d}^n P_{mpi} = [P_{mT1}, P_{mT2} \dots P_{mNT}, P_{Wm1}, P_{Wm2} \dots P_{WNw}]$, (6.7b)

Where,

P_{TN_T} Is the active power generated by thermal power generators for the area.
 P_{WN_w} Is the active power generated by wind power generators for each area.

By using the quadratic form, Equation (6.7) can be rewritten, where the P_{mpd} is the unknown variable in the equation.

$$XP_{mpd}^2 + YP_{mpd} + Z = 0 \quad (6.8)$$

Where

$$X = B_{dd} \quad (6.9)$$

$$\sum_{j \neq d}^n P_{mpj} (B_{jd} + B_{dj}) + B_{do} - 1 \quad (6.10)$$

$$Z = \sum_{i \neq d}^n \sum_{j \neq d}^n P_{mpi} B_{ij} P_{mpj} + \sum_{i \neq d}^n B_{io} P_{mpi} + B_{moo} + P_{Dm} - \sum_{i \neq d}^n P_{mpi} \quad (6.11)$$

Equation (6.8) positive root can be found as follows:

$$P_{mpd} = \frac{-Y + \sqrt{Y^2 - 4XZ}}{2X}, \text{ where } Y^2 - 4XZ \geq 0 \quad (6.12)$$

Now the real power vector is shaped as the $P_{mp} = [P_{mpd}, P_{mpi}, i = 1, n, i \neq d]$

where $p = \overline{1, N_p}$

Step 6: Compute the following objective functions for the initial positions of the particles.

Fuel cost function

$$F_C(P_{mn}) = \sum_{n=1}^M \sum_{n=1}^{N_m} (a_{mn} P_{Gmn}^2 + b_{mn} P_{Gmn} + c_{mn}) \quad (6.13)$$

Emission function

$$F_e = \sum_{n=1}^M \sum_{n=1}^{N_m} (d_{mn} P_{mn}^2 + e_{mn} P_{mn} + f_{mn}) \quad (6.14)$$

Combined economic emission function

$$F_T = \sum_{n=1}^M \sum_{n=1}^{N_m} (a_{mn} P_{mn}^2 + b_{mn} P_{mn} + c_{mn}) + h_{mn} (d_{mn} P_{mn}^2 + e_{mn} P_{mn} + f_{mn}) \quad (6.15)$$

Where the Max-Max price penalty factor is computed as:

$$h_{mn} = \frac{a_{mn} P_{mn,max}^2 + b_{mn} P_{mn,max} + c_{mn}}{d_{mn} P_{mn,max}^2 + e_{mn} P_{mn,max} + f_{mn}}, n = \overline{1, M, N_m} \quad (6.16)$$

The fuel cost parameters F_C of all the particles are arranged in ascending order. The first position value in the ascending order is picked as the F_T^{best}

Step 7: Select the best initial position and the global best initial position as follows:

The initial particle locations in the swarm are assumed to be optimal.

$$P_{mp}^{best} = \min P_{mp}^{best}, p = \overline{1, N_p}, i = \overline{1, n}.$$

The best position out of all the best particles $\min P_{mp}^{best}, p = \overline{1, N_p}$ is taken as

$$G_{mp}^{best} = \min P_{mp}^{best}, p = \overline{1, N_p}$$

l^{th} step of the iteration process commences, where $l = l + 1$

Step 8: Calculate new velocity using Equation (6.17)

$$V_{pi}^{new^l} = \omega \cdot V_{mpi}^{l-1} + c1 * rand1() (P_{mp}^{best^{l-1}} - P_{mpi}^{l-1}) + c1 * rand1() (G^{best^{l-1}} - P_{mpi}^{l-1}),$$

$$p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.17)$$

Check the limits on the lowest and highest velocities.

$$\text{If } V_{mpi}^{new^l} > V_{mpi}^{max^{l-1}}, V_{mpi}^{new^l} = V_{mpi}^{max^{l-1}} \text{ and}$$

$$\text{If } V_{mpi}^{new^l} < V_{mpi}^{min^{l-1}}, V_{mpi}^{new^l} = V_{mpi}^{min^{l-1}}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.18)$$

Step 9: Apply Equation (6.18) to determine the generator's new locations within the particles.

$$\text{If } P_{mpi}^{new^l} = P_{mpi}^{l-1} + V_{mpi}^{new^l}, p = \overline{1, N_p}, i = \overline{1, n} \quad (6.19)$$

Step 10: Employing the constraint Equation (6.6), determine the generators' new locations within the particles as follows:

$$P_{pi}^{new^l} = \left\{ \begin{array}{l} P_{mpi}^{min}, \quad P_{mpi}^{new^l} \leq P_{mpi}^{min} \\ P_{mpi}^{max}, \quad P_{mpi}^{new^l} \geq P_{mpi}^{max} \\ P_{mpi}^{new}, \quad P_{mpi}^{min} \leq P_{mpi}^{new^l} \leq P_{mpi}^{max} \end{array} \right\}, p = \overline{1, N_p}, i = \overline{1, n-1} \quad (6.20)$$

Step 11: Determine the new real power of the slack bus generator. Employing the formula from step 5, create the new real power vector $P_{mpi}^{new^l}$. Utilising the constraint Equation (6.6), determine the slack bus generators' new location within the particles.

$$P_{pd}^{new^l} = \left\{ \begin{array}{l} P_{mpd}^{min}, \quad P_{mpd}^{new^l} \leq P_{mpd}^{min} \\ P_{mpd}^{max}, \quad P_{mpd}^{new^l} \geq P_{mpd}^{max} \\ P_{mpd}^{new}, \quad P_{mpd}^{min} \leq P_{mpd}^{new^l} \leq P_{mpd}^{max} \end{array} \right\} \quad (6.21)$$

Step 12: The full active power vector for the l^{th} iteration is:

$$P_{mpd}^{new^l} = (P_{mpd}^{new^l}, P_{mpi}^{new^l}, i \neq d, i = \overline{1, n}), p = \overline{1, N_p} \quad (6.22)$$

Step 13: Compute the new objective functions F_{mT}^{new} using Step 6

Step 14: Verify the new objective function F_T^{new} as explained below

$$\begin{aligned} \text{If } F_{mT}^{new^l} < F_{mT}^{best^{l-1}} \text{ then } F_{mT}^{best^l} &= F_{mT}^{new^l} \text{ and } P_{mpi}^{best^l} = P_{mpi}^{new^l} \\ \text{Else If } F_{mT}^{best^l} &= F_{mT}^{best^{l-1}} \text{ and } P_{mpi}^{best^l} = P_{mpi}^{best^{l-1}} \end{aligned} \quad (6.23)$$

$$G^{best^l} = P_{mp}^{best^l}, p = \overline{1, N_p}$$

where l is the number of iterations

The best solution G^{best} is only one for the whole system. The best solution per particle is only one $P_{mp}^{best} = \min P_{mpi}, i = \overline{1, n}$.

The best solution for the entire system is $P_{mp}^{best} = [P_{m1}^{best}, P_{m1}^{best}, \dots, P_{N_p}^{best}]$. Then

$$G^{best} = \min P_{mp}^{best^l}, p = \overline{1, N_p}$$

Step 15: Repeat steps 5-13 until the highest number of iterations is attained.

6.4 Case studies of the multi-area MAWTEED problem solutions

Three benchmark models for multi-area power systems are used to test the proposed algorithm:

- (i) There are two areas with six generators and three thermal generating units each, after taking into account transmission line losses, tie-line power transfer across areas, and wind power of 330MW injected in area 1.
- (ii) Four areas with three thermal units in each area, considering the transmission line losses, and 330MW of wind power from three wind farms supplying 110MW each.
- (iii) Two areas with 20 generating units in each area, and a wind farm of 330MW, applied in area 1. The PSO flowchart is shown in Figure 6.1 below.

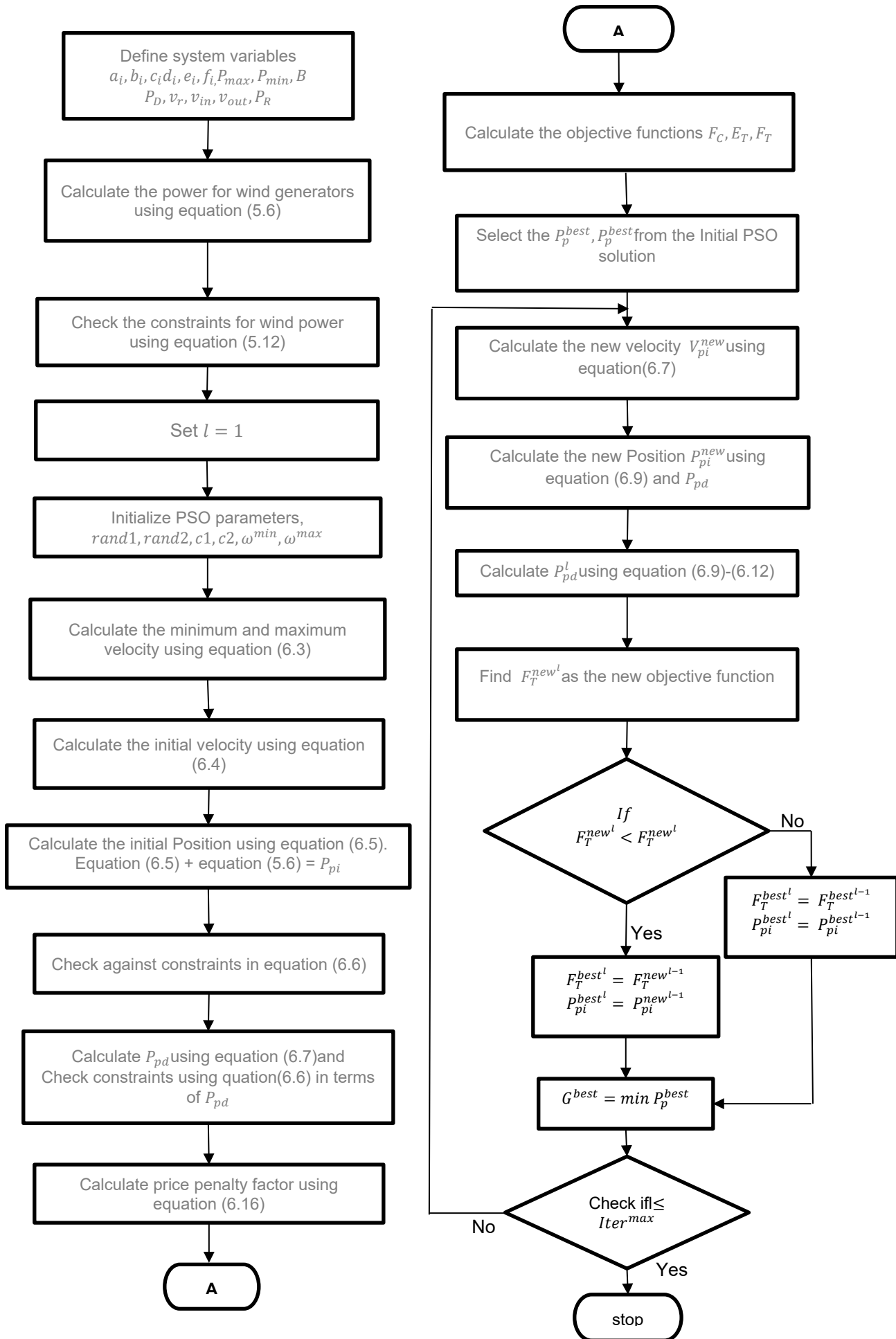


Figure 6.1: The MAWTEED problem solution flowchart of applied to PSO algorithm

6.4.1 Test system I: IEEE 30 bus system with 6 generating units.

The MAWTEED problem is solved using two areas with six conventional units, each containing three thermal generators. The three wind park network supplies 110MW of wind power each to the entire dispatch problem (Alli, 2024). The total power demand is 1263 [MW]. The area demand is 60% for area 1, and 40% for area 2. The demand for area 1 is 757.8 MW, and for area 2, it is 505.2MW. The data for the fuel cost is taken from (Basu, 2013) and B-loss coefficients (Krishnamurthy et al., 2017). Several power demand values are presented in Table 6.1 to validate the system's performance under fluctuations in power demand. The MATLAB script is called MAWTEED_casePSO6units.m, and the program is provided in Appendix D1.

Table 6.1: The MAWTEED problem applied to the PSO algorithm with various power demands

PD[MW]	600	700	800	900	1000	1263
P1,1[MW]	100	100.0000	130.83	102.306	114.281	283.255
P1,2[MW]	50	50.0000	52.263	108.768	145.408	156.508
P1,3[MW]	50	50.0000	66.46	80.7334	91.9783	115.813
P2,1[MW]	80	101.9249	80.0	153.983	185.284	261.211
P2,2[MW]	50	50.0000	121.84	82.241	95.1919	72.6066
P2,3[MW]	50	57.5588	58.094	81.4515	77.3408	83.089
Pw[MW]	290.5184	290.5184	290.52	290.518	290.518	290.518
PL[MW]	2.9584	3.3925	5.274	7.43403	10.2943	20.8807
F _c [\$/h]	4854.9860	5104.9225	5936.3	6750.67	7569.49	9797.22
E _T [Kg/h]	223.2592	235.9724	309.92	322.468	410.726	923.159
CEED[Kg/h]	7285.6285	7639.6617	8909.10	10151.5	11803.5	16560.8
Computational time(s)						30.14 s

The solution of the MAWTEED problem is shown in Table 6.1 above. The real power generators (P1,1-P1,3) and (P2,1-P2,3) units represent the thermal generators for area 1 and area 2, wind (Pw) generators represent the wind power generators for all three wind parks in [MW], fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h]. The obtained fuel cost using PSO is compared with Artificial Bee Colony Optimization (ABCO), Differential Evolution (DE), Evolutionary Programming (EP), Real-coded Genetic Algorithm (RCGA), and Semi-define Programming (SDP) (Basu, 2013), and (Alli, 2024) algorithms that are found in the literature, and proposed the LMM that was found in Chapter 5, as shown in Table 6.2 below.

Table 6.2: PSO and LM compared with other optimisation algorithms for the MAWTEED problem using PD = 1263[MW]

Reference	(Basu.,2013)				(Alli,2024)	Proposed LMM	Proposed PSO
Algorithm	ABCO	DE	EP	RCGA	SDP		
P1,1[MW]	500.0000	500.0000	500.0000	500.0000	311.0838	232.7670	283.255
P1,2[MW]	200.0000	200.0000	200.0000	200.0000	200.0000	120.1745	156.508
P1,3[MW]	149.9997	150.0000	149.9919	149.6328	150.0000	96.7054	115.813
P2,1[MW]	204.3358	204.3341	206.4493	205.9398	162.8737	238.7650	261.211
P2,2[MW]	154.9954	154.7048	154.8892	155.8322	159.5473	169.1088	72.6066
P2,3[MW]	67.2915	67.5770	65.2717	65.2209	101.7656	110.7344	83.089
Pw [MW]	-	-	-	-	-	313.9185	290.518
PL[MW]	13.6224	13.6159	13.6021	13.6257	-	19.1629	20.8807
Fc[\$/h]	12255.39	12255.42	12255.43	12256.23	10722.00	9819.9287	9797.22
%Deviation of Fc for LMM in relation to the literature	5.57	5.57	5.57	5.57	2.25	0.057	4.10 Average
E _T [Kg/h]	-	-	-	-	-	830.2617	923.159
CEED[Kg/h]	-	-	-	-	-	16427.6875	16560.8

Figure 6.2 illustrates the relationship between fuel cost [\$/h] and power demand [MW] for PSO and other optimisation techniques, outlined in Table 6.2 above.

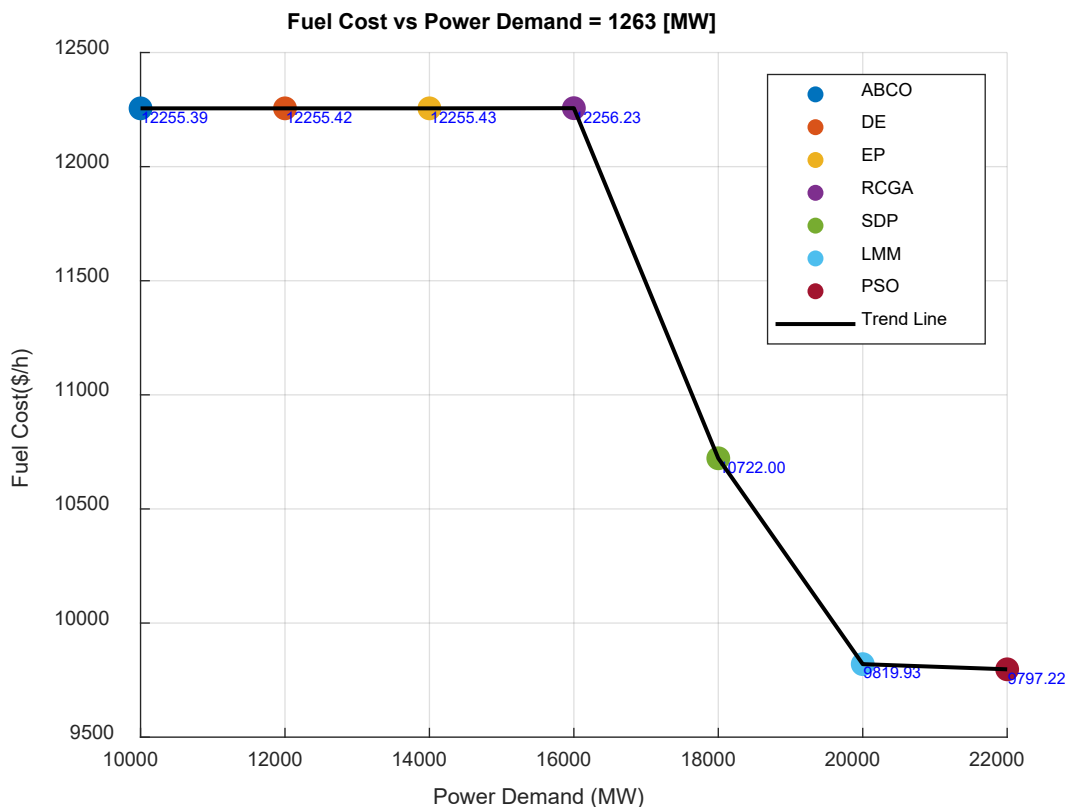


Figure 6.2: Fuel cost versus power demand for different optimisation methods using the PSO algorithm for a 6-unit system

6.4.1.1 The MAWTEED problem results, and discussion for the 6-Unit System

This system utilises three wind farm networks, which supply 330 [MW] to the power dispatch problem. The following parameters for the PSO algorithm are used. Swarm Size is 80, maximum number of iterations is 600, initial weight w is 0.72, and c_1 , c_2 are both 1.49. The proposed algorithm for a 6-unit multi-area system is compared with the LM method, and other optimization algorithms in the literature, namely, Artificial Bee Colony Optimization (ABCO), Differential Evolution (DE), Evolutionary Programming (EP), Real-coded Genetic Algorithm (RCGA), and Semi-define Programming (SDP)(Basu, 2013), and (Alli, 2024). The comparison is of the simulation results shown in Table 5.2 above.

The fuel cost results for the ABCO, DE, EP, RCGA, SDP, and LM algorithms are 5.57%, 5.57%, 5.57%, 5.57%, 2.25%, and 0.057%, respectively, compared to the PSO algorithm. When using the PSO algorithm, there is a 1–4% reduction in fuel consumption when wind power is added to the economic emission dispatch, compared with other optimisation algorithms.

6.4.2 Test System 2: IEEE30 bus system with 12 generating units.

This test system consists of a standard IEEE 30-bus system with four areas, 12 thermal generators (3 in each area), and a three-wind-park network that supplies 110MW of wind power to the entire dispatch problem. The total power demand is 2090 [MW]. The area demand is considered to be 500 [MW] for area 1, 410 [MW] for area 2, 580 [MW] for area 3, and 600 [MW] for area 4. The fuel cost and wind parameters are formed based on the ones reported in (Krishnamurthy & Tzoneva, 2016) and (Alli, 2024) As a test unit, several power demand values are presented in Table 6.3 to test the system's behaviour to changes in power demand. The MATLAB script is called MAWTEED_casePSO12units. m, and the software is provided in Appendix D2.

Table 6.3: The MAWTEED problem using PSO with various power demands for a 12-unit system.

PD[MW]	1500	1600	1800	1900	2090
P1,1[MW]	35.0000	35.0000	35.0000	55.3949	58.5930
P1,2[MW]	130.0000	130.0000	130.0000	130.0000	175.3381
P1,3[MW]	125.0000	125.0000	125.0000	125.0000	138.4997
P2,1[MW]	10.0000	10.0000	10.0000	10.0000	53.1994
P2,2[MW]	49.4221	69.3285	92.1409	100.7025	77.3587
P2,3[MW]	125.0000	125.0000	125.2665	132.6416	165.1398
P3,1[MW]	108.2540	146.1657	148.5243	140.9480	152.7173
P3,2[MW]	78.1069	80.8725	161.7085	101.5956	128.8915
P3,3[MW]	50.0000	50.0000	50.0000	146.3462	182.5738
P4,1[MW]	82.4448	110.7047	118.6657	146.6789	175.0000
P4,2[MW]	146.6411	160.4819	102.8930	119.1091	189.9407
P4,3[MW]	50.0000	50.0000	185.3564	171.3252	153.4674
Pw[MW]	330.3487	330.3487	330.3487	330.3487	330.3487
PL[MW]	11.4070	13.7845	19.2397	21.4340	29.7363
F _c [\$/h]	61402.9487	68225.1214	78007.8138	84856.2654	102939.913
E _T [Kg/h]	544.3535	657.5582	754.4482	818.4158	1103.8629
CEED[Kg/h]	97366.9480	111456.1810	126874.800	137412.0394	176832.189

The solution of the MAWTEED problem is shown in Table 6.3 above. The real power generators (P1,1-P1,3), (P2,1-P2,3), (P3,1-P3,3), and (P4,1-P4,3) units represent the thermal generators for area 1, area 2, area 3, and area 4. Wind (Pw) generators represent the wind power generators for all three wind parks in [MW], fuel cost (F_c), total emission (E_T) in [kg/h], and CEED in [Kg/h]. The obtained fuel cost and emission using PSO is compared with Lagrange's Decomposition- Coordinating Method (LDCM), Particle Swarm Optimisation (PSO), and Simplex-Particle Swarm Optimisation (SPSO)(Chopra et al., 2018) algorithms found in the literature, as shown in Table 6.4 below.

Table 6.4: PSO compared with other optimisation algorithms for the MAWTEED problem,

PD = 2090[MW]

Algorithm	LDCM	PSO	SPSO	LMM (Krishnamurthy,2011)	Proposed LMM	Proposed PSO
	(Chopra et al., 2018)					
P1,1[MW]	131.45	160.9	165	182.7879	87.5974	58.5930
P1,2[MW]	209.49	163.3	260	302.6497	138.5237	175.3381
P1,3[MW]	202.25	289.4	265	287.4964	133.0488	138.4997
P2,1[MW]	150	109.6	150	130.5891	86.1913	53.1994
P2,2[MW]	110	117.1	75	110.0000	110.0000	77.3587
P2,3[MW]	191.63	184.4	175	147.6606	125.0000	165.1398
P3,1[MW]	175	171.5	175	142.9309	146.1331	152.7173
P3,2[MW]	215	197.5	160	181.2219	182.9771	128.8915
P3,3[MW]	236.38	198.3	280	168.9267	173.4331	182.5738
P4,1[MW]	164.09	230	175	126.3394	141.6098	175.0000
P4,2[MW]	180.2	144.8	160	140.9621	156.0605	189.9407
P4,3[MW]	306.18	211.5	280	236.9631	262.9685	153.4674
Pw[MW]	-	-	-	-	329.2499	330.3487
F _c [\$]	144058.2	136598.3	134557.6	125883.5243	106977.016	102939.913
%Deviation of F _c for LMM in relation to the literature	8.3236	7.02568	6.65642	5.01339	0.9616	5.59614

PL[MW]	61.82	48.22	43.804	68.5286	33.6248	29.7363
ET[T]	1923.7	3713.93	1473.935	1684.6603	1120.2618	1103.8629
%Deviation of E_T for LMM in relation to the literature	13.5396	27.0878	7.17807	10.4141	0.36866	11.7176
CEED[\$/h]	266400.92	277258.2	232500.67	225665.1721	181987.099	176832.189
%Deviation of CEED for LMM in relation to the literature	10.104	11.0579	6.7999	6.06625	0.71832	6.94927

Figures 6.3, 6.4, and 6.5 graphically illustrate the relationship between fuel cost [\$/h], emission [Kg/h], and CEED with power demand [MW] for various optimisation strategies.

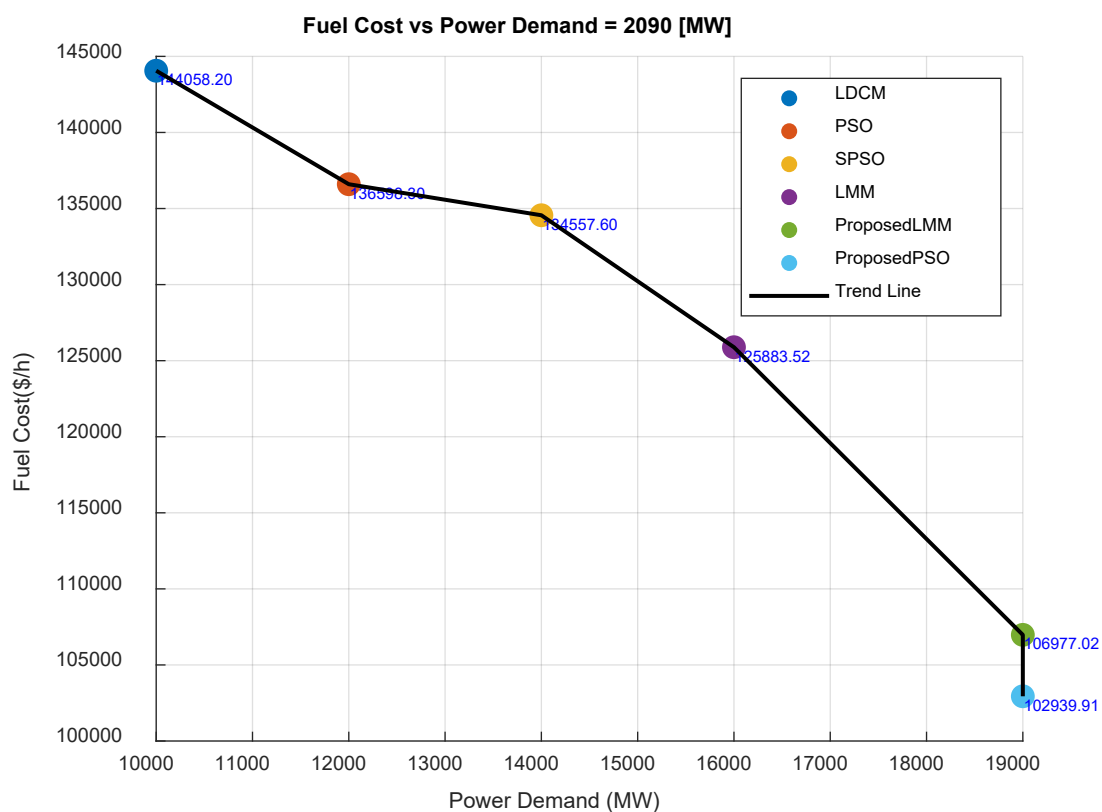


Figure 6.3: Values of fuel cost and power demand for various optimisation strategies applied to the PSO algorithm for a 12-unit system

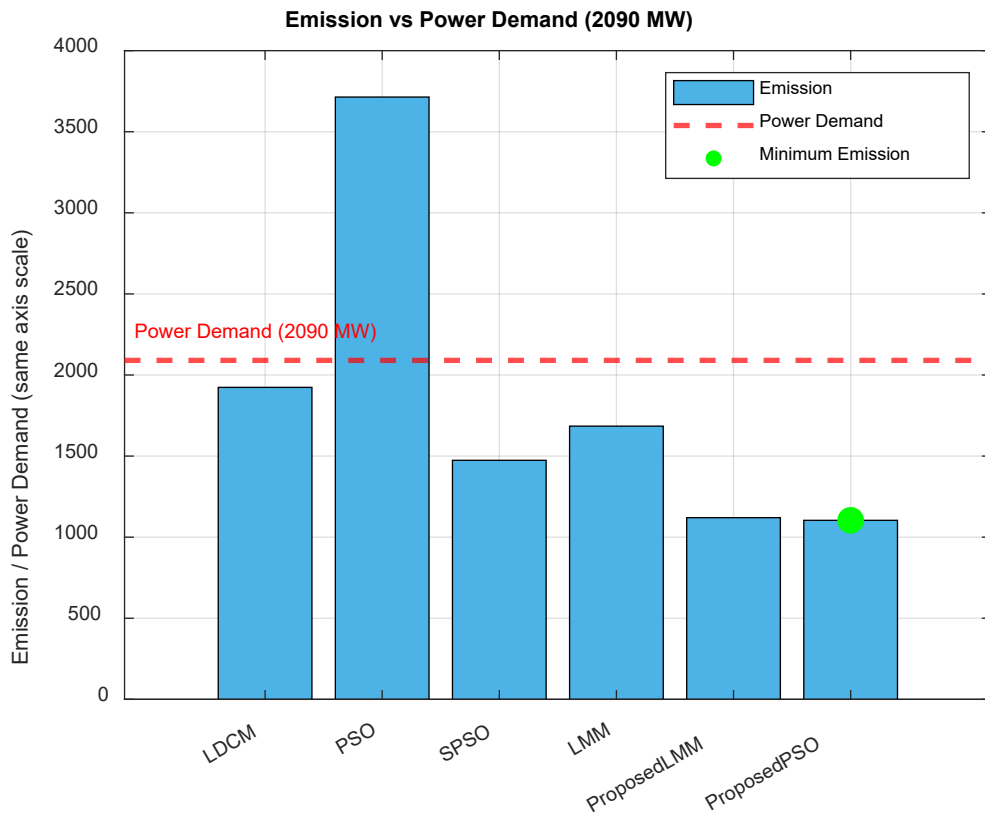


Figure 6.4: Emission versus power demand for different optimisation methods using the PSO algorithm for a 12-unit system

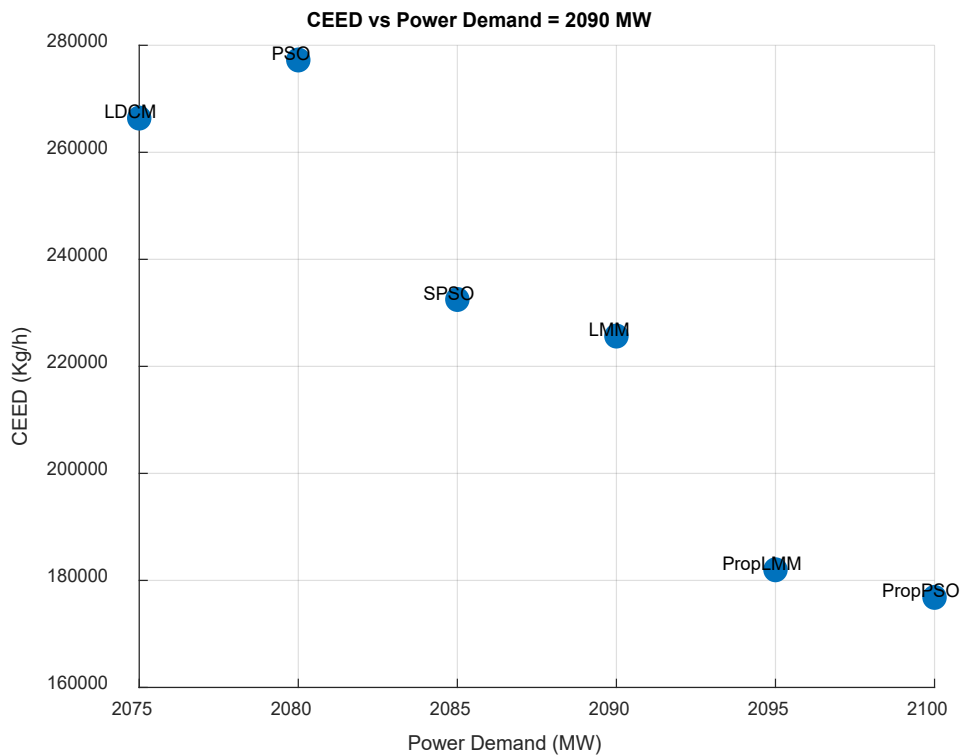


Figure 6.5: CEED versus power demand for different optimisation methods using the PSO algorithm for a 12-unit system

6.4.2.1 The MAWTEED problem results, and discussion for 12-Unit System

The PSO is applied for solving the multi-area economic emission dispatch problem with wind power, utilizing three wind farms of 110MW each. The following parameters for the PSO algorithm are used. Swarm Size is 100, maximum number of iterations is 500, initial weight w is 0.9, and c_1 , c_2 are both 2. The PSO is compared with Lagrange's Decomposition-Coordinating Method (LDCM), Particle Swarm Optimisation (PSO), and Simplex-Particle Swarm Optimisation (SPSO)(Chopra et al., 2018)and LMM developed in Chapter 5. The fuel cost results for LDCM, PSO, SPSO, LMM, and the developed LMM algorithms are 8.32%, 7.026%, 6.67%, 5.01%, and 0.96%, respectively, compared to the proposed PSO algorithm. When using the PSO algorithm, there is a 1–6% reduction in fuel consumption when wind power is added to the economic emission dispatch, compared with other optimisation algorithms. The resultant NOx emissions are 13.54%, 27.09%, 7.18%, 10.41%, and 0.37% lower than those of the developed PSO algorithm. The PSO algorithm has effectively reduced pollutant levels by 1–12% compared to other optimization algorithms.

The proposed algorithm has lower fuel cost and lower emissions and is observed to be superior to all other optimization algorithms.

6.4.3 Test System 3: IEEE30 bus system with 40 generating units.

The problem of solving MAWTEED using the Lagrange algorithm is carried out on a standard IEEE 30-bus two-area system with 40 thermal generators (20 in each area) and a three-wind park network supplying 110MW each to the entire dispatch problem. The total power demand is considered as 10500MW. The area demand is considered as 7500 MW for area 1 and 3000 MW for area 2, respectively. The fuel cost and wind parameters are formed based on the ones reported in (Krishnamurthy & Tzoneva, 2016) and (Alli, 2024) and are shown in Tables 6.5 and 6.6.

Table 6.5: Wind-speed data

v_{in} Cut-in wind speed	v_r Rated wind-speed	v_o Cut-out wind speed	w_r Rated Power	C_{pw} Underestimation	C_{rw} Overestimation	d_w direct cost
5	15	45.	330	5	5	0

Table 6.6: IEEE 30 Bus System data for 40 thermal systems.

Generating Unit [MW]	Generator Limits		Fuel cost coefficients			Emission coefficients		
	P_{min}	P_{max}	a_i [\$/ (MWh) ²]	b_i [\$/MWh]	c_i [\$/h]	α_i [t/(MWh) ²]	β_i [t/MWh]	γ_i [t/h]
1	36	114	0.0069	6.73	94.705	0.048	-2.22	60
2	36	114	0.0069	6.73	94.705	0.048	-2.22	60
3	60	120	0.02028	7.07	309.54	0.0762	-2.36	100
4	80	190	0.00942	8.18	369.03	0.054	-3.14	120
5	47	97	0.0114	5.35	148.89	0.085	-1.89	50
6	68	140	0.01142	8.05	222.33	0.0854	-3.08	80
7	110	300	0.00357	8.03	287.71	0.0242	-3.06	100
8	135	300	0.00492	6.99	391.98	0.031	-2.32	130
9	135	300	0.00573	6.6	455.76	0.0335	-2.11	150
10	130	300	0.00605	12.9	722.82	0.425	-4.34	280
11	94	375	0.00515	12.9	635.2	0.0322	-4.34	220
12	94	375	0.00569	12.8	654.69	0.0338	-4.28	225
13	125	500	0.00421	12.5	913.4	0.0296	-4.18	300
14	125	500	0.00752	8.84	1760.4	0.0512	-3.34	520
15	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
16	125	500	0.00708	9.15	1728.3	0.0496	-3.55	510
17	220	500	0.00313	7.97	647.85	0.0151	-2.68	220
18	220	500	0.00313	7.95	649.69	0.0151	-2.66	222
19	242	550	0.00313	7.97	647.83	0.0151	-2.68	220
20	242	550	0.00313	7.97	647.81	0.0151	-2.68	220
21	254	550	0.00298	6.63	785.96	0.0145	-2.22	290
22	254	550	0.00298	6.63	785.96	0.0145	-2.22	285
23	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
24	254	550	0.00284	6.66	794.53	0.0138	-2.26	295
25	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
26	254	550	0.00277	7.1	801.32	0.0132	-2.42	310
27	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
28	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
29	10	150	0.52124	3.33	1055.1	1.842	-1.11	360
30	47	97	0.0114	5.35	148.89	0.085	-1.89	50
31	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
32	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
33	60	190	0.0016	6.43	222.92	0.0121	-2.08	80
34	90	200	0.0001	8.95	107.87	0.0012	-3.48	65
35	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
36	90	200	0.0001	8.62	116.58	0.0012	-3.24	70
37	25	110	0.0161	5.88	307.45	0.095	-1.98	100
38	25	110	0.0161	5.88	307.45	0.095	-1.98	100
39	25	110	0.0161	5.88	307.45	0.095	-1.98	100
40	242	550	0.00313	7.97	647.83	0.0151	-2.68	220

Several power demand values are presented in Table 6.7 to validate the system's performance under alterations in power demand. The MATLAB script is identified as WTEED_casestudy9. m, and the software is available in Appendix D3. The solution of the MAWTEED problem is shown in Table 6.7. The real power generators (P1,1-P1,20) units represent the thermal generators for area 1, generators from (P2,1-2,20) represent generators for area 2, and wind (P_w) generators represent only wind power for area1 all in [MW], fuel cost (F_C), total emission (E_T) in [kg/h], and CEED in [Kg/h].

Table 6.7: The MAWTEED problem PSO method with various power demands for a 40-unit system

PD[MW]	8000	8500	9000	9500	10000	10500
P1,1[MW]	36.0000	114.0000	114.0000	114	114.0000	114.0000
P1,2[MW]	36.0000	114.0000	114.0000	36	36.0000	114.0000
P1,3[MW]	60.0000	102.8100	115.0000	120	120.0000	60.0000
P1,4[MW]	190.0000	190.0000	190.0000	190	80.0000	190.0000
P1,5[MW]	97.0000	97.0000	47.0000	97	97.0000	97.0000
P1,6[MW]	134.1925	112.6848	140.0000	140	140.0000	140.0000
P1,7[MW]	110.0000	300.0000	300.0000	300	300.0000	300.0000
P1,8[MW]	135.0000	175.5269	300.0000	300	300.0000	300.0000
P1,9[MW]	300.0000	300.0000	300.0000	300	300.0000	300.0000
P1,10[MW]	300.0000	300.0000	300.0000	300	300.0000	300.0000
P1,11[MW]	216.6743	299.4848	375.0000	375	375.0000	375.0000
P1,12[MW]	375.0000	375.0000	375.0000	375	375.0000	375.0000
P1,13[MW]	314.6343	500.0000	500.0000	500	500.0000	500.0000
P1,14[MW]	500.0000	476.6063	500.0000	500	500.0000	500.0000
P1,15[MW]	500.0000	500.0000	500.0000	500	500.0000	500.0000
P1,16[MW]	500.0000	342.3620	500.0000	500	500.0000	500.0000
P1,17[MW]	399.2286	370.5245	500.0000	500	500.0000	500.0000
P1,18[MW]	500.0000	500.0000	500.0000	500	500.0000	500.0000
P1,19[MW]	516.2649	550.0000	550.0000	550	550.0000	550.0000
P1,20[MW]	550.0000	550.0000	550.0000	550	550.0000	550.0000
P2,1[MW]	254.0000	254.0000	254.0000	254	453.9478	301.2412
P2,2[MW]	254.0000	254.0000	254.0000	254	254.0000	254.0000
P2,3[MW]	254.0000	254.0000	254.0000	254	254.0000	254.0000
P2,4[MW]	254.0000	254.0000	254.0000	254	254.0000	254.0000
P2,5[MW]	254.0000	254.0000	254.0000	254	254.0000	254.0000
P2,6[MW]	254.0000	254.0000	254.0000	254	254.0000	254.0000
P2,7[MW]	10.0000	10.0000	10.0000	10	10.0000	10.0000
P2,8[MW]	10.0000	10.0000	10.0000	10	10.0000	10.0000
P2,9[MW]	10.0000	10.0000	10.0000	10	41.9918	10.0000
P2,10[MW]	47.0000	47.0000	47.0000	47	97.0000	97.0000
P2,11[MW]	60.0000	60.0000	60.0000	60	116.3246	190.0000
P2,12[MW]	60.0000	60.0000	60.0000	190	184.7120	189.4034
P2,13[MW]	60.0000	60.0000	60.0000	60	75.4467	125.3571
P2,14[MW]	90.0000	90.0000	90.0000	90	90.0000	90.0000
P2,15[MW]	90.0000	90.0000	90.0000	90	90.0000	200.0000
P2,16[MW]	90.0000	90.0000	90.0000	90	143.5606	90.0000
P2,17[MW]	25.0000	25.0000	25.0000	25	25.0000	25.0000
P2,18[MW]	25.0000	25.0000	25.0000	25	25.0000	25.0000
P2,19[MW]	25.0000	25.0000	25.0000	25	25.0000	25.0000
P2,20[MW]	242.0000	242.0000	242.0000	242	242.0000	242.0000
Pw[MW]	330	330	330	330	330	330
Fc[\$/h]	106104.2224	111354.5625	117996.8615	118687.8507	121485.3538	121665.9732
Pl[MW]	-					
Et[Kg/h]	99759.4099	99968.6527	111461.7101	111791.3554	115512.0981	112105.2725
CEED[Kg/h]	184679.0933	197631.2948	217073.7455	219149.4535	224408.7740	225669.8748

The wind-thermal multi-area economic emission dispatch problem using the PSO algorithm in relation to other optimization algorithms, the Salp Swarm Algorithm(SSA), the Flower Pollination Algorithm(FPA), and the Backtracking Search Algorithm(BSA) (Alli, 2024), and Hybridizing Sum-Local Search Optimize (HLSO)(Chaudhary et al., 2020) and are given in Table 6.8.

Table 6.8: MAWTEED using PSO in relation to other optimization algorithms applied 40-unit system, PD = 10500[MW]

Algorithm	SSA	FPA	BSA	HLSO	Developed LMM 330[MW] wind power	Developed PSO 330MW wind power
Reference	(Alli.,2024)			(Chaudhary.,2020)		
P1,1[MW]	113.9998	97.4000	97.3999	110.8012	114.0000	114.0000
P1,2[MW]	113.9996	179.7331	179.7331	113.9997	114.0000	114.0000
P1,3[MW]	120	87.7999	87.7999	120.0	120.0000	60.0000
P1,4[MW]	179.73331	105.3999	105.3999	179.7331	184.4384	190.0000
P1,5[MW]	96.0324	300	259.5996	95.551	97.0000	97.0000
P1,6[MW]	140	284.5997	284.5996	140.0	140.0000	140.0000
P1,7[MW]	300	295.3663	284.5997	300.0	300.0000	300.0000
P1,8[MW]	284.5995	279.5997	204.7997	284.5997	300.0000	300.0000
P1,9[MW]	284.6002	94	94	284.5997	300.0000	300.0000
P1,10[MW]	269.9999	94	94	270.0	194.2785	300.0000
P1,11[MW]	168.7999	214.7598	304.5195	94.0	239.9567	375.0000
P1,12[MW]	350.0002	394.2794	394.2793	300.0	238.2515	375.0000
P1,13[MW]	394.2794	394.2794	394.2793	304.5195	326.5568	500.0000
P1,14[MW]	394.2793	394.2794	394.2793	394.2797	359.8966	500.0000
P1,15[MW]	304.5197	489.2794	489.2794	484.0395	358.8979	500.0000
P1,16[MW]	484.0391	399.5196	489.2793	484.0391	358.8979	500.0000
P1,17[MW]	489.2794	511.2794	511.2794	489.2794	500.0000	500.0000
P1,18[MW]	489.2796	511.2794	511.2793	489.2796	500.0000	500.0000
P1,19[MW]	511.2794	511.2794	523.2794	549.9998	550.0000	550.0000
P1,20[MW]	511.2793	511.2794	523.2794	511.2791	550.0000	550.0000
P2,1[MW]	523.2795	523.2794	523.2794	523.2792	477.1028	301.2412
P2,2[MW]	343.7598	523.2794	523.2793	523.2791	476.5912	254.0000
P2,3[MW]	254	523.2794	523.2794	523.2794	478.2959	254.0000
P2,4[MW]	523.2794	523.2794	523.2794	523.2794	478.2959	254.0000
P2,5[MW]	523.2793	10	10	523.2795	453.0060	254.0000
P2,6[MW]	523.2793	10	10	254.0	453.0060	254.0000
P2,7[MW]	109.9999	10	10	10.0001	11.0158	10.0000
P2,8[MW]	109.9999	87.7999	87.7999	10	11.0158	10.0000
P2,9[MW]	110	190	190	10	11.0158	10.0000
P2,10[MW]	87.7998	190	190	87.7997	97.0000	97.0000
P2,11[MW]	159.733	190	190	188.5959	477.1028	190.0000
P2,12[MW]	159.733	200	196.9619	159.7331	476.5912	189.4034
P2,13[MW]	159.7331	164.7999	164.7998	159.733	478.2959	125.3571
P2,14[MW]	90	164.7999	164.7998	164.8002	478.2959	90.0000
P2,15[MW]	164.8	110	109.9997	164.7998	453.0060	200.0000
P2,16[MW]	164.8	110	89.1141	164.7998	453.0060	90.0000
P2,17[MW]	72.296	110	109.9997	89.1143	11.0158	25.0000
P2,18[MW]	89.114	511.2794	511.2793	89.114	11.0158	25.0000
P2,19[MW]	89.114	550	549.9992	89.1134	11.0158	25.0000
P2,20[MW]	242	550	550	242.0001	97.0000	242.0000
Pw[MW]	-	-	-	-	282.5545	330
Fc[\$/h]	120857.2447	130573.2847	130580.7421	125100.2621	120069.1486	121665.9732
%Deviation of Fc for LMM in relation to the literature	0.166732	1.76565	1.76707	0.69586	0.330284	0.945119
PL[MW]					-	
ET[Kg/h]					79614.2253	112105.2725
CEED[Kg/h]	-	-	-	-	214795.2613	225669.8748

Figure 6.6 shows the relationship between the fuel cost [\$/h] and the power demand [MW] for several optimisation methods.

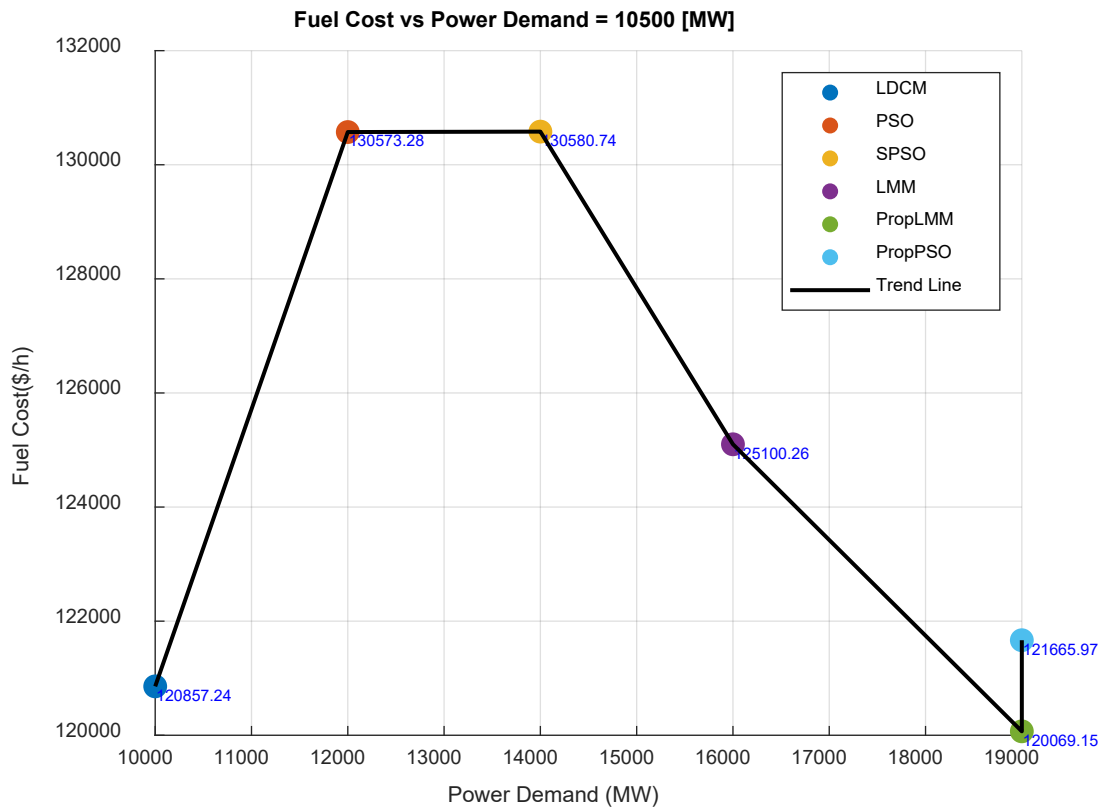


Figure 6.6: Values of fuel cost and power demand for the MAWTEED problem applied to PSO with a 40-unit system

As shown in Table 6.9, the fuel cost and emission figures are further compared with the statistical results for various algorithms.

Table 6.9: Relation of PSO with various algorithms (Ahmed et al., 2022)

Algorithm	Best cost (\$/h)	Best cost (%) Deviation	Best Emission (Kg/h)	Best Emission (%) Deviation
ABC	126 480.56	0.97011	209285.74	15.1187
EMA	125910.69	0.85725	210238.19	15.2218
NSGA-II	125830.00	0.84123	210950.00	15.2984
SSA-WSA	125760.05	0.82733	206705.97	14.8365
MOSSA	125591.29	0.79377	205965.40	14.7546
CSOA	124330.50	0.54158	116560.5	0.97418
Developed LMM	120069.1486	0.330284	79614.2253	8.47359
Developed PSO	121665.9732	0.80521	112105.2725	12.7007

The best fuel [\$/h] and emission [Kg/h] values for different optimization algorithms are compared with those of the PSO algorithm, as shown in Table 6.11 above. The best emission values are plotted against power demand [MW] as illustrated in Figure 6.7 below.

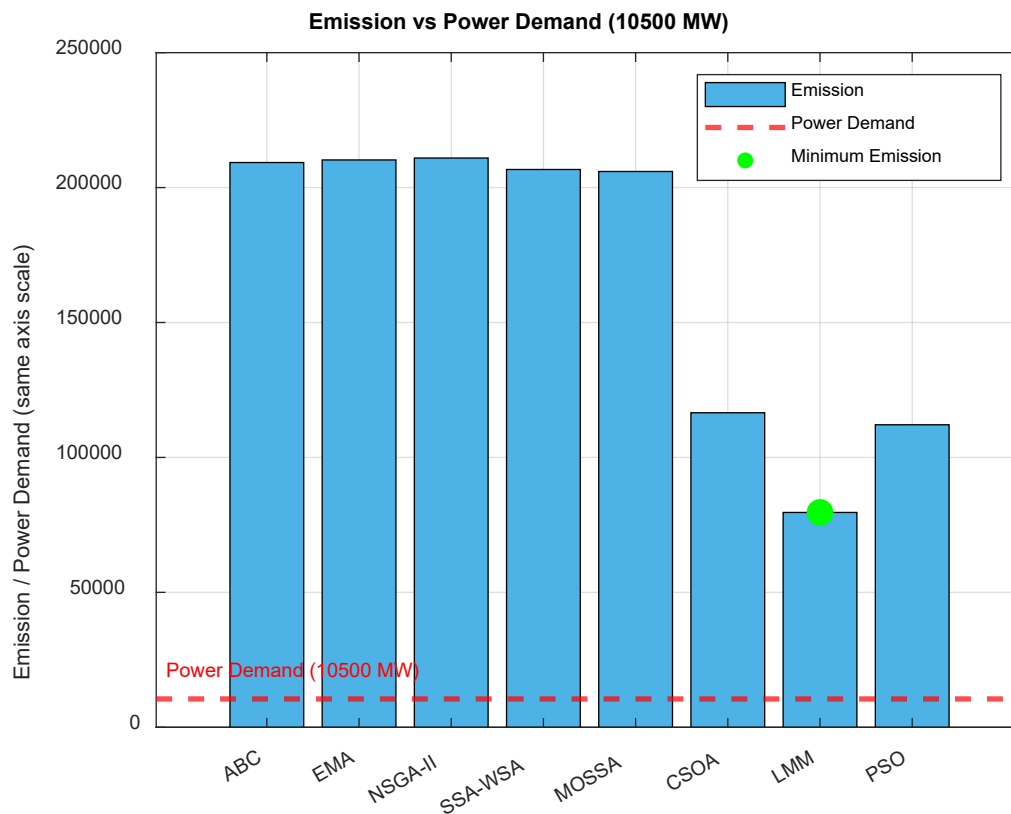


Figure 6.7: Emission versus power demand for the bi-criteria dispatch problem using PSO for a 40-unit system

6.4.3.1 The MAWTEED problem results and discussion for the 40-Unit System

The studied system includes a fourth generating unit to illustrate the effectiveness of the PSO algorithm compared to other optimization methods in minimizing fuel costs and emissions. The parameters used for the PSO algorithm are as follows. Swarm Size is 100, maximum number of iterations is 1000, initial weight w is 0.9, and c_1 , c_2 are both 2. The PSO algorithm is compared with different heuristic algorithms, i.e., Salp Swarm Algorithm (SSA), Flower Pollination Algorithm (FPA), and Backtracking Search Algorithm (BSA) (Alli, 2024), and Hybridizing Sum-Local Search Optimize (HLSO)(Chaudhary et al., 2020). The comparison is made based on the best cost and lowest emissions. The summary of the comparison between the PSO algorithm and the mentioned heuristic algorithms is given in Table 6.11.

Table 6.11 shows that the PSO values for fuel cost and emission minimization are 1% and 13% better, respectively, than those for the MAWTEED problem.

6.5 Conclusions

In this chapter, a Multi-Area Wind-Thermal Economic Emission Dispatch problem is solved using the PSO. Fuel and emission costs are minimised in the bi-objective problem of economic emission dispatch optimisation. This chapter presents the

transmission line losses, emissions, and inequality limits. Three test systems: a 6-unit system with two areas, a 12-unit system with four areas, and a 40-unit system with two areas are used to evaluate the algorithm. Compared to other methods, the fuel cost for 6-unit systems is 1-5% cheaper. Additionally, compared with previous optimisation techniques, the 12-unit system's fuel cost and emissions are 1-6% and 1-12%, respectively. Lastly, fuel consumption and emissions for the 40-unit system have been decreased by 1% and 1-14%, respectively.

By carefully selecting the PSO parameters w , c_1 , c_2 , population size, and number of iterations, the procedure efficiently converges to an optimal solution. The fuel and emissions for the MAWTEED problem are affected by the random selection of PSO variables, and the resulting LMM and PSO values differ by 1% across all test systems. The optimal requirements for the 6-unit, 12-unit, and 40-unit systems, however, remain within the anticipated ranges for fuel cost, emissions, and total generation in the MAWTEED problem when compared to the literature. Compared to the heuristic methods described in the literature, the classical Lagrange approach utilising decomposition coordination can easily produce optimal results for fuel and emission reduction. For simple convex instances, Lagrange's traditional techniques are practical and precise.

The PSO algorithm can solve the MAWTEED problem better than the Lagrange method when the objective function and constraints are nonlinear and nonconvex.

CHAPTER SEVEN

CONCLUSION AND FUTURE RECOMMENDATIONS

7.1 Introduction

This thesis explores wind energy in the current grid to reduce emissions and generation costs. Relative works are as follows: relative contributions to the findings of chapter 2 of how literature's value of the problem differs from the results of the WTEED single-area (chapter 3) and multi-area (subsequent chapters 4) problems solved by efforts from this thesis. The WTEED single-area problem is solved in Chapter 3 using Lagrange multipliers, and in Chapter 4 using PSO, both of which are compared with the literature. The WTEED multi-area problem is solved in Chapter 5 using Lagrange multipliers, and in Chapter 6 using PSO, both of which are compared with the literature. This conclusion provides an overview synthesis of such efforts for both implementing wind energy in the current grid for reduced emissions and costs and is broken down as follows: Section 7.1, Aims and Objective, Section 7.2, Study Contribution, Section 7.3, Findings and Application, Section 7.4, Suggestions for Future Studies, and Section 7.5, Author's Note for paper publication for clarity.

7.2 Research aim and objectives

7.2.1 Research Aim

To enhance the wind-thermal economic emission dispatch problem with formulations and algorithms, and solve it for single-area and multi-area systems. To provide a decomposition-coordinating solution to the dispatch problem via Lagrange's method. Software operates sequentially on one computer.

7.2.2 Objectives

- To review the literature of already existing formulations, methods, and algorithms of wind-thermal, wind-diesel, wind-PV, and hydrothermal economic dispatch problems.
- To formulate the wind-thermal economic emission dispatch problem with constraints for the single-area power system.
- To formulate the wind-thermal economic dispatch problem with constraints for the multi-area power system.
- To formulate LaGrange's method for the wind-thermal economic dispatch problem for single and multi-area power systems.
- To formulate the PSO method for the wind-thermal economic dispatch problem for single and multi-area power systems.
- To construct MATLAB software for LaGrange's and PSO methods for the wind-thermal economic dispatch problem for the single area power systems.

- To construct MATLAB software for LaGrange's and PSO methods for the wind-thermal economic dispatch problem for the multi-area power systems based on decomposition.
- To test the constructed software on standard IEEE benchmark systems and compare the obtained solutions with existing solutions in the literature.

7.3 The deliverables of the thesis

7.3.1 A comparative review of the current methodologies for addressing the single-area and multi-area economic emission dispatch problem.

In Chapter Two, Various optimizations and algorithms for single-area and multi-area wind-thermal economic emission dispatch solutions are assessed. This study compares classical, heuristic, and hybrid optimization strategies and algorithms for economic emission dispatch problems in single- and multi-area systems. First, economic emission dispatch solutions for single and multi-area systems are comprehensively investigated and thereafter tabulated, starting with single-area WTEED, then hybrid, and finally multi-area economic emission dispatch solutions. For example, the studies are relative to the number of studies reported per year, the methods and algorithms used, and the literature review articles assessing single-area and multi-area emission dispatch with single-criterion and multi-criterion optimization for economic dispatch. The table assessing these articles goes even further, covering: System (wind, storage, coal, diesel, etc.); Objective function (single- or multi-objective); Constraints (equality and inequality); Algorithm; Software; Power systems used; and Real-world application.

7.3.2 Mathematical formulation of the economic dispatch problems

A formulation of the quadratic cost function and the Weibull Distribution Function (WDF) for single- and multi-area Wind-Thermal Economic Emission (WTEED) is explored to solve the WTEED for multi-criteria dispatch. Formulations for single- and multi-area dispatch are discussed in Chapters 3 and 5, respectively.

7.3.3 Optimisation methods developed to solve the economic emission dispatch problems

The Lagrange method for the single-area WTEED is derived in Chapter 3. The solution for multi-area WTEED is derived using the Lagrange Decomposition method from Chapter 5. AI optimization of Particle Swarm Optimization (PSO) to solve single-area WTEED is employed in Chapter 4, while PSO to solve multi-area WTEED is employed in Chapter 6. A comparison is made between the solutions derived in Chapters 3-6 and other methods in the literature applied to single- and multi-area dispatch problems..

7.3.4 Software development and implementation for the solution to the economic emission dispatch problem for both single and multi-area systems.

Software developed for practical implementation by engineers is based on Lagrange methods for single-area and multi-area decomposition-coordination in the Wind-Thermal Economic Emission Dispatch (WTEED). Software developed from PSO methods of solution for use by practical implementation engineers for single-area and multi-area WTEED problems. This software was designed as a solution to dispatch issues and was verified against standard IEEE benchmarks and compared with other solutions in the literature. The software for dispatching problems in single- and multi-area systems is presented in Tables 7.1 and 7.2.

Table 7.1: Developed programs for the solution of a single area WTEED problem

Type of functions used in the WTEED problem	Algorithm	Type of Benchmark/Network	Appendix Identification	MATLAB Identification
Quadratic cost, emission, and Weibull Distribution Functions	Lagrange	IEEE30 Bus 6-unit system	Appendix A1	WTEED_case6units.m
		IEEE30 Bus 10-unit system	Appendix A2	WTEED_case10units.m
		IEEE30 Bus 40-unit system	Appendix A3	WTEED_case40units.m
Quadratic cost, emission, and Weibull Distribution Functions	PSO	IEEE30 Bus 6-unit system	Appendix B1	WTEED_casePSO6units.m
		IEEE30 Bus 10-unit system	Appendix B2	WTEED_casePSO10units.m
		IEEE30 Bus 40-unit system	Appendix B3	WTEED_casePSO40units.m

The developed programs for a single-area WTEED problem are illustrated in Table 7.1.

Table 7.2: Developed programs for the solution of a multi-area WTEED problem

Type of functions used in the WTEED problem	Algorithm	Type of Benchmark/Network	Tie line	Appendix x Identity	MATLAB Identification
Quadratic cost, emission, and Weibull Distribution Functions	Lagrange	IEEE30 Bus 6-unit system (i) Two areas (ii) 3 Thermal units in each (iii) Wind power of 330MW	1	Appendix C1	MAWTEED_case6units.m
		IEEE30 Bus 12-unit system (i) Four areas (ii) 3 Thermal units in each (iii) Wind power of 330MW	6	Appendix C2	MAWTEED_case10units.m
		IEEE30 Bus 40-unit system (i) Two areas (ii) 20 Thermal units in each (iii) Wind power of 330MW	1	Appendix C3	MAWTEED_case40units.m
Quadratic cost, emission, and Weibull Distribution Functions	PSO	IEEE30 Bus 6-unit system (i) Two areas (ii) 3 Thermal units in each (iii) Wind power of 330MW	1	Appendix D1	MAWTEED_casePSO6units.m
		IEEE30 Bus 12-unit system (i) Four areas (ii) 3 Thermal units in each (iii) Wind power of 330MW	6	Appendix D2	MAWTEED_casePSO10units.m
		IEEE30 Bus 40-unit system (i) Two areas (ii) 20 Thermal units in each (iii) Wind power of 330MW	1	Appendix D3	MAWTEED_casePSO40units.m

The established programs for a multi-area WTEED problem are illustrated in Table 7.2 above.

7.4 Implementation of the thesis findings

Some industrial facilities with comparable features can use the created techniques, algorithms, and software applications with little adjustments, such as:

- Solve the Economic dispatch problem in both single and multiple area power systems.
- Enhancement of Power Systems Economic Dispatch Based on Coal and Wind Renewable Energy Sources.
- Economic dispatch Solutions for power grid energy management systems in national or regional control centers' decision-making.

- Apply the developed economic dispatch algorithm for distributed and parallel power system network optimization.
- Apply the developed optimization methods in postgraduate research and educational courses
- Develop a framework for Smart Grids by solving the combined wind-coal economic dispatch problem.

7.5 Future research

Potential advances can be listed as follows:

- Applying the created techniques, algorithms, and programs for demand response, electric vehicles (EVs), hydro, wind, solar, storage, and pumped storage systems.
- Application development, programming, and solution implementation to the multi-area dispatch problem using a Cluster of Computers.
- More heuristic algorithms can be implemented and tested more efficiently to achieve the global optimum of the WTEED problems.
- Proposed algorithms can be implemented in a looped optimisation of the dispatch problem using CC and RTDS with a real-time lab open to network connectivity.
- Validate the developed application on larger IEEE systems.

7.6 Publications

Mbangeni, L., & Krishnamurthy, S. (2025). A Lagrange-Based Multi-Objective Framework for Wind-Thermal Economic Emission Dispatch. *MDPI(Processes)*, 13(9), 2814. <https://doi.org/10.3390/pr13092814>

Mbangeni, L., & Krishnamurthy, S. (2026). Performance Assessment of Particle Swarm Optimization for Wind Thermal_Economic_Emission_Dispatch submit to *Optimisation and Engineering*, Springer, Journal (Under Review) in February 2026

Mbangeni, L., & Krishnamurthy, S. (2026). Implementation of the Lagrange decomposition Method for solution of the Multi-Area Wind-Thermal Economic Emission Dispatch (MAWTEED) problem submitted to *Results in Control and Optimization Journal*(Under Review) in February 2026.

Mbangeni, L., & Krishnamurthy, S. (2026). Multi-area wind-thermal economic dispatch problem using the PSO Method, Anticipated to submit to *Power and Energy Conversion Journal* in February 2026.

7.7 Conclusion

The goals and objectives of the thesis, as well as the deliverables for developing techniques, algorithms, and software for single and multi-area wind-thermal economic emission dispatch problems, are outlined in this chapter. The chapter offers recommendations on customising software, algorithms, and the proposed dispatch problem technique for use in utility applications. A list of the author's publications and the direction of future study is provided.

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APPENDICES

APPENDIX A: DEVELOPED MATLAB PROGRAM FOR A SINGLE AREA WTEED PROBLEM USING LAGRANGE'S ALGORITHM

APPENDIX A1: MATLAB script file – WTEED_case6units.m

```
% M-File : WTEED_cases6units.m
% IEEE 30 bus SIX GENERATOR SYSTEM
% =====M-File Description=====
% The M-File is used to solve WTEED problem using Lagrange's Algorithm
clearvars, clc
tic;
global lambda PTmin PTmax n a b c d e f B B01 B00 h;
propmt='Enter the Power demand value (in MW)= ';
PD = input(propmt);
%=====Fuel cost coefficients=====
a=[10 10 20 10 20 10];
b=[200 150 180 100 180 150];
c=[100 120 40 60 40 100];
%=====Emission coefficients=====
d=[4.091 2.543 4.258 5.326 4.258 6.131];
e=[-5.554 -6.047 -5.094 -3.55 -5.094 -5.555];
f=[6.49 5.638 4.586 3.38 4.586 5.151];
Wmin = 1;
Wmax = 200;
nW = 1;
%===== Transmission loss coefficients=====
B00=[0.0014];
B01=[0.010731 1.7704 -4.0645 3.8453 1.3832 5.5503]*10.^(-3);
B=[ 0.0218 0.0107 -0.00036 -0.0011 0.00055 0.0033
0.0107 0.01704 -0.0001 -0.00179 0.00026 0.0028
-0.0004 -0.0002 0.02459 -0.01328 -0.0118 -0.0079
-0.0011 -0.00179 -0.01328 0.0265 0.0098 0.0045
0.00055 0.00026 -0.0118 0.0098 0.02616 -0.0001
0.0033 0.0028 -0.00792 0.0045 -0.00012 0.0297];
%===== Generator limits in per unit scale=====
PTmin=[0.05 0.05 0.05 0.05 0.05 0.05];
PTmax=[0.5 0.6 1.0 1.2 1.0 0.6];
%=====Initial values of Lagrange's algorithm=====
n=6; % Number of generators
lambda=200; % Initial Lambda
PT=[0.50 0.20 0.2 0.10 0.10 0.12];% Initial Real Powers
m=8000; % Total number of iterations
epsilon=0.01; % Tolerance Value
varepsilon=0.1; % Tolerance value of deltalambda
%=====Wind power modeling using Weibull =====
windData = [ 9.891 10.785 6.861 14.482 12.184 4.602];% wind speed data
v0 = windData';vbins = 0:0.5:max(windData)+1;
pdwind = fitdist(v0,'weibull');
prated = 7.88*10^6;vin =3; vr =12;vout=25;
pwwbins = zeros(size(vbins));
pwwbins(vbins>=vin & vbins<vr) = prated*(vbins(vbins>=vin & vbins<vr).^2-
vin^2)/(vr^2-vin^2);
pwwbins(vbins>=vr & vbins<=vout)= prated;
pdfv = pdf(pdwind,vbins);
avgpower = trapz(vbins,pdfv.*pwwbins);
pwd = (avgpower/1e6); %Power of each wind power unit
nWindunits = input('Enter number of wind generating units (MW) = ');
if isempty(nWindunits),nWindunits = 0;
end
TotalwindPower = (nWindunits*pwd)/100;
```

```

fprintf('Available wind = %.3f MW\n',TotalwindPower);
TotalwindPower = max(Wmin,min(TotalwindPower,Wmax));
%% COST FUNCTION
% actualpw=TotalwindPower*1e6;
% schedw= 0.8*PD*1e6;
% %cwi=1.75;% direct cost coefficient
% cpw=1;% Penalty cost coefficient for over generation
% crw=3.1;% reserve cost coefficient for under generation
% % dCost = cwi*actualpw;% Direct cost of wind power.
% % This factor exists only if the wind farm is not owned by the grid
% % operator.
% UE = cpw*(actualpw-schedw);% Underestimation of wind power
% OE = crw*(schedw-actualpw); % overestimation of wind power
% cost2= (UE + OE)/10^6; % Cost of wind power due to both
% for i=1:nW
% if cost2(i)<=Wmin(i)
% cost2(i)=Wmin(i);
% elseif cost2(i)>=Wmax(i)
% cost2(i)=Wmax(i);
% else cost2(i)=cost2(i);
% end
% end
%=====Lagrange's algorithm starts here=====
for iter=1:m
iter
% =====To solve the WTEED Problem using Lagrange's
algorithm=====
fsolve(@WTEED_Casestudy1_funct,PT)
PT=ans;
% P = PT + cost2*10^(-2)
P = PT + TotalwindPower*10^(-2)
% P = max(PTmin,min(P,PTmax));
%=====Checking of generator limits=====
for i=1:n
if P(i)<=PTmin(i);
P(i)=PTmin(i);
elseif P(i)>=PTmax(i);
P(i)=PTmax(i);
else P(i)=P(i);
end
end
%===== Calculation of Transmission loss=====
PL1=B00;
PL2=zeros(1,n);
for i=1:n
PL2(i)=(B01(i)*P(i));
end
PL2=sum(PL2(:,:));
PL3=zeros(n,n);
for i=1:n
for j=1:n
PL3(i,j)=P(i)*B(i,j)*P(j);
end
end
PL3=sum(PL3(:,:));
PL3=sum(PL3(:,:));
PL=PL1+PL2+PL3;
%===== Calculation of deltalambda=====
deltalambda=PD+PL-sum(P(:,:))
if abs(deltalambda)<=epsilon | iter>=m
break
else lambda=lambda+(deltalambda);

```

```

end
end
% =====Lagrange's algorithm ends here=====
%===== Pre-allocation of fuel cost, emission and CEED=====
fuelcost=zeros(1,n);
emissioncost=zeros(1,n);
CEED=zeros(1,n);
%===== Calculation of fuel cost, emission and CEED=====
for i=1:n
fuelcost(i)=(10.^(-2)*c(i)*P(i)^2+b(i)*P(i)+a(i));
emissioncost(i)=(10.^(-2))*(f(i)*P(i)^2+e(i)*P(i)+d(i));
CEED(i)=(c(i)*P(i)^2+b(i)*P(i)+a(i))+h(i)*(10.^(-
2))*(f(i)*P(i)^2+e(i)*P(i)+d(i));
end
%===Printing of Real power, Transmission loss, Fuel cost, Emission and
CEED===
totalfuelcost=sum(fuelcost(:, :))
totalemissioncost=sum(emissioncost(:, :))
CEED=sum(CEED(:, :))
iter
%=====Results=====
fprintf('\n=====Final Dispatch
results=====\n');
fprintf('Total Demand PD = %.3f MW\n', PD)
fprintf('Total Wind Supply TotalWindPower = %.3f MW\n', TotalwindPower)
fprintf('Sum of thermal generators = %.3f MW\n', sum(P))
fprintf('Transmission loss PL = %.3f MW\n', PL)
fprintf('Checking Power Balance (PD + PL-(Sumthermal + Pwind)) = %.6f
MW\n', PD+PL-(sum(P)+TotalwindPower));
fprintf('-----\n');
for i =1:n
    fprintf(' P(%d) = %8.4f(min %.2f, max %.2f)\n', i,
P(i),PTmin(i),PTmax(i))
end
toc
%%=====
% M-File: WTEED_Casestudy1_funcnt.m
% IEEE 30 bus system
% =====M-File Description=====
% The function is used to calculate the real power using Lagrange's
Algorithm

function F = WTEED_Casestudy1_funcnt(PT)
global lambda PTmin PTmax n a b c d e f B B01 h ;
%===== Calculation of price penalty factors (h)=====
h=zeros(1,n); % Pre-allocation of price penalty factor (h)
for i=1:n
h(i)=(c(i)*PTmin(i)^2+b(i)*PTmin(i)+a(i))/((f(i)*PTmax(i)^2+e(i)*PTmax(i)+d
(i)));
end
%===== Calculation of real power of the generators=====
for i=1:n
for j=1:n
F(i)=((2*c(i)*PT(i)+b(i))+2*h(i)*f(i)*PT(i)+(h(i)*e(i))+lambda*(2*PT(j)*B(
i,j)+B01(i))))-lambda;
end
end
end
%=====

```

APPENDIX A2: MATLAB script file – WTEED_case10units.m

```
% M-File : WTEED_case10units.m
%IEEE 118 BUS SYSTEM WITH TEN GENERATOR SYSTEM.
%The study focuses on 2000MW power demand as presented in (Mishra and
Shaik, 2024)
% The line data, fuel cost coefficients and emission co-efficients are also
% take from the above reference.
% =====M-File Description=====
% The M-File is used to solve WTEED Problem with using Lagrange's Algorithm
clear
clc;
tic;
% ==Economic dispatch problem including losses and generator limits==
% =====Initial Lagrange's variable=====
% lambda=-500; % Initial lambda
propmt='Enter the estimated value of lambda = ';
lambda = input(propmt);
epsil=0.001; % Tolerance value
alfa=0.001; % Incremental deltalambda
n=10; % No of thermal genrators
m=3000; % Total number of iterations
propmt='Enter the Power demand value (in MW)= ';
PD = input(propmt);

% =====Fuel cost coefficients and Emission Coefficients
=====
Data=[1000.403    40.5407    0.12951    360.0012    -3.9864    0.04702    10
55;
950.606    39.5804    0.10908    350.0056    -3.9524    0.04652    20    80;
900.705    36.5104    0.12511    330.0056    -3.9023    0.04652    47    120;
800.705    39.5104    0.12111    330.0056    -3.9023    0.04652    20    130;
756.799    38.5390    0.15247    13.8593    0.3277    0.00420    50    160;
451.325    46.1592    0.10587    13.8593    0.3277    0.00420    70    240;
1243.531    38.3055    0.03546    40.2669    -0.5455    0.00680    60    300;
1049.998    40.3965    0.02803    40.2669    -0.5455    0.00680    70    340;
1658.569    36.3278    0.02111    42.8955    -0.5112    0.00460    135    470;
1356.659    38.2704    0.01799    42.8955    -0.5112    0.00460    150    470];
% =====Fuel cost coefficients=====
a=Data(:,3);
b=Data(:,2);
c=Data(:,1);
% ===== Emission Coefficients=====
d=Data(:,6);
e=Data(:,5);
f=Data(:,4);
%=====Generator Limits =====
PTmin=Data(:,7);
PTmax=Data(:,8);
nW = 1;
Wmax = 500;
Wmin = 1;
% =====Transmission loss coefficients=====
B00=0.0055;
B01 = 10^-2.*[0.1 -0.2 -2.8 -0.1 0.1 -0.3 -0.2 -0.2 0.6 3.9]';
B= [0.000049 0.000014 0.000015 0.000015 0.000016 0.000017 0.000017 0.000018
0.000019 0.000020
0.000014 0.000045 0.000016 0.000016 0.000017 0.000015 0.000015 0.000016
0.000018 0.000018
0.000015 0.000016 0.000039 0.000010 0.000012 0.000012 0.000014 0.000014
0.000016 0.000016
```

```

0.000015 0.000016 0.000010 0.000040 0.000014 0.000010 0.000011 0.000012
0.000014 0.000015
0.000016 0.000017 0.000012 0.000014 0.000035 0.000011 0.000013 0.000013
0.000015 0.000016
0.000017 0.000015 0.000012 0.000010 0.000011 0.000036 0.000012 0.000012
0.000014 0.000015
0.000017 0.000015 0.000014 0.000011 0.000013 0.000012 0.000038 0.000016
0.000016 0.000018
0.000018 0.000016 0.000014 0.000012 0.000013 0.000012 0.000016 0.000040
0.000015 0.000016
0.000019 0.000018 0.000016 0.000014 0.000015 0.000014 0.000016 0.000015
0.000042 0.000019
0.000020 0.000018 0.000016 0.000015 0.000016 0.000015 0.000018 0.000016
0.000019 0.000044];
%=====Parameters for wind Power calculations=====
data =[9.891 10.785 6.861 14.482 12.184 4.602 7.232 8.036 12.333 11.074
10.040];
v0= data';
vbins=0:0.5:max(data)+ 1;
%=====weibull data distribution=====
pdwind = fitdist(v0, 'weibull');
prated=5.429*10^6;
vin=5;
vr=15;
vout=45;
%=====wind velocity constraint=====
pwvbins = zeros(size(vbins));
powercurve = (vbins>vin)&(vbins<vr);
pwvbins(powercurve) = prated*(vbins(powercurve).^2 - vin^2)./(vr^2-vin^2);
pwvbins(vbins>vr&vbins<=vout)=prated;
%=====wind power calculation=====
pdfv=pdf(pdwind,vbins);
avgpower=trapz(vbins,pdfv.*pwvbins);
pwd=(avgpower/(10^6));
nWindunits =input('Enter the number of available wind generators = ');
if isempty(nWindunits)|| nWindunits < 0
nWindunits = 0;
end
TotalwindPower =nWindunits*pwd;% Total wind Power from available wind
generators
fprintf('\n\n=====');
fprintf('\n The average wind Power available is = %8.3f
Megawatts\n',TotalwindPower);
fprintf('=====');
if TotalwindPower<Wmin
TotalwindPower=Wmin;
elseif TotalwindPower>Wmax
TotalwindPower=Wmax;
end
% end
% =====Calculation of Price Penalty factor=====
h=((a.*PTmax.^2+b.*PTmax+c))./((d.*PTmax.^2+e.*PTmax+f));
%=====Intial Power and min/max
limit=====
P = min(max((PD-TotalwindPower)/n*ones(n,1),PTmin),PTmax);
%=====Lagrange's algorithm starts here =====
for iter=1:m
WG = P + (TotalwindPower/n);
PL = B00 + B01'*WG + WG'*B*WG;
deltalambda=PD+PL-(sum(P)+ TotalwindPower);
if mod(iter,500)==0

```

```

fprintf('iter %d:deltalambda = %.6f MW, lambda = %.6f\n',iter,
deltalambda,lambda)
end
if abs(deltalambda)<=epsil
fprintf('\nSolution at iter %d with deltalambda = %.6f
MW\n',iter,deltalambda)
break;
end
% =====Calculation of generator real PTower =====
PT = (lambda - (b+h.*e))./(2.*(a+h.*d));
max(PTmin,min(PTmax,PT));%Generator limit checking
P = PT;
lambda = lambda+alfa*deltalambda;
if lambda <=0
lambda = epsil;
end
if iter == m
warning('Maximum iterations reached without solution. Final deltalambda =
%.6f MW',deltalambda);
end
WG = P + (TotalwindPower/n);
PL = B00 + B01'*WG + WG'*B*WG;
%=====
end
%===== Calculation of fuel cost, emission and CEED values =====
fuelcost=sum(a.*(P.^2)+b.*P+c);
emissioncost= sum(d.*(P.^2)+e.*P+f);
CEED= fuelcost+sum(h.*(d.*(P.^2)+e.*P+f));
%=====cost function for wind power=====
%=====Not considered in this simulation
actualpw=TotalwindPower*1e6;
schedw= 0.8*PD*1e6;
%cwi=1.75;% cost coefficient
cpw=1;% Penalty cost coefficient for over generation
crw=3.1;% reserve cost coefficient for under generation
%dCost = cwi*actualpw;
UE = cpw*(actualpw-schedw);
OE = crw*(schedw-actualpw);
cost2=(UE + OE)/10^6;
%=====
%=====Results=====
fprintf('\n=====Final Dispatch
results=====\n');
fprintf('Total Demand PD = %.3f MW\n', PD)
fprintf('Total Wind Supply TotalWindPower = %.3f MW\n', TotalwindPower)
fprintf('Sum of thermal generators = %.3f MW\n', sum(P))
fprintf('Transmission loss PL = %.3f MW\n', PL)
fprintf('Checking Power Balance (PD + PL-(Sumthermal + Pwind)) = %.6f
MW\n',PD+PL-(sum(P)+TotalwindPower));
fprintf('-----\n');
for i =1:n
fprintf(' P(%d) = %8.4f(min %.2f, max %.2f)\n',i, P(i),PTmin(i),PTmax(i))
end
fprintf('-----\n');
fprintf('Fuel cost = %.6f\n',fuelcost);
fprintf('Emission = %.6f\n',emissioncost);
fprintf('CEED (fuel+ penalty*emission) = %.6f\n',CEED);
fprintf('Wind reserve cost = %.6f\n',cost2);
fprintf('Total combined cost = %.6f\n',fuelcost + cost2);
fprintf('Iterations = %d\n',iter);

```

```

toc
%%=====
APPENDIX A3: MATLAB script file – WTEED_case40units.m
% M-File : WTEED_case40units.m
%IEEE 30 bus with 40 Units GENERATOR SYSTEM with wind power
%The simulation data for power limits, fuel cost coefficients,
%emission coefficients, and B-loss coefficients used in this test system
% are those used in (Secui et al.,2024). This program is used for the table
% 3.10 and 3.11. The wind power can be varied by changing the number of
% available wind turbines and rated wind power.
clearvars; close all; clc;
tic;
lambda = 8.9914;      % initial Lagrange multiplier
epsilon = 1e-3;      % convergence tolerance (MW)
alfa = 1e-3;        % lambda update step size
n = 40;              % number of thermal generators
m = 35000;          % max iterations
PD = input('Enter the Power demand value (in MW) = ');
% =====Fuel cost coefficients, Emission Coefficients, and limits of a
generator =====
data1 = [36      114    0.0069 6.73    94.705    0.048 -2.22 60
        36      114    0.0069 6.73    94.705 0.048 -2.22 60
        60      120    0.02028   7.07   309.54 0.0762 -2.36 100
        80      190    0.00942   8.18   369.03 0.054 -3.14 120
        47      97     0.0114 5.35   148.89 0.085 -1.89 50
        68      140    0.01142   8.05   222.33 0.0854 -3.08 80
        110     300    0.00357   8.03   287.71 0.0242 -3.06 100
        135     300    0.00492   6.99   391.98 0.031 -2.32 130
        135     300    0.00573   6.6    455.76 0.0335 -2.11 150
        130     300    0.00605   12.9   722.82 0.425 -4.34 280
        94      375    0.00515   12.9   635.2 0.0322 -4.34 220
        94      375    0.00569   12.8   654.69 0.0338 -4.28 225
        125     500    0.00421   12.5   913.4 0.0296 -4.18 300
        125     500    0.00752   8.84   1760.4 0.0512 -3.34 520
        125     500    0.00708   9.15   1728.3 0.0496 -3.55 510
        125     500    0.00708   9.15   1728.3 0.0496 -3.55 510
        220     500    0.00313   7.97   647.85 0.0151 -2.68 220
        220     500    0.00313   7.95   649.69 0.0151 -2.66 222
        242     550    0.00313   7.97   647.83 0.0151 -2.68 220
        242     550    0.00313   7.97   647.81 0.0151 -2.68 220];

data2 = [254     550    0.00298    6.63   785.96 0.0145 -2.22 290
        254     550    0.00298    6.63   785.96 0.0145 -2.22 285
        254     550    0.00284    6.66   794.53 0.0138 -2.26 295
        254     550    0.00284    6.66   794.53 0.0138 -2.26 295

        254     550    0.00277    7.1    801.32 0.0132 -2.42 310
        254     550    0.00277    7.1    801.32 0.0132 -2.42 310

        10      150    0.52124    3.33  1055.1 1.842 -1.11 360
        10      150    0.52124    3.33  1055.1 1.842 -1.11 360
        10      150    0.52124    3.33  1055.1 1.842 -1.11 360
        47      97     0.0114 5.35   148.89 0.085 -1.89 50
        60      190    0.0016 6.43   222.92 0.0121 -2.08 80
        60      190    0.0016 6.43   222.92 0.0121 -2.08 80
        60      190    0.0016 6.43   222.92 0.0121 -2.08 80
        90      200    0.0001 8.95   107.87 0.0012 -3.48 65
        90      200    0.0001 8.62   116.58 0.0012 -3.24 70
        90      200    0.0001 8.62   116.58 0.0012 -3.24 70
        25      110    0.0161 5.88   307.45 0.095 -1.98 100
        25      110    0.0161 5.88   307.45 0.095 -1.98 100

```

```

                25    110    0.0161 5.88    307.45 0.095 -1.98 100
242    550    0.00313    7.97    647.83    0.0151 -2.68 220];

```

```
data = [data1;data2];
```

```

%=====Generator Limits =====
Pmin=data(:,1);
Pmax=data(:,2);
Wmax = 2000;
Wmin = 1;
% =====Fuel cost coefficients=====
a=data(:,3);
b=data(:,4);
c=data(:,5);
% ===== Emission Coefficients=====
d=data(:,6);
e=data(:,7);
f=data(:,8);
% =====Transmission loss coefficients=====
B00=0.56;
B01=10^-4.*[-3.908 -1.297 7.047 0.591 2.161 -6.635 -3.908 -1.297 7.047...
            0.591 2.161 -6.635 -3.908 -1.297 7.047 0.591 2.161 -6.635...
            -3.908 -1.297 7.047 0.591 2.161 -6.635 -3.908 -1.297 7.047...
            0.591 2.161 -6.635 -3.908 -1.297 7.047 0.591 2.161 -6.635...
            -3.908 -1.297 7.047 0.591]';

```

```

B1_half=[17 12 7 -1 -5 -2 17 12 7 -1 -5
-2 17 12 7 -1 -5 -2 17 12
12 14 9 1 -6 -1 12 14 9 1 -6 -1
12 14 9 1 -6 -1 12 14
7 9 31 0 -10 -6 7 9 31 0 -10 -6
7 9 31 0 -10 -6 7 9
-1 1 0 24 -6 -8 -1 1 0 24 -6 -8
-1 1 0 24 -6 -8 -1 1
-5 -6 -10 -6 129 -2 -5 -6 -10 -6 129 -2 -5
-6 -10 -6 129 -2 -5 -6
-2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
-2 -1 -6 -8 -2 150 -2 -1
17 12 7 -1 -5 -2 17 12 7 -1 -5 -2
17 12 7 -1 -5 -2 17 12
12 14 9 1 -6 -1 12 14 9 1 -6 -1
12 14 9 1 -6 -1 12 14
7 9 31 0 -10 -6 7 9 31 0 -10 -6
7 9 31 0 -10 -6 7 9
-1 1 0 24 -6 -8 -1 1 0 24 -6 -8
-1 1 0 24 -6 -8 -1 1
-5 -6 -10 -6 129 -2 -5 -6 -10 -6 129 -2 -5
-6 -10 -6 129 -2 -5 -6
-2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
-2 -1 -6 -8 -2 150 -2 -1
17 12 7 -1 -5 -2 17 12 7 -1 -5 -2
17 12 7 -1 -5 -2 17 12
12 14 9 1 -6 -1 12 14 9 1 -6 -1
12 14 9 1 -6 -1 12 14
7 9 31 0 -10 -6 7 9 31 0 -10 -6 7
9 31 0 -10 -6 7 9
-1 1 0 24 -6 -8 -1 1 0 24 -6 -8
-1 1 0 24 -6 -8 -1 1

```

```

-5 -6 -10 -6 129 -2 -5 -6 -10 -6 129 -2 -5
-6 -10 -6 129 -2 -5 -6 -10 -6 129 -2 -5
-2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
-2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
17 12 7 -1 -5 -2 17 12 7 -1 -5 -2
17 12 7 -1 -5 -2 17 12 7 -1 -5 -2
12 14 9 1 -6 -1 12 14 9 1 -6 -1
12 14 9 1 -6 -1 12 14];

```

```

B2_half=[7 -1 -5 -2 17 12 7 -1 -5 -2 17
12 7 -1 -5 -2 17 12 7 -1 -5 -2 17
9 1 -6 -1 12 14 9 1 -6 -1 12 14
9 1 -6 -1 12 14 9 1 -6 -1 12 14
31 0 -10 -6 7 9 31 0 -10 -6 7 9
31 0 -10 -6 7 9 31 0 -10 -6 7 9
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-6 -8 -2 150 -2 -1 -6 -8 -2 150 -2 -1
-6 -8 -2 150 -2 -1 -6 -8 -2 150 -2 -1
7 -1 -5 -2 17 12 7 -1 -5 -2 17 12
7 -1 -5 -2 17 12 7 -1 -5 -2 17 12
9 1 -6 -1 12 14 9 1 -6 -1 12 14
9 1 -6 -1 12 14 9 1 -6 -1 12 14
31 0 -10 -6 7 9 31 0 -10 -6 7 9
31 0 -10 -6 7 9 31 0 -10 -6 7 9
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-6 -8 -2 150 -2 -1 -6 -8 -2 150 -2 -1
-6 -8 -2 150 -2 -1 -6 -8 -2 150 -2 -1
7 -1 -5 -2 17 10 -6 7 9 31 0 -10
-6 7 9 31 0 -10 -6 7 9 31 0 -10
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
0 24 -6 -8 -1 1 0 24 -6 -8 -1 1
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-10 -6 129 -2 -5 -6 -10 -6 129 -2 -5 -6
-6 -8 12 7 -1 -5 -2 17 12 7 -1 -5
-2 17 12 7 -1 9 31 0 -10 -6 -1 12 14
9 1 -6 -1 12 14 9 1 -6 -1 12 14
9 1 -6 -1 12 14 9 1 -6 -1 12 14
31 0 -2 150 -2 -1 -6 -8 -2 150 -2 -1
-6 -8 -2 150 -2 -1 -6 -8 -2 150 -2 -1
7 -1 -5 -2 17 12 7 -1 -5 -2 17 12
7 -1 -5 -2 17 12 7 -1 -5 -2 17 12
9 1 -6 -1 12 14 9 1 -6 -1 12 14
9 1 -6 -1 12 14 9 1 -6 -1 12 14

```

```

B3_half = [ 7 9 31 0 -10 -6 7 9 31 0
-10 -6 7 9 31 0 -10 -6 7 9 31 0
-8 -1 1 0 24 -6 -8 -1 1 0 24 -6
-8 -1 1 0 24 -6 -8 -1 1 0 24 -6
-5 -6 -10 -6 129 -2 -5 -6 -10 -6 129
-2 -5 -6 -10 -6 129 -2 -5 -6 -10 -6 129
-2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
150 -2 -1 -6 -8 -2 150 -2 -1 -6 -8 -2 150
-2 17 12 7 -1 -5 -2 17 12 7 -1 -5
-2 17 12 7 -1 -5 -2 17 12 7 -1 -5
12 14 9 1 -6 -1 12 14 9 1 -6
-1 12 14 9 1 -6 -1 12 14 9 1 -6

```

	79	31	0	-10	-6	7	9	31	0	-10	-6
7	9	31	0	-10	-6	7	9				
	-1	1	0	24	-6	-8	-1	1	0	24	-6
-8	-1	1	0	24	-6	-8	-1	1			
	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129
-2	-5	-6	-10	-6	129	-2	-5	-6			
	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2
150	-2	-1	-6	-8	-2	150	-2	-1			
	17	12	7	-1	-5	-2	17	12	7	-1	-5
-2	17	12	7	-1	-5	-2	17	12			
	12	14	9	1	-6	-1	12	14	9	1	-6
-1	12	14	9	1	-6	-1	12	14			
	79	31	0	-10	-6	7	9	31	0	-10	-6
7	9	31	0	-10	-6	7	9				
	-1	1	0	24	-6	-8	-1	1	0	24	-6
-8	-1	1	0	24	-6	-8	-1	1			
	-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129
-2	-5	-6	-10	-6	129	-2	-5	-6			
	-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2
150	-2	-1	-6	-8	-2	150	-2	-1			
	17	12	7	-1	-5	-2	17	12	7	-1	-5
-2	17	12	7	-1	-5	-2	17	12			
	12	14	9	1	-6	-1	12	14	9	1	-6
-1	12	14	9	1	-6	-1	12	14			
	79	31	0	-10	-6	7	9	31	0	-10	-6
7	9	31	0	-10	-6	7	9				
	-1	1	0	24	-6	-8	-1	1	0	24	-6
-8	-1	1	0	24	-6	-8	-1	1];			
B4_half =	31	0	-10	-6	7	9	31	0	-10	-6	
7	9	31	0	-10	-6	7	9	31	0		
	024	-6	-8	-1	1	0	24	-6	-8	-1	1
0	24	-6	-8	-1	1	0	24				
	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6			
	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2
-1	-6	-8	-2	150	-2	-1	-6	-8			
	7-1	-5	-2	17	12	7	-1	-5	-2	17	12
7	-1	-5	-2	17	12	7	-1				
	91	-6	-1	12	14	9	1	-6	-1	12	14
9	1	-6	-1	12	14	9	1				
	31	0	-10	-6	7	9	31	0	-10	-6	7
9	31	0	-10	-6	7	9	31	0			
	024	-6	-8	-1	1	0	24	-6	-8	-1	1
0	24	-6	-8	-1	1	0	24				
	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6			
	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2
-1	-6	-8	-2	150	-2	-1	-6	-8			
	7-1	-5	-2	17	12	7	-1	-5	-2	17	12
7	-1	-5	-2	17	12	7	-1				
	91	-6	-1	12	14	9	1	-6	-1	12	14
9	1	-6	-1	12	14	9	1				
	31	0	-10	-6	7	9	31	0	-10	-6	7
9	31	0	-10	-6	7	9	31	0			
	024	-6	-8	-1	1	0	24	-6	-8	-1	1
0	24	-6	-8	-1	1	0	24				
	-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6			
	-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2
-1	-6	-8	-2	150	-2	-1	-6	-8			

```

7       7-1   -5    -2    17    12    7     -1    -5    -2    17    12
7       -1   -5    -2    17    12    7     -1
9       91   -6    -1    12    14    9     1    -6    -1    12    14
9       1    -6    -1    12    14    9     1
9       31   0    -10   -6    7     9    31   0    -10   -6    7
9       31   0    -10   -6    7     9    31   0
0       024  -6    -8    -1    1     0    24  -6    -8    -1    1
0       24  -6    -8    -1    1     0    24];

```

```

B= 10^-6.*[B1_half B2_half;B3_half B4_half ];
%=====Parameters for wind Power calculations=====
data =[9.891 10.785 6.861 14.482 12.184 4.602 7.232 8.036 12.333 11.074
10.040];
v0= data';
vbins=0:0.5:max(data)+ 1;
%=====weibull data
distribution=====.
pdwind = fitdist(v0, 'weibull');
prated=5.429*10^6;
vin=5;
vr=15;
vout=45;
%=====wind velocity constraint=====
pwvbins = zeros(size(vbins));
powercurve = (vbins>vin)&(vbins<vr);
pwvbins(powercurve) = prated*(vbins(powercurve).^2 - vin^2)./(vr^2-vin^2);
pwvbins(vbins>vr&vbins<=vout)=prated;
%=====wind power calculation=====
pdfv=pdf(pdwind,vbins);
avgpower=trapz(vbins,pdfv.*pwvbins);
pwd=(avgpower/(10^6));
nWindunits =input('Enter the number of available wind generators = ');
if isempty(nWindunits)|| nWindunits < 0
nWindunits = 0;
end
TotalwindPower =nWindunits*pwd;% Total wind Power from available wind
generators
fprintf('\n\n=====')
);
fprintf('\n The average wind Power available is = %8.3f
Megawatts\n',TotalwindPower);
fprintf('=====');
if TotalwindPower<Wmin
TotalwindPower=Wmin;
elseif TotalwindPower>Wmax
TotalwindPower=Wmax;
end
% end
% =====Calculation of Price Penalty factor=====
h=((a.*Pmax.^2+b.*Pmax+c)./((d.*Pmax.^2+e.*Pmax+f)));
%=====Intial Power and min/max
limit=====
P = min(max((PD-TotalwindPower)/n*ones(n,1),Pmin),Pmax);
%=====Lagrange's algorithm starts here =====
for iter = 1:m
G = P + (TotalwindPower / n);
PL = B00 + B01' * G + G' * B * G;
deltalambda = PD + PL - (sum(P) + TotalwindPower);
if abs(deltalambda) <= epsilon
fprintf('\nConverged at iter %d: deltalambda = %.6f MW\n', iter,
deltalambda);
break;

```

```

end
PT = (lambda - (b + h.*e)) ./ (2 .* (a + h.*d));
PT = max(Pmin, min(Pmax, PT));
P = PT;
lambda = max(eps, lambda + alfa * deltalambda);
if mod(iter, 500) == 0
    fprintf('iter %d: mismatch = %.6f, lambda = %.6f\n', iter,
deltalambda, lambda);
end
end
if iter == m
warning('Max iterations reached. Final mismatch = %.6f MW', deltalambda);
end
end
%=====
%==== Calculation of fuel cost, emission and CEED values =====
G = P + (TotalwindPower / n);
PL = B00 + B01' * G + G' * B * G;
fuelCost = sum(a .* P.^2 + b .* P + c);
emissionCost = sum(d .* P.^2 + e .* P + f);
CEED = fuelCost + sum(h .* (d .* P.^2 + e .* P + f));
%=====
%====cost function for wind power=====
%====Not considered in this simulation
UE = 1*(TotalwindPower*1e6 - 0.8*PD*1e6);
OE = 3.1*(0.8*PD*1e6 - TotalwindPower*1e6);
windCost = (UE + OE) / 1e6;
%=====
%=====
%=====Results=====
fprintf('\n=== Results ===\n');
fprintf('PD = %.3f MW, Wind supply = %.3f MW, Thermal sum = %.3f MW\n', PD,
TotalwindPower, sum(P));
fprintf('Loss PL = %.6f MW\nBalance check: PD + PL - (th + wind) = %.6f
MW\n', PL, PD + PL - (sum(P) + TotalwindPower));
disp('--- Unit outputs ---');
for i = 1:n
fprintf('P(%2d) = %.4f MW (min %.2f, max %.2f)\n', i, P(i), Pmin(i),
Pmax(i));
end
fprintf('Fuel cost = %.6f\nEmission cost = %.6f\nCEED = %.6f\nWind cost
term = %.6f\nTotal cost = %.6f\n', ...
fuelCost, emissionCost, CEED, windCost, fuelCost + windCost);
fprintf('Iterations = %d\n', iter);
toc;

```

APPENDIX B: DEVELOPED MATLAB PROGRAM FOR A SINGLE AREA WTEED PROBLEM USING PSO ALGORITHM

APPENDIX B1: MATLAB script file – WTEED_casePSO6units.m

```

%This is IEEE30 bus system with 6 generating units. Named:
WTEED_casePSO6units.m.
% The program is created using a per unit scale. But table 4.1 is recreated
% back to normal scale.This program is used to create Table 4.1, and is
%also used in table 4.2. It is using a function called objective2.m
%
clearvars;clc; close all;tic;
%=====User to enter power demand of the system=====
PD = input('What is the Power demand in (MW)=');
n =6; %number of used generators
num_particles = 50;% number of particles in the population
maxIter = 1000; %Number of iterations
w = 0.9; c1 = 1.5; c2 = 1.5;
penaltyEmissionFactor = 10000;
powerBalancePenalty = 1000000;
printInterval = 10;
nW = 1;
Wmax = 500;
Wmin = 1;
%=====Fuel cost with valve point effect coefficients=====
a=[10 10 20 10 20 10]';
b=[200 150 180 100 180 150]';
c=[100 120 40 60 40 100]';
%% Emission with valve point effect coefficients
d=[4.091 2.543 4.258 5.326 4.258 6.131]';
e=[-5.554 -6.047 -5.094 -3.55 -5.094 -5.555]';
f=[6.49 5.638 4.586 3.38 4.586 5.151]';
Wmin = 1;
Wmax = 2000;
nW = 1;
Pmin=[0.05 0.05 0.05 0.05 0.05 0.05]';
Pmax=[0.5 0.6 1.0 1.2 1.0 0.6]';
% =====Transmission loss coefficients=====
B00=0.0014;
B01=[0.010731; 1.7704; -4.0645; 3.8453; 1.3832; 5.5503]*10.^(-3);
B=[ 0.0218 0.0107 -0.00036 -0.0011 0.00055 0.0033
    0.0107 0.01704 -0.0001 -0.00179 0.00026 0.0028
   -0.0004 -0.0002 0.02459 -0.01328 -0.0118 -0.0079
   -0.0011 -0.00179 -0.01328 0.0265 0.0098 0.0045
    0.00055 0.00026 -0.0118 0.0098 0.02616 -0.0001
    0.0033 0.0028 -0.00792 0.0045 -0.00012 0.0297];
%=====Parameters for wind Power calculations=====
data =[9.891 10.785 6.861 14.482 12.184 4.602 7.232 8.036 12.333 11.074
10.040];
v0= data';
vbins=0:0.5:max(data)+ 1;
%=====weibull data
distribution=====.
pdwind = fitdist(v0, 'weibull');
prated=11.429*10^6;
vin=5;
vr=15;
vout=45;
%=====wind velocity constraint=====
pwvbins = zeros(size(vbins));
powercurve = (vbins>vin)&(vbins<vr);
pwvbins(powercurve) = prated*(vbins(powercurve).^2 - vin^2)./(vr^2-vin^2);

```

```

pwvbins(vbins>=vr&vbins<=vout)=prated;
%=====wind power calculation=====
pdfv=pdf(pdwind,vbins);
avgpower=trapz(vbins,pdfv.*pwvbins);
pwd=(avgpower/(10^6));
nWindunits =input('Enter the number of available wind generators = ');
if isempty(nWindunits)|| nWindunits < 0
    nWindunits = 0;
end
TotalwindPower =nWindunits*pwd/100;% Total wind Power from available wind
generators
fprintf('\n\n=====')
);
fprintf('\n The average wind Power available is = %8.3f
Megawatts\n',TotalwindPower);
fprintf('=====');
TotalwindPower = max(Wmin,min(TotalwindPower,Wmax));
%=====
%%===== Initial variables of the PSO algorithm=====
dim = n; lb = Pmin; ub = Pmax;
vmax = 0.2*(ub-lb); vmin = -vmax;
X =zeros(num_particles,dim); V = zeros(num_particles,dim);
pbest = X; pbestVal =inf(num_particles,1); gbest = zeros(1,dim);gbestVal
=inf;
for i=1:num_particles
    X(i,:)=(lb+(ub-lb).*rand(dim,1))';
    V(i,:)= (vmin+(vmax-vmin).*rand(dim,1))';
[val,~]=objective2(X(i,:) ',PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyE
missionFactor,powerBalancePenalty);
    pbest(i,:)=X(i,:);
    pbestVal(i)=val;
    if val<gbestVal
        gbest=X(i,:);
        gbestVal = val;
    end
end
end
% =====Main loop of the PSO algorithm=====
for iter =1:maxIter
for i=1:num_particles
    r1 =rand(1,dim);r2 =rand(1,dim);
    V(i,:)=w*V(i,:)+c1*r1.*(pbest(i,:)-X(i,:))+c2*r2.*(gbest-X(i,:));
    V(i,:)=max(min(V(i,:),vmax'),vmin');
    X(i,:)=X(i,:)+V(i,:);
    X(i,:)=max(min(X(i,:),ub'),lb')
[val,~]=objective2(X(i,:) ',PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyE
missionFactor,powerBalancePenalty);
    if val<pbestVal(i), pbestVal(i)= val; pbest(i,:)= X(i,:);end
    if val<gbestVal,gbestVal = val; gbest = X(i,:);
    end
    if mod(iter,printInterval)==0
        fprintf('Iter %d CEED=%8.3f\n',iter,gbestVal);
    end
end
end
end
%=====Final evaluation of
variables=====
[Pcost,details]=objective2(gbest ',PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,p
enaltyEmissionFactor,powerBalancePenalty);
fprintf('\n=====Final PSO Dispatch (6units)=====');
for i=1:n
    fprintf(' P(%d)=%8.3f MW (min %8.1f max
%8.1f)\n',i,gbest(i),Pmin(i),Pmax(i))

```

```

end
fprintf('Sum Thermal=%.3f MW, Wind=%.3f MW, Loss=%.3f
MW\n',sum(gbest),TotalwindPower,details.PL)
    fprintf('Fuel Cost=%.3f , Emission=%.3f ,
CEED=%.3f\n',details.fuelcost,details.emission,Pcost);
toc;
% This function is called on the main program: WTEED_casePS06units for
calculation
% of PL,fuelcost,emission.
function
[cost,details]=objective2(P,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,k1,kpb)
    P =P(:); WG = P+(TotalwindPower/length(P));
    PL = B00+B01'*WG+WG'*B*WG; % Calculation of Power losses
    fuel=sum(a.*(P.^2)+b.*P+c); %calculation of fuel cost function
    em=sum((10.^(-2)).*(d.*(P.^2)+e.*P+f));% Emission calculation
    % em =sum((d.*(P.^2)+e.*P+f));
    CEED = fuel+k1*em;% Combined emission calculation
    % CEED = fuel+k1*em.*(10.^(-2));
    mismatch=PD+PL-(sum(P)+TotalwindPower); % Total power balance
    penalty=kpb*mismatch^2;
    cost =CEED+penalty;
    details.PL=PL;details.fuelcost=fuel;details.emission=em;% all values
that are defined
    % under details to be called on the main script file.
en

```

APPENDIX B2: MATLAB script file – WTEED_casePSO10units.m

```

%%=====Main program=====
%This is IEEE30 bus system with 10 generathing units. Named:
WTEED_casePSO10units.m.
% The program is used to create table 4.3 and also used in Table 4.4
% It is using a function called objective.m
clearvars;clc; close all;tic;
%=====User to enter power demand of the system=====
PD = input('What is the Power demand in (MW)=');
n =10; %number of used generators
num_particles = 40;% number of particles in the population
maxIter = 500; %Number of iterations
w = 0.7; c1 = 1.5; c2 = 1.5;
penaltyEmissionFactor = 1;
powerBalancePenalty = 1000000;
printInterval = 10;

% =====Fuel cost coefficients and Emission Coefficients
=====
Data=[1000.403    40.5407    0.12951    360.0012    -3.9864    0.04702    10
55;
    950.606    39.5804    0.10908    350.0056    -3.9524    0.04652    20
80;
    900.705    36.5104    0.12511    330.0056    -3.9023    0.04652    47
120;
    800.705    39.5104    0.12111    330.0056    -3.9023    0.04652    20
130;
    756.799    38.5390    0.15247    13.8593    0.3277    0.00420    50
160;
    451.325    46.1592    0.10587    13.8593    0.3277    0.00420    70
240;
    1243.531    38.3055    0.03546    40.2669    -0.5455    0.00680    60
300;
    1049.998    40.3965    0.02803    40.2669    -0.5455    0.00680    70
340;

```

```

1658.569  36.3278  0.02111  42.8955  -0.5112  0.00460  135
470;
1356.659  38.2704  0.01799  42.8955  -0.5112  0.00460  150
470];
% =====Fuel cost coefficients=====
a=Data(:,3);
b=Data(:,2);
c=Data(:,1);
% ===== Emission Coefficients=====
d=Data(:,6);
e=Data(:,5);
f=Data(:,4);
%=====Generator Limits =====
Pmin=Data(:,7);
Pmax=Data(:,8);
nW = 1;
Wmax = 500;
Wmin = 1;
% =====Transmission loss coefficients=====
B00=0.0055;
B01=10^-2.*[ 0.1 -0.2 -2.8 -0.1 0.1 -0.3 -0.2 -0.2 0.6 3.9]';
B= [ 0.000049 0.000014 0.000015 0.000015 0.000016 0.000017 0.000017
0.000018 0.000019 0.000020
0.000014 0.000045 0.000016 0.000016 0.000017 0.000015 0.000015 0.000016
0.000018 0.000018
0.000015 0.000016 0.000039 0.000010 0.000012 0.000012 0.000014 0.000014
0.000016 0.000016
0.000015 0.000016 0.000010 0.000040 0.000014 0.000010 0.000011 0.000012
0.000014 0.000015
0.000016 0.000017 0.000012 0.000014 0.000035 0.000011 0.000013 0.000013
0.000015 0.000016
0.000017 0.000015 0.000012 0.000010 0.000011 0.000036 0.000012 0.000012
0.000014 0.000015
0.000017 0.000015 0.000014 0.000011 0.000013 0.000012 0.000038 0.000016
0.000016 0.000018
0.000018 0.000016 0.000014 0.000012 0.000013 0.000012 0.000016 0.000040
0.000015 0.000016
0.000019 0.000018 0.000016 0.000014 0.000015 0.000014 0.000016 0.000015
0.000042 0.000019
0.000020 0.000018 0.000016 0.000015 0.000016 0.000015 0.000018 0.000016
0.000019 0.000044];
%=====Parameters for wind Power calculations=====
data =[9.891 10.785 6.861 14.482 12.184 4.602 7.232 8.036 12.333 11.074
10.040];
v0= data';
vbins=0:0.5:max(data)+ 1;
%=====weibull data
distribution=====.
pdwind = fitdist(v0, 'weibull');
prated=11.429*10^6;
vin=5;
vr=15;
vout=45;
%=====wind velocity constraint=====
pwvbins = zeros(size(vbins));
powercurve = (vbins>vin)&(vbins<vr);
pwvbins(powercurve) = prated*(vbins(powercurve).^2 - vin^2)./(vr^2-vin^2);
pwvbins(vbins>vr&vbins<=vout)=prated;
%=====wind power calculation=====
pdfv=pdf(pdwind,vbins);
avgpower=trapz(vbins,pdfv.*pwvbins);
pwd=(avgpower/(10^6));

```

```

nWindunits =input('Enter the number of available wind generators = ');
if isempty(nWindunits)|| nWindunits < 0
    nWindunits = 0;
end
TotalwindPower =nWindunits*pwd;% Total wind Power from available wind
generators
fprintf('\n\n=====')
);
fprintf('\n The average wind Power available is = %8.3f
Megawatts\n',TotalwindPower);
fprintf('=====');
TotalwindPower = max(Wmin,min(TotalwindPower,Wmax));
%% Initial variables of the PSO algorithm
dim = n; lb = Pmin; ub = Pmax;
vmax = 0.5*(ub-lb); vmin = -vmax;
X =zeros(num_particles,dim); V = zeros(num_particles,dim);
pbest = X; pbestVal =inf(num_particles,1); gbest = zeros(1,dim);gbestVal
=inf;
for i=1:num_particles
    X(i,:)=(lb+(ub-lb).*rand(dim,1))';
    V(i,:)= (vmin+(vmax-vmin).*rand(dim,1))';

[val,~]=objective(X(i,:) ,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyEm
issionFactor,powerBalancePenalty);
    pbest(i,:)=X(i,:);
    pbestVal(i)=val;
    if val<gbestVal
        gbest=X(i,:);
        gbestVal = val;
    end
end
% =====Main loop of the PSO algorithm=====
for iter =1:maxIter
for i=1:num_particles
    r1 =rand(1,dim);r2 =rand(1,dim);
    V(i,:)=w*V(i,:)+c1*r1.*(pbest(i,:)-X(i,:))+c2*r2.*(gbest-X(i,:));
    V(i,:)=max(min(V(i,:),vmax'),vmin');
    X(i,:)=X(i,:)+V(i,:);
    X(i,:)=max(min(X(i,:),ub'),lb');

[val,~]=objective(X(i,:) ,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyEm
issionFactor,powerBalancePenalty);
    if val<pbestVal(i), pbestVal(i)= val; pbest(i,:)= X(i,:);end
    if val<gbestVal,gbestVal = val; gbest = X(i,:);
    end
    if mod(iter,printInterval)==0
        fprintf('Iter %d CEED=%8.3f\n',iter,gbestVal);
    end
end
end
%=====Final evaluation of
variables=====
[Pcost,details]=objective(gbest' ,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,pe
naltyEmissionFactor,powerBalancePenalty);

fprintf('\n=====Final PSO Dispatch (6units)=====');
for i=1:n
    fprintf(' P(%d)=%8.3f MW (min %8.1f max
%8.1f)\n',i,gbest(i),Pmin(i),Pmax(i))
end
fprintf('Sum Thermal=%8.3f MW, Wind=%8.3f MW, Loss=%8.3f
MW\n',sum(gbest),TotalwindPower,details.PL)

```

```

fprintf('Fuel Cost=%.3f , Emission=%.3f ,
CEED=%.3f\n',details.fuelcost,details.emission,Pcost);
toc;

% This function is called on the main program: WTEED_casePS010units for
calculation
% of PL,fuelcost,emission.Named: objective.m
function [cost,details]=objective(P,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,
k1,kpb)
    P =P(:); WG = P+(TotalwindPower/length(P));
    PL = B00+B01'*WG+WG'*B*WG;
    fuel=sum(a.*(P.^2)+b.*P+c);
    em =sum(d.*(P.^2)+e.*P+f);
    CEED = fuel+k1*em;
    mismatch=PD+PL-(sum(P)+TotalwindPower);
    penalty=kpb*mismatch^2;
    cost =CEED+penalty;
    details.PL=PL;details.fuelcost=fuel;details.emission=em;
end
=====
=

```

APPENDIX B3: MATLAB script file – WTEED_casePSO40units.m

```

%%=====Main program=====
%This is IEEE30 bus system with 40 generathing units. Named:
WTEED_casePSO40units.m.
% The program is used to create table 4.5 and also used in Table 4.6
% It is using a function called objective.m
% This is IEEE30 bus system with 40 generathing units.
clear all; clc; close all;tic;
%=====User to enter power demand of the system=====
PD = input('What is the Power demand in (MW)=');
n =40; %number of used generators
num_particles = 40;% number of particles in the population
maxIter = 1000; %Number of iterations
w = 0.65; c1 = 1.5; c2 = 1.5;
penaltyEmissionFactor = 10000;
powerBalancePenalty = 1000000;
printInterval = 10;
% =====Fuel cost coefficients, Emission Coefficients, and limits of a
generator =====
data1 = [36      114      0.0069 6.73      94.705      0.048 -2.22 60
        36      114      0.0069 6.73      94.705 0.048 -2.22 60
        60      120      0.02028      7.07      309.54 0.0762 -2.36 100
        80      190      0.00942      8.18      369.03 0.054 -3.14 120
        47      97      0.0114 5.35      148.89 0.085 -1.89 50
        68      140      0.01142      8.05      222.33 0.0854 -3.08 80
        110     300      0.00357      8.03      287.71 0.0242 -3.06 100
        135     300      0.00492      6.99      391.98 0.031 -2.32 130
        135     300      0.00573      6.6      455.76 0.0335 -2.11 150
        130     300      0.00605      12.9     722.82 0.425 -4.34 280
        94      375      0.00515      12.9     635.2 0.0322 -4.34 220
        94      375      0.00569      12.8     654.69 0.0338 -4.28 225
        125     500      0.00421      12.5     913.4 0.0296 -4.18 300
        125     500      0.00752      8.84     1760.4 0.0512 -3.34 520
        125     500      0.00708      9.15     1728.3 0.0496 -3.55 510
        125     500      0.00708      9.15     1728.3 0.0496 -3.55 510
        220     500      0.00313      7.97     647.85 0.0151 -2.68 220
        220     500      0.00313      7.95     649.69 0.0151 -2.66 222
        242     550      0.00313      7.97     647.83 0.0151 -2.68 220
        242     550      0.00313      7.97     647.81 0.0151 -2.68 220];

```

```

data2 = [254    550    0.00298    6.63    785.96 0.0145 -2.22 290
        254    550    0.00298    6.63    785.96 0.0145 -2.22 285
          254  550    0.00284    6.66    794.53 0.0138 -2.26 295
          254  550    0.00284    6.66    794.53 0.0138 -2.26 295

          254  550    0.00277    7.1      801.32  0.0132 -2.42 310
        254    550    0.00277    7.1      801.32  0.0132 -2.42 310
        10    150    0.52124    3.33   1055.1 1.842 -1.11 360
          10    150    0.52124    3.33   1055.1 1.842 -1.11 360
          10    150    0.52124    3.33   1055.1 1.842 -1.11 360
          47    97    0.0114 5.35   148.89 0.085  -1.89 50
          60    190    0.0016 6.43   222.92 0.0121 -2.08 80
          60    190    0.0016 6.43   222.92 0.0121 -2.08 80
          60    190    0.0016 6.43   222.92 0.0121 -2.08 80
          90    200    0.0001 8.95   107.87 0.0012 -3.48 65
          90    200    0.0001 8.62   116.58 0.0012 -3.24 70
          90    200    0.0001 8.62   116.58 0.0012 -3.24 70
          25    110    0.0161 5.88   307.45 0.095  -1.98 100
          25    110    0.0161 5.88   307.45 0.095  -1.98 100
          25    110    0.0161 5.88   307.45 0.095  -1.98 100
          242  550    0.00313    7.97    647.83  0.0151 -2.68 220];
data = [data1;data2];
%=====Generator Limits =====
Pmin=data(:,1);
Pmax=data(:,2);
Wmax = 2000;
Wmin = 1;
% =====Fuel cost coefficients=====
a=data(:,3);
b=data(:,4);
c=data(:,5);
% ===== Emission Coefficients=====
d=data(:,6);
e=data(:,7);
f=data(:,8);
% =====Transmission loss coefficients=====
B00=0.56;
B01=10^-4.*[-3.908  -1.297 7.047  0.591  2.161  -6.635 -3.908 -1.297 7.047...
            0.591  2.161  -6.635 -3.908 -1.297 7.047  0.591  2.161  -6.635...
            -3.908 -1.297 7.047  0.591  2.161  -6.635 -3.908 -1.297 7.047...
            0.591  2.161  -6.635 -3.908 -1.297 7.047  0.591  2.161  -6.635...
            -3.908 -1.297 7.047  0.591]';

B1_half=[17  12  7  -1  -5  -2  17  12  7  -1  -5
         -2  17  12  7  -1  -5  -2  17  12  7  -1  -5
          12  14  9  1  -6  -1  12  14  9  1  -6
          -1  12  14  9  1  -6  -1  12  14  9  1  -6
           7  9  31  0  -10  -6  7  9  31  0  -10
          -6  7  9  31  0  -10  -6  7  9  31  0  -10
          -1  1  0  24  -6  -8  -1  1  0  24  -6  -8
          -8  -1  1  0  24  -6  -8  -1  1  0  24  -6  -8
          -5 -6 -10 -6  129 -2  -5  -6 -10 -6  129 -2
          -5  -6  -10  -6  129 -2  -5  -6  -6  -6  129 -2
          -2  -1  -6  -8  -2  150 -2  -1  -6  -8  -2
         150  -2  -1  -6  -8  -2  150 -2  -1  -6  -8  -2
          17  12  7  -1  -5  -2  17  12  7  -1  -5
          -2  17  12  7  -1  -5  -2  17  12  7  -1  -5

```

12	14	9	1	-6	-1	12	14	9	1	-6
-1	12	14	9	1	-6	-1	12	14		
7	9	31	0	-10	-6	7	9	31	0	-10
-6	7	9	31	0	-10	-6	7	9		
-1	1	0	24	-6	-8	-1	1	0	24	-6
-8	-1	1	0	24	-6	-8	-1	1		
-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129
-5	-6	-10	-6	129	-2	-5	-6			
-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2
150	-2	-1	-6	-8	-2	150	-2	-1		
17	12	7	-1	-5	-2	17	12	7	-1	-5
-2	17	12	7	-1	-5	-2	17	12		
12	14	9	1	-6	-1	12	14	9	1	-6
-1	12	14	9	1	-6	-1	12	14		
7	9	31	0	-10	-6	7	9	31	0	-10
7	9	31	0	-10	-6	7	9			
-1	1	0	24	-6	-8	-1	1	0	24	-6
-8	-1	1	0	24	-6	-8	-1	1		
-5	-6	-10	-6	129	-2	-5	-6	-10	-6	129
-5	-6	-10	-6	129	-2	-5	-6			
-2	-1	-6	-8	-2	150	-2	-1	-6	-8	-2
150	-2	-1	-6	-8	-2	150	-2	-1		
17	12	7	-1	-5	-2	17	12	7	-1	-5
-2	17	12	7	-1	-5	-2	17	12		
12	14	9	1	-6	-1	12	14	9	1	-6
-1	12	14	9	1	-6	-1	12	14		

B2_half=[

7	-1	-5	-2	17	12	7	-1	-5	-2	17
12	7	-1	-5	-2	17	12	7	-1		
9	1	-6	-1	12	14	9	1	-6	-1	12
14	9	1	-6	-1	12	14	9	1		
31	0	-10	-6	7	9	31	0	-10	-6	7
9	31	0	-10	-6	7	9	31	0		
0	24	-6	-8	-1	1	0	24	-6	-8	1
1	0	24	-6	-8	-1	1	0	24		
-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6		
-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2
-1	-6	-8	-2	150	-2	-1	-6	-8		
7	-1	-5	-2	17	12	7	-1	-5	-2	17
12	7	-1	-5	-2	17	12	7	-1		
9	1	-6	-1	12	14	9	1	-6	-1	12
14	9	1	-6	-1	12	14	9	1		
31	0	-10	-6	7	9	31	0	-10	-6	7
9	31	0	-10	-6	7	9	31	0		
0	24	-6	-8	-1	1	0	24	-6	-8	-1
1	0	24	-6	-8	-1	1	0	24		
-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6		
-6	-8	-2	150	-2	-1	-6	-8	-2	150	-2
-1	-6	-8	-2	150	-2	-1	-6	-8		
7	-1	-5	-2	17	10	-6	7	9	31	0
-10	-6	7	9	31	0	-10	-6	7		
0	24	-6	-8	-1	1	0	24	-6	-8	-1
1	0	24	-6	-8	-1	1	0	24		
-10	-6	129	-2	-5	-6	-10	-6	129	-2	-5
-6	-10	-6	129	-2	-5	-6	-10	-6		
-6	-8	12	7	-1	-5	-2	17	12	7	-1
-5	-2	17	12	7	-1	9	31	0		
9	1	-6	-1	12	14	9	1	-6	-1	12
14	9	1	-6	-1	12	14	9	1		

```

    31  0   -2  150  -2  -1  -6  -8  -2  150  -2
   -1  -6  -8  -2  150  -2  -1  -6  -8  -2  17
    7  -1  -5  -2  17  12  7  -1  -5  -2  17
   12  7  -1  -5  -2  17  12  7  -1  -1  12
    9  1  -6  -1  12  14  9  1  -6  -1  12
   14  9  1  -6  -1  12  14  9  1];

```

```

B3_half = [ 7  9  31  0  -10  -6  7  9  31  0
            -10 -6  7  9  31  0  -10  -6  7  9  31  0
            -1  -1  1  0  24  -6  -8  -1  1  0  24
            -6  -8  -1  1  0  24  -6  -8  -1  1  0  24
            -5  -5  -6  -10  -6  129  -2  -5  -6  -10  -6
            129  -2  -5  -6  -10  -6  129  -2  -5  -6  -8
            -2  -2  -1  -6  -8  -2  150  -2  -1  -6  -8
            -2  150  -2  -1  -6  -8  -2  150  -2  -1  -1
            17  12  7  -1  -5  -2  17  12  7  -1
            -5  -2  17  12  7  -1  -5  -2  17  12
            12  14  9  1  -6  -1  12  14  9  1
            -6  -1  12  14  9  1  -6  -1  12  14
            79  31  0  -10  -6  7  9  31  0  -10
            -6  7  9  31  0  -10  -6  7  9
            -1  1  0  24  -6  -8  -1  1  0  24
            -6  -8  -1  1  0  24  -6  -8  -1  1
            -5  -6  -10  -6  129  -2  -5  -6  -10  -6
            129  -2  -5  -6  -10  -6  129  -2  -5  -6  -8
            -2  -2  -1  -6  -8  -2  150  -2  -1  -6  -8
            -2  150  -2  -1  -6  -8  -2  150  -2  -1  -1
            17  12  7  -1  -5  -2  17  12  7  -1
            -5  -2  17  12  7  -1  -5  -2  17  12
            12  14  9  1  -6  -1  12  14  9  1
            -6  -1  12  14  9  1  -6  -1  12  14
            79  31  0  -10  -6  7  9  31  0  -10
            -6  7  9  31  0  -10  -6  7  9
            -1  1  0  24  -6  -8  -1  1  0  24
            -6  -8  -1  1  0  24  -6  -8  -1  1
            -5  -6  -10  -6  129  -2  -5  -6  -10  -6
            129  -2  -5  -6  -10  -6  129  -2  -5  -6  -8
            -2  -2  -1  -6  -8  -2  150  -2  -1  -6  -8
            -2  150  -2  -1  -6  -8  -2  150  -2  -1  -1
            17  12  7  -1  -5  -2  17  12  7  -1
            -5  -2  17  12  7  -1  -5  -2  17  12
            12  14  9  1  -6  -1  12  14  9  1
            -6  -1  12  14  9  1  -6  -1  12  14
            79  31  0  -10  -6  7  9  31  0  -10
            -6  7  9  31  0  -10  -6  7  9
            -1  1  0  24  -6  -8  -1  1  0  24
            -6  -8  -1  1  0  24  -6  -8  -1  1];

```

```

B4_half = [ 31  0  -10  -6  7  9  31  0  -10  -6
            7  9  31  0  -10  -6  7  9  31  0
            0 24  -6  -8  -1  1  0  24  -6  -8
            1  0  24  -6  -8  -1  1  0  24
            -10 -6  129  -2  -5  -6  -10  -6  129  -2
            -5  -6  -10  -6  129  -2  -5  -6  -10  -6
            -2  -1  -6  -8  -2  150  -2  -1  -6  -8
            7 -1  -5  -2  17  12  7  -1  -5  -2
            12  7  -1  -5  -2  17  12  7  -1
            14  9  1  -6  -1  12  14  9  1
            31  0  -10  -6  7  9  31  0  -10  -6
            7  9  31  0  -10  -6  7  9  31  0

```

```

1      024      -6      -8      -1      1      0      24      -6      -8      -1
1      0      24      -6      -8      -1      1      0      24      -6      -8      -1
-5     -10     -6     129     -2     -5     -6     -10     -6     129     -2
-5     -6     -10     -6     129     -2     -5     -6     -10     -6     129     -2
-2     -6     -8     -2     150     -2     -1     -6     -8     -2     150     -2
-2     -1     -6     -8     -2     150     -2     -1     -6     -8     -2     150
12     7-1     -5     -2     17     12     7     -1     -5     -2     17
12     7     -1     -5     -2     17     12     7     -1     -5     -2     17
14     91     -6     -1     12     14     9     1     -6     -1     12
14     9     1     -6     -1     12     14     9     1     -6     -1     12
7      31     0     -10     -6     7     9     31     0     -10     -6
7      9     31     0     -10     -6     7     9     31     0     -10     -6
1      024     -6     -8     -1     1     0     24     -6     -8     -1
1      0     24     -6     -8     -1     1     0     24     -6     -8     -1
-5     -10     -6     129     -2     -5     -6     -10     -6     129     -2
-5     -6     -10     -6     129     -2     -5     -6     -10     -6     129     -2
-2     -6     -8     -2     150     -2     -1     -6     -8     -2     150     -2
-2     -1     -6     -8     -2     150     -2     -1     -6     -8     -2     150
12     7-1     -5     -2     17     12     7     -1     -5     -2     17
12     7     -1     -5     -2     17     12     7     -1     -5     -2     17
14     91     -6     -1     12     14     9     1     -6     -1     12
14     9     1     -6     -1     12     14     9     1     -6     -1     12
7      31     0     -10     -6     7     9     31     0     -10     -6
7      9     31     0     -10     -6     7     9     31     0     -10     -6
1      024     -6     -8     -1     1     0     24     -6     -8     -1
1      0     24     -6     -8     -1     1     0     24     -6     -8     -1
B= 10^-6.*[B1_half B2_half;B3_half B4_half ];
%=====Parameters for wind Power calculations=====
data =[9.891 10.785 6.861 14.482 12.184 4.602 7.232 8.036 12.333 11.074
10.040];
v0= data';
vbins=0:0.5:max(data)+ 1;
%=====weibull data
distribution=====
pdwind = fitdist(v0, 'weibull');
prated=11.429*10^6;
vin=5;
vr=15;
vout=45;
%=====wind velocity constraint=====
pwbins = zeros(size(vbins));
powercurve = (vbins>vin)&(vbins<vr);
pwbins(powercurve) = prated*(vbins(powercurve).^2 - vin^2)./(vr^2-vin^2);
pwbins(vbins>vr&vbins<=vout)=prated;
%=====wind power calculation=====
pdfv=pdf(pdwind,vbins);
avgpower=trapz(vbins,pdfv.*pwbins);
pwd=(avgpower/(10^6));
nWindunits =input('Enter the number of available wind generators = ');
if isempty(nWindunits)|| nWindunits < 0
nWindunits = 0;
end
TotalwindPower =nWindunits*pwd;% Total wind Power from available wind
generators
fprintf('\n\n=====')
);
fprintf('\n The average wind Power available is = %8.3f
Megawatts\n',TotalwindPower);
fprintf('=====');
TotalwindPower = max(Wmin,min(TotalwindPower,Wmax));
%% Initial variables of the PSO algorithm
dim = n; lb = Pmin; ub = Pmax;

```

```

vmax = 0.5*(ub-lb); vmin = -vmax;
X =zeros(num_particles,dim); V = zeros(num_particles,dim);
pbest = X; pbestVal =inf(num_particles,1); gbest = zeros(1,dim);gbestVal
=inf;
for i=1:num_particles
X(i,:)=(lb+(ub-lb).*rand(dim,1))';
V(i,:)= (vmin+(vmax-vmin).*rand(dim,1))';

[val,~]=objective(X(i,:) ,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyEm
issionFactor,powerBalancePenalty);
pbest(i,:)=X(i,:);
pbestVal(i)=val;
if val<gbestVal
    gbest=X(i,:);
    gbestVal = val;
end
end
% =====Main loop of the PSO algorithm=====
for iter =1:maxIter
for i=1:num_particles
    r1 =rand(1,dim);r2 =rand(1,dim);
    V(i,:)=w*V(i,:)+c1*r1.*(pbest(i,:)-X(i,:))+c2*r2.*(gbest-X(i,:));
    V(i,:)=max(min(V(i,:),vmax'),vmin');
    X(i,:)=X(i,:)+V(i,:);
    X(i,:)=max(min(X(i,:),ub'),lb');

[val,~]=objective(X(i,:) ,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,penaltyEm
issionFactor,powerBalancePenalty);
    if val<pbestVal(i), pbestVal(i)= val; pbest(i,:)= X(i,:);end
    if val<gbestVal,gbestVal = val; gbest = X(i,:);
    end
if mod(iter,printInterval)==0
    fprintf('Iter %d CEED=%.3f\n',iter,gbestVal);
end
end
end
%=====Final evaluation of
variables=====
[Pcost,details]=objective(gbest',PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,pe
naltyEmissionFactor,powerBalancePenalty);

fprintf('\n=====Final PSO Dispatch (6units)=====');
for i=1:n
    fprintf(' P(%d)=%.3f MW (min %.1f max
%.1f)\n',i,gbest(i),Pmin(i),Pmax(i))
end
fprintf('Sum Thermal=%.3f MW, Wind=%.3f MW, Loss=%.3f
MW\n',sum(gbest),TotalwindPower,details.PL)
fprintf('Fuel Cost=%.3f , Emission=%.3f ,
CEED=%.3f\n',details.fuelcost,details.emission,Pcost);
toc
% This function is called on the main program: WTEED_casePS040units for
calculation
% of PL,fuelcost,emission.Named: objective.m
function [cost,details]=objective(P,PD,TotalwindPower,a,b,c,d,e,f,B00,B01,B,
k1,kpb)
P =P(:); WG = P+(TotalwindPower/length(P));
PL = B00+B01'*WG+WG'*B*WG;
fuel=sum(a.*(P.^2)+b.*P+c);
em =sum(d.*(P.^2)+e.*P+f);
CEED = fuel+k1*em;
mismatch=PD+PL-(sum(P)+TotalwindPower);

```

```

penalty=kpb*mismatch^2;
cost =CEED+penalty;
details.PL=PL;details.fuelcost=fuel;details.emission=em;
end

```

```

%=====
==

```

APPENDIX C: DEVELOPED MATLAB PROGRAM FOR MULTI-AREA WTEED PROBLEM USING LAGRANGE'S ALGORITHM

APPENDIX C1: MATLAB script file – MAWTEED_case6units.m

```

% M-File : MAWTEED_case6units.m
% two-area and 3 generator in each area
% Transmission loss considered in this case
% 1 tie-lines are used to interconnect the two-area power system
% =====M-File Description=====
% The M-File is used to solve Multiarea economic emission dispatch problem
by Lagrange's Algorithm
% The software is developed for MAWTEED problem. This program ised to
% create table 5.1, and also used in table 5.2.
clearvars
clc
%% Multi area economic dispatch data taken from the reference paper
(Basu.,2013 and Alli.,2024)
tic
%% Multi area Wind thermal economic emission dispatch data
m=2; % No of area
n=6; % Total No of Generators in all the area
NG=3; % No of Generators in each area
TL=1; % NO of Tie lines
N_iter=1000; % No of iteration
lambda=[50 50];
lambda1=lambda(1);lambda2=lambda(2);
lambda={lambda(1),lambda(2)};
PD=[757.8 505.2]; % Area power demand
%PD=[525 435 605 625]; % Area power demand
alfa=[0.01 0.01]; %Incremental deltalambda Tolerance value of each area
epsilon=[0.01 0.01]; % Tolerance value of each area
%%=====Multi area Generator fuel Cost coefficients=====
c=[550 350 310 240 200 126];
c={c(1:3),c(4:6)};
b=[8.10 7.50 8.10 7.74 8.00 8.60];
b={b(1:3),b(4:6)};
a = [0.00028 0.00056 0.00056 0.00324 0.00254 0.00284];
a={a(1:3),a(4:6)};
%%=====Multi area Emission coefficients=====
d = [0.00683 0.00461 0.00461 0.00484 0.00754 0.00661];
d={d(1:3),d(4:6)};
e=[-0.54551 -0.51160 -0.51160 -0.32767 -0.54551 -0.63262];
e={e(1:3),e(4:6)};
f = [40.26690 42.89553 42.89553 33.85932 50.639310 45.83267];
f={f(1:3),f(4:6)};
%%=====Multi area Generator real power limits=====
Pmin = [100 50 50 80 50 50];
Pmin1={Pmin(1:3),Pmin(4:6)};
Pmax = [500 200 150 300 200 120];
Pmax1={Pmax(1:3),Pmax(4:6)};
%%=====Intial Tie line values (Assumed)=====
PT_mj=[10];
PT_jm=[15];
%%=====Tie line limits=====
PTmin_mj=[5];

```

```

PTmin_jm=[5];
PTmax_mj=[100];
PTmax_jm=[100];
%%=====Tie line coefficients=====
q_mj=rand(1,1);q_jm=rand(1,1);
%%=====Tie line Fractional loss rate values=====
flr_jm=[0.11];
%%=====Tie line incremental value=====
alpha_mj=[0.000001];
alpha_jm=[0.00001];
%%=====Transmission loss coefficients=====
B_area=[ 0.000071 0.00003 0.000025
         0.00003 0.000069 0.000032
         0.000025 0.000032 0.00008
         0.000056 0.000045 0.000015
         0.000023 0.000042 0.000047
         0.000032 0.000023 0.000027];
B_area1={B_area((1:3),:),B_area((4:6),:)};
% =====Wind power data for each area=====
windData = {[9.891 10.785 6.861 14.482 12.184 4.602]...
            [8.5 7.2 6.9 10.4 12.1 5.8]};

Prated = [ 555 0]; %Rated wind power per area in (MW)
Vin = 3; Vr = 12; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
for area = 1:m
v0 = windData{area}';
pwind = fitdist(v0,'Weibull');
%===== Power for each area=====
pwwbins = zeros(size(vbins));
pwwbins(vbins>=Vin & vbins<Vr)= Prated(area).*...
((vbins(vbins>=Vin & vbins<Vr).^2 - Vin^2) / (Vr^2 - Vin^2));
pwwbins(vbins>=Vr & vbins<=Vout) = Prated(area);
% =====Expected wind power=====
pdfv = pdf(pwind,vbins);
avgpower = trapz(vbins,pdfv .*pwwbins);
fprintf('Area %d: Expected Wind ≈ %.2f MW\n',area,avgpower);
for s =1:Ns
v = random(pwind);
if v<Vin
Pw = 0;
elseif v < Vr
Pw = Prated(area) * ((v^2 - Vin^2)/(Vr^2 - Vin^2));
elseif v < Vout
Pw = Prated(area);
else
Pw = 0;
end
TotalwindPower(area,s) = Pw;
end
end
%=====Expected wind power
=====
Pwind_exp = mean(TotalwindPower,2);
% =====CEED with wind
power=====
Pwind = Pwind_exp; % Expected wind power
% Generator real power calculation
%% =====Lambda values for 2
areas=====

```

```

        lambda = [lambda1, lambda2];
        %%=====WTEED=====
        for iter = 1:N_iter
            fprintf('Iter %d\n',iter);
            %%=====Caculation of generator power per
            area=====
            Power1 =zeros(m,3); %Pre allocation of variables
            h1 =zeros(m,3);
            for i =1:m
                %%=====Calculation of the penalty factor h using max/max
                =====
                h=(a{i}.*Pmax1{i}.^2+b{i}.*Pmax1{i}+c{i})./(d{i}.*Pmax1{i}.^2+e{i}.*Pmax1{i}
                }+f{i});
                E = diag((a{i}+h.*d{i}) ./lambda(i));
                D = 0.5*(1-(b{i}+h.*e{i})./lambda(i))';
                Power=E\D;
                Power1(i,:)=Power';
                h1(i,:)=h;
            end
            P=reshape(Power1',1,6);
            h=reshape(h1',1,6);
            h_cell ={h(1:3),h(4:6)};

            %% =====Check generator limits=====
            for i = 1:n

                P(i) = min(max(P(i), Pmin(i)),Pmax(i));
            end
            %%=====Tie line power flow=====
            ePT_mj=q_mj+lambda1;
            PT_mj=(PT_mj-alpha_mj.*ePT_mj);
            ePT_jm=q_jm-(1-flr_jm).*lambda1 ;
            PT_jm=PT_jm-alpha_jm.*ePT_jm;
            %%=====Tie Line limits=====
            TL=1;
            for i=1:TL
                PT_mj(i)=min(max(PT_mj(i),PTmin_mj(i)),PTmax_mj(i));
                PT_jm(i)=min(max(PT_jm(i),PTmin_jm(i)),PTmax_jm(i));
            end
            Tielinepower=PT_mj-(1-flr_jm).*PT_jm;
            %%=====Tie line flows per area net
            injection=====
            % Tieline_area1 = Tielinepower(1) + Tielinepower(2) + Tielinepower(3);
            Tieline_area1 = Tielinepower;
            Tieline_area2 = -Tielinepower;
            Tieline_area = [Tieline_area1, Tieline_area2];
            %%=====Transmission line loss=====
            B_area11=permute(reshape(B_area,3,2,[]),[1 3 2]);
            P=reshape(P,3,1,[]);
            PL_area=bsxfun(@times,P,reshape(P,1,3,[])).*B_area11;
            PL=sum(reshape(PL_area,[],2));
            %%=====Calculation of delta using P sums per area=====
            P1 = P(1:3);P2 = P(4:6);
            sumP = [sum(P1),sum(P2)];
            deltalambda = ( PD + PL + Tieline_area)-(sumP+Pwind');
            %%=====Updating lambda using gradient procedure=====
            lambda = lambda + alfa.*deltalambda;
            %%=====Breaking upon convergence and reaching max
            iterations===
            if all(abs(deltalambda)<=epsilon)

```

```

        fprintf('Converged in %d iterations (all |deltalambda| <=
epsilon).\n',iter);
        break;
    elseif iter>= N_iter
        fprintf('Reached maximum iterations %d (not all area
converged).\n',N_iter)
        break;
    end
end
P1 = P(1:3);P2 = P(4:6);
h = h_cell;
% lambda = {lambda1, lambda2};
lambda
P
Tielinepower;
PT_mj;
PT_jm;
P={P(1:3),P(4:6)};
%=== Calculation of fuel cost, emission and CEED values of MAEED problem
solution===
for i=1:m
fuelcost_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i});
fuelcost(i,:)=fuelcost_area;
emissioncost_area=sum(d{i}.*P{i}.^2+e{i}.*P{i}+f{i});
emissioncost(i,:)=emissioncost_area;
ceed_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i}+h{i}.*(d{i}.*P{i}.^2+e{i}.*P{i}
+f{i}));
ceed(i,:)=ceed_area;
end
fuelcost=sum(fuelcost)
emissioncost=sum(emissioncost)
ceed=sum(ceed)
ans=[fuelcost emissioncost ceed iter toc]
fprintf('Final Wind Injection per Area (MW):\n')
disp(Pwind');
fprintf('Final results after %d iterations\n',iter);
fprintf('Total Fuel cost = %.4f\n',fuelcost);
fprintf('Total Emission cost = %.4f\n',emissioncost)
fprintf('Total CEED = %.4f\n',ceed);
fprintf('Final Wind Injection per Area (MW):\n');disp(Pwind' );
toc

```

APPENDIX C2: MATLAB script file – MAWTEED_case12units.m

```

% M-File : MAWTEEDP_case12units.m
% =====M-File Description=====
% This test system consists of a standard IEEE30 bus system with four-area
% ,12 thermal generators, comprising 3 generators in each area,
% and a three-wind park network that supplies
% wind power of 110MW each to the entire dispatch problem.
% The total power demand is considered as 2090[MW].
% The software is developed for MAWTEED problem. The program is used to
% develop table 5.3 and used in table 5.4
clearvars;
clc
%% Multi area Wind thermal economic emission dispatch data
m=4; % No of area
n=12; % Total No of Generators in all the area
NG=3; % No of Generators in each area
TL=6; % NO of Tie lines
N_iter=20000; % No of iteration
lambda=[100 100 100 100];

```

```

lambda1=lambda(1);lambda2=lambda(2);lambda3=lambda(3);lambda4=lambda(4);
lambda={lambda(1),lambda(2),lambda(3),lambda(4)};
PD=[500 410 580 600]; % Area power demand
%PD=[525 435 605 625]; % Area power demand
alfa=[0.01 0.01 0.01 0.01]; %Incremental deltalambda Tolerance value of
each area
epsilon=[0.01 0.01 0.01 0.01]; % Tolerance value of each area
%%=====Multi area Generator fuel Cost coefficients=====
a=[0.03546 0.02111 0.01799...
    0.15247 0.02803 0.14834...
    0.10587 0.07505 0.11934...
    0.10587 0.13552 0.08963];
a={a(1:3),a(4:6),a(7:9),a(10:12)};

b=[38.30553 36.32782 38.27041...
    38.53973 40.39655 38.34001...
    46.15916 43.83562 50.63211...
    46.15916 41.03782 33.56211];
b={b(1:3),b(4:6),b(7:9),b(10:12)};

c=[1243.5311 1658.5696 1356.6592...
    0756.7989 0449.9977 0558.5696...
    0451.3251 0673.0267 0530.7199...
    0851.3251 1038.533 1285.907];
c={c(1:3),c(4:6),c(7:9),c(10:12)};
%%=====Multi area Emission coefficients=====
d=[0.00683 0.00461 0.00461...
    0.00484 0.00754 0.00661...
    0.00914 0.00533 0.00674...
    0.00728 0.00479 0.00387];
d={d(1:3),d(4:6),d(7:9),d(10:12)};

e=[-0.54551 -0.51160 -0.51160...
    -0.32767 -0.54551 -0.63262...
    -0.43211 -0.61173 -0.49731...
    -0.6821 -0.50660 -0.49340];
e={e(1:3),e(4:6),e(7:9),e(10:12)};

f=[40.26690 42.89553 42.89553...
    33.85932 50.639310 45.83267...
    48.21560 52.45210 41.10420...
    30.36320 25.17650 27.75490];
f={f(1:3),f(4:6),f(7:9),f(10:12)};
Wmin = 1;
Wmax = 2000;
nW = 1;
%%=====Multi area Generator real power limits=====
Pmin=[35 130 125 10 35 125 15 30 50 15 30 50];
Pmin1={Pmin(1:3),Pmin(4:6),Pmin(7:9),Pmin(10:12)};
Pmax=[210 325 315 150 110 215 175 215 335 175 215 335];
Pmax1={Pmax(1:3),Pmax(4:6),Pmax(7:9),Pmax(10:12)};
%%=====Intial Tie line values (Assumed)=====
PT_mj=[10 15 12 20 18 29];
PT_jm=[15 18 20 14 22 19];
%%=====Tie line limits=====
PTmin_mj=[5 5 5 5 5 5];
PTmin_jm=[5 5 5 5 5 5];
PTmax_mj=[60 50 60 60 60 50];
PTmax_jm=[50 60 60 60 50 60];
%%=====Tie line coefficients=====
q_mj=rand(1,6);q_jm=rand(1,6);
%%=====Tie line Fractional loss rate values=====

```

```

% flr_jm=[0.11 0.21 0.14 0.16];
flr_jm=[0.11 0.21 0.14 0.16 0.22 0.11];
%%=====Tie line incremental value=====
alpha_mj=[0.000001 0.000001 0.000001 0.000001 0.000001 0.000001];
% alpha_mj=[0.000001 0.000001 0.000001 0.000001];
alpha_jm=[0.00001 0.00001 0.00001 0.00001 0.00001 0.00001];
% alpha_jm=[0.00001 0.00001 0.00001 0.00001];
%%=====Transmission loss coefficients=====
B_area=[ 0.000071 0.00003 0.000025
          0.00003 0.000069 0.000032
          0.000025 0.000032 0.00008
          0.000056 0.000045 0.000015
          0.000023 0.000042 0.000047
          0.000032 0.000023 0.000027
          0.00002 0.000028 0.000053
          0.000086 0.000034 0.000016
          0.000053 0.000016 0.000028
          0.000074 0.00003 0.000025
          0.000049 0.000069 0.000037
          0.000022 0.000032 0.000083];
B_area1={B_area((1:3),:),B_area((4:6),:),B_area((7:9),:),B_area((10:12),:)}
;
% =====Wind power data for each area=====
windData = {[9.891 10.785 6.861 14.482 12.184 4.602];...
            [8.5 7.2 6.9 10.4 12.1 5.8];...
            [7.3 8.6 6.2 11.0 9.8 4.5];...
            [6.5 7.9 5.1 9.2 8.7 4.0]};
Prated = [ 215 210 210 212]; %Rated wind power per area in (MW)
Vin = 3; Vr = 12; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
for area = 1:m
    v0 = windData{area}';
    pwind = fitdist(v0,'Weibull');
    %%===== Power for each area=====
    pwvbins = zeros(size(vbins));
    pwvbins(vbins>=Vin & vbins<Vr)= Prated(area).*...
        ((vbins(vbins>=Vin & vbins<Vr).^2 - Vin^2)/(Vr^2 - Vin^2));
    pwvbins(vbins>=Vr & vbins<=Vout) = Prated(area);
    % =====Expected wind power=====
    pdfv = pdf(pwind,vbins);
    avgpower = trapz(vbins,pdfv .*pwvbins);
    fprintf('Area %d: Expected Wind = %.2f MW\n',area,avgpower);
    for s =1:Ns
        v = random(pwind);
        if v<Vin
            Pw = 0;
        elseif v < Vr
            Pw = Prated(area) * ((v^3 - Vin^3)/(Vr^3 - Vin^3));
        elseif v < Vout
            Pw = Prated(area);
        else
            Pw = 0;
        end
        TotalwindPower(area,s) = Pw;
    end
end
%=====Expected wind power =====
Pwind_exp = mean(TotalwindPower,2);
% =====CEED with wind power=====
Pwind = Pwind_exp; % Expected wind power

```

```

%=====Generator real power calculation=====
for iter=1:N_iter
iter;
for i=1:m
%h=(a{i}.*Pmin1{i}.^2+b{i}.*Pmin1{i}+c{i})./(d{i}.*Pmax1{i}.^2+e{i}.*Pmax1{
i}+f{i});
h=(a{i}.*Pmax1{i}.^2+b{i}.*Pmax1{i}+c{i})./(d{i}.*Pmax1{i}.^2+e{i}.*Pmax1{i
}+f{i});
%h=(a{i}.*Pmin1{i}.^2+b{i}.*Pmin1{i}+c{i})./(d{i}.*Pmin1{i}.^2+e{i}.*Pmin1{
i}+f{i});
%h=(a{i}.*Pmax1{i}.^2+b{i}.*Pmax1{i}+c{i})./(d{i}.*Pmin1{i}.^2+e{i}.*Pmin1{
i}+f{i});
E=diag((a{i}+h.*d{i})./lambda{i})+B_area1{i};
D=0.5*(1-(b{i}+h.*e{i})./lambda{i})';
Power=E\D;
Power1(i,:)=Power;
h1(i,:)=h;
end
P=reshape(Power1',1,12);
h=reshape(h1',1,12);
h={h(1:3),h(4:6),h(7:9),h(10:12)};
%%=====Generator Real powers=====
P=[P(1:3),P(4:6),P(7:9),P(10:12)];
%%=====Generator real power limits=====
for i=1:n % Total Number of generators in all the four area is n=12
P(i)=min(max(P(i),Pmin(i)),Pmax(i));
end
%%=====Tie line power flow=====
ePT_mj=q_mj+lambda1;PT_mj=(PT_mj-alpha_mj.*ePT_mj);
ePT_jm=q_jm-(1-flr_jm).*lambda1 ;PT_jm=PT_jm-alpha_jm.*ePT_jm;
%%=====Tie Line limits=====
TL=6;
for i=1:TL

PT_mj(i)=min(max(PT_mj(i),PTmin_mj(i)),PTmax_mj(i));
PT_jm(i)=min(max(PT_jm(i),PTmin_jm(i)),PTmax_jm(i));
end
Tielinepower=PT_mj-(1-flr_jm).*PT_jm;
Tielinepower_area = (sum(Tielinepower) / m) * ones(1,m);
%%=====Transmission line loss=====
B_area11=permute(reshape(B_area,3,4,[]),[1 3 2]);
P=reshape(P,3,1,[]);
PL_area=bsxfun(@times,P,reshape(P,1,3,[])).*B_area11;
PL=sum(reshape(PL_area,[],4));
%%=====Incremental lambda=====
P1=P(1:3);P2=P(4:6);P3=P(7:9);P4=P(10:12);
deltalambda1=(PD(1)+PL(1)+Tielinepower(1))-(sum(P1)+Pwind(1));
deltalambda2=(PD(2)+PL(2)+Tielinepower(2))-(sum(P2)+Pwind(2));
deltalambda3=(PD(3)+PL(3)+Tielinepower(3))-(sum(P3)+Pwind(3));
deltalambda4=(PD(4)+PL(4)+Tielinepower(4))-(sum(P4)+Pwind(4));
deltalambda=[deltalambda1 deltalambda2 deltalambda3 deltalambda4];
if abs(deltalambda1)<=epsilon(1) && iter>=N_iter
fprintf('Converged in %d iterations (all |deltalambda| <=
epsilon).\n',iter);
break
else
lambda1=lambda1+(deltalambda1*alfa(1));
end
if abs(deltalambda2)<=epsilon(2) && iter>=N_iter
break
else lambda2=lambda2+(deltalambda2*alfa(2));
end

```

```

if abs(deltalambda3)<=epsilon(3) && iter>=N_iter
break
else lambda3=lambda3+(deltalambda3*alfa(3));
end
if abs(deltalambda4)<=epsilon(4) && iter>=N_iter
break
else lambda4=lambda4+(deltalambda4*alfa(4));
end
lambda={lambda1,lambda2,lambda3,lambda4};
end
deltalambda=[deltalambda1 deltalambda2 deltalambda3 deltalambda4];
P
PL
Tielinepower
PT_mj
PT_jm
P={P(1:3),P(4:6),P(7:9),P(10:12)}
for i=1:m
fuelcost_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i});
fuelcost(i,:)=fuelcost_area;
emissioncost_area=sum(d{i}.*P{i}.^2+e{i}.*P{i}+f{i});
emissioncost(i,:)=emissioncost_area;
ceed_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i}+h{i}.*(d{i}.*P{i}.^2+e{i}.*P{i}
+f{i}));
ceed(i,:)=ceed_area;
end
fuelcost=sum(fuelcost)
emissioncost=sum(emissioncost)
ceed=sum(ceed)
% fprintf('Final Wind Injection per Area (MW):\n');
% disp(Pwind');

fprintf('Final results after %d iterations\n', iter);
fprintf('Total Fuel cost = %.4f\n', fuelcost);
fprintf('Total Emission cost = %.4f\n', emissioncost);
fprintf('Total CEED = %.4f\n', ceed);
fprintf('Final Wind Injection per Area (MW):\n'); disp(Pwind');
Pwind = sum(Pwind(:, :))
PL = sum(PL(:, :))

```

APPENDIX C3: MATLAB script file – MAWTEED_case40units.m

```

% M-File : MAWTEED_case40units.m
% =====M-File Description=====
% two-area and 20 generator in each area. Transmission loss is omitted in
this case
% 1 tie-lines are used to interconnect the two-area power system
% a three-wind park network that supplies wind power of 110MW each to the
entire dispatch problem.
% The total power demand is considered as 10500[MW].
% The software is developed for MAWTEED problem. The program is used to
% develop table 5.9 and used in table 5.10
% =====M-File Description=====
clearvars
clc
%% Multi area economic dispatch data taken from the reference paper
(Basu,2011)
tic
m=2; % No of area
n=40; % Total No of Generators in all the area
TL=1; % NO of Tie lines
N_iter=50000; % No of iteration

```

```

lambda=[100 100]; % Initial Lagrangian variable
lambda1=lambda(1);lambda2=lambda(2);
lambda={lambda(1),lambda(2)};
% Total power demand of the system, PD=10500[MW]
PD=[7500 3000]; % Area power demand
alfa=[0.01 0.01]; %Incremental deltalambda Tolerance value of each area
epsilon=[0.01 0.01]; % Tolerance value of each area
%% Multi area Generator fuel Cost coefficients
%% Single area Generator fuel Cost coefficients
%% =====Data are given in the reference paper (Basu, 2013)=====
%The data are given in the format[GenNum Pmin Pmax a b c d e f]=====
Data=[.....
1 36 114 0.0069 6.73 94.705 0.048 -2.22 60
2 36 114 0.0069 6.73 94.705 0.048 -2.22 60
3 60 120 0.02028 7.07 309.54 0.0762 -2.36 100
4 80 190 0.00942 8.18 369.03 0.054 -3.14 120
5 47 97 0.0114 5.35 148.89 0.085 -1.89 50
6 68 140 0.01142 8.05 222.33 0.0854 -3.08 80
7 110 300 0.00357 8.03 287.71 0.0242 -3.06 100
8 135 300 0.00492 6.99 391.98 0.031 -2.32 130
9 135 300 0.00573 6.6 455.76 0.0335 -2.11 150
10 130 300 0.00605 12.9 722.82 0.425 -4.34 280
11 94 375 0.00515 12.9 635.2 0.0322 -4.34 220
12 94 375 0.00569 12.8 654.69 0.0338 -4.28 225
13 125 500 0.00421 12.5 913.4 0.0296 -4.18 300
14 125 500 0.00752 8.84 1760.4 0.0512 -3.34 520
15 125 500 0.00752 8.84 1760.4 0.0496 -3.55 510
16 125 500 0.00752 8.84 1760.4 0.0496 -3.55 510
17 220 500 0.00313 7.97 647.85 0.0151 -2.68 220
18 220 500 0.00313 7.95 649.69 0.0151 -2.66 222
19 242 550 0.00313 7.97 647.83 0.0151 -2.68 220
20 242 550 0.00313 7.97 647.81 0.0151 -2.68 220
21 254 550 0.00298 6.63 785.96 0.0145 -2.22 290
22 254 550 0.00298 6.63 785.96 0.0145 -2.22 285
23 254 550 0.00284 6.66 794.53 0.0138 -2.26 295
24 254 550 0.00284 6.66 794.53 0.0138 -2.26 295
25 254 550 0.00277 7.1 801.32 0.0132 -2.42 310
26 254 550 0.00277 7.1 801.32 0.0132 -2.42 310
27 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
28 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
29 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
30 47 97 0.0114 5.35 148.89 0.085 -1.89 50
31 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
32 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
33 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
34 90 200 0.0001 8.95 107.87 0.0012 -3.48 65
35 90 200 0.0001 8.62 116.58 0.0012 -3.24 70
36 90 200 0.0001 8.62 116.58 0.0012 -3.24 70
37 25 110 0.0161 5.88 307.45 0.095 -1.98 100
38 25 110 0.0161 5.88 307.45 0.095 -1.98 100
39 25 110 0.0161 5.88 307.45 0.095 -1.98 100
40 242 550 0.00313 7.97 647.83 0.0151 -2.68 220];
%% =====Multi area fuel cost coefficients=====
a=Data(:,4)';
a={a(1:20),a(21:40)};
b=Data(:,5)';
b={b(1:20),b(21:40)};
c=Data(:,6)';
c={c(1:20),c(21:40)};
%%=====Multi area Emmis on coefficients=====
d=Data(:,7)';
d={d(1:20),d(21:40)};

```

```

e=Data(:,8)';
e={e(1:20),e(21:40)};
f=Data(:,9)';
f={f(1:20),f(21:40)};
%% =====Multi area Generator real power limits=====
Pmin=Data(:,2)';
Pmin1={Pmin(1:20),Pmin(21:40)};
Pmax=Data(:,3)';
Pmax1={Pmax(1:20),Pmax(21:40)};
%%===== Initial Tie line values between 100 to 200 [MW] (Assumed)
PT_mj=randi([100 200],1,1);
PT_jm=randi([100 200],1,1);
%% =====Tie line limits (Assumed)=====
PTmin_mj=[100];
PTmin_jm=[100];
PTmax_mj=[1500];
PTmax_jm=[1500];
%% =====Tie line coefficients (Assumed)=====
q_mj=rand(1,1);
q_jm=rand(1,1);
%% =====Tie line Fractional loss rate values (Assumed)=====
flr_jm=rand(1,1);
%%=====Tie line incremental value (Assumed)=====
alpha_mj=[0.01];
alpha_jm=[0.01];
% =====Wind power data for each area=====
windData = {[9.891 10.785 6.861 14.482 12.184 4.602]...
            [8.5 7.2 6.9 10.4 12.1 5.8]};
Prated = [ 555 0]; %Rated wind power per area in (MW)
Vin = 5; Vr = 15; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
for area = 1:m
    v0 = windData{area}';
    pwind = fitdist(v0,'Weibull');
    %%===== Power for each area=====
    pwvbins = zeros(size(vbins));
    pwvbins(vbins>=Vin & vbins<Vr)= Prated(area).*...
        ((vbins(vbins>=Vin & vbins<Vr).^2 - Vin^2) / (Vr^2 - Vin^2));
    pwvbins(vbins>=Vr & vbins<=Vout ) = Prated(area);
    % =====Expected wind power=====
    pdfv = pdf(pwind,vbins);
    avgpower = trapz(vbins,pdfv .*pwvbins);
    fprintf('Area %d: Expected Wind = %.2f MW\n',area,avgpower);
    for s =1:Ns
        v = random(pwind);
        if v<Vin
            Pw = 0;
        elseif v < Vr
            Pw = Prated(area) * ((v^2 - Vin^2)/(Vr^2 - Vin^2));
        elseif v < Vout
            Pw = Prated(area);
        else
            Pw = 0;
        end
        TotalwindPower(area,s) = Pw;
    end
end
%%=====Expected wind power =====
Pwind_exp = mean(TotalwindPower,2);
% =====CEED with wind power=====

```

```

Pwind = Pwind_exp; % Expected wind power
% Generator real power calculation
%% =====Lambda values for 2 areas=====
lambda = [lambda1, lambda2];
%%=====WTEED=====
for iter = 1:N_iter
    fprintf('Iter %d\n',iter);
    %=====Calculation of generator power per area=====
    Power1 =zeros(m,20); %Pre allocation of variables
    h1 =zeros(m,20);
    for i =1:m
        %=====Calculation of the penalty factor h using max/max =====
        h=(a{i}.*Pmax1{i}.^2+b{i}.*Pmax1{i}+c{i})./(d{i}.*Pmax1{i}.^2+e{i}.*Pmax1{i}
        +f{i});
        E = diag((a{i}+h.*d{i}) ./lambda(i));
        D = 0.5*(1-(b{i}+h.*e{i})./lambda(i))';
        Power=E\D;
        Power1(i,:)=Power';
        h1(i,:)=h;
    end
    P=reshape(Power1',1,40);
    h=reshape(h1',1,40);
    h_cell ={h(1:20),h(21:40)};

%%% =====Check generator limits=====
    for i = 1:n
        P(i) = min(max(P(i), Pmin(i)),Pmax(i));
    end
    %=====Tie line power flow=====
    ePT_mj=q_mj+lambda1;
    PT_mj=(PT_mj-alpha_mj.*ePT_mj);
    ePT_jm=q_jm-(1-flr_jm).*lambda1 ;
    PT_jm=PT_jm-alpha_jm.*ePT_jm;
    %=====Tie Line limits=====
    TL=1;
    for i=1:TL
        PT_mj(i)=min(max(PT_mj(i),PTmin_mj(i)),PTmax_mj(i));
        PT_jm(i)=min(max(PT_jm(i),PTmin_jm(i)),PTmax_jm(i));
    end
    Tielinepower=PT_mj-(1-flr_jm).*PT_jm;
    %=====Tie line flows per area net
    injection=====
        % Tieline_area1 = Tielinepower(1) + Tielinepower(2) + Tielinepower(3);
        Tieline_area1 = Tielinepower;
        Tieline_area2 = -Tielinepower;
        Tieline_area = [Tieline_area1, Tieline_area2];
        %=====Calculation of delta using P sums per area=====
        P1 = P(1:20);P2 = P(21:40);
        sumP = [sum(P1),sum(P2)];
        dotalambda = ( PD + Tieline_area)-(sumP+Pwind');
    %=====Updating lambda using gradient procedure=====
        lambda = lambda + alfa.*dotalambda;
    %=====Breaking upon convergence and reaching max
    iterations===
        if all(abs(dotalambda)<=epsilon)
            fprintf('Converged in %d iterations (all |dotalambda| <=
            epsilon).\n',iter);
            break;
        elseif iter>= N_iter
            fprintf('Reached maximum iterations %d (not all area
            converged).\n',N_iter)

```

```

        break;
    end
end
end
P1 = P(1:20);P2 = P(21:40);
h = h_cell;
% lambda = {lambda1, lambda2};
lambda
P
Tielinepower;
PT_mj;
PT_jm;
P={P(1:20),P(21:40)};
%=== Calculation of fuel cost, emission and CEED values of MAEED problem
solution===
for i=1:m
fuelcost_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i});
fuelcost(i,:)=fuelcost_area;
emissioncost_area=sum(d{i}.*P{i}.^2+e{i}.*P{i}+f{i});
emissioncost(i,:)=emissioncost_area;
ceed_area=sum(a{i}.*P{i}.^2+b{i}.*P{i}+c{i}+h{i}.*(d{i}.*P{i}.^2+e{i}.*P{i}
+f{i}));
ceed(i,:)=ceed_area;
end
fuelcost=sum(fuelcost)
emissioncost=sum(emissioncost)
ceed=sum(ceed)
ans=[fuelcost emissioncost ceed iter toc]
fprintf('Final Wind Injection per Area (MW):\n')
disp(Pwind');
fprintf('Final results after %d iterations\n', iter);
fprintf('Total Fuel cost = %.4f\n', fuelcost);
fprintf('Total Emission cost = %.4f\n', emissioncost);
fprintf('Total CEED = %.4f\n', ceed);
fprintf('Final Wind Injection per Area (MW):\n'); disp(Pwind');
toc
ans1 = [P Pwind fuelcost emissioncost ceed]
lambda

```

APPENDIX D: DEVELOPED MATLAB PROGRAM FOR MULTI-AREA WTEED PROBLEM USING PSO ALGORITHM

APPENDIX D1: MATLAB script file – MAWTEED_casePSO6units.m

```

% M-File : MAWTEED_casePSO6units.m
% two-area and 3 generator in each area
% Transmission loss considered in this case
% 1 tie-lines are used to interconnect the two-area power system
% =====M-File Description=====
% The M-File is used to solve Multiarea economic emission dispatch problem
using PSO Algorithm
% The software is developed for MAWTEED problem. This program is used to
% create table 6.1 and used in table 6.2. It is used with the function
% named: objective_funPSO.m
clearvars
clc
%% Multi area economic dispatch data taken from the reference paper
(Basu.,2013 and Alli.,2024)
tic
%% Multi area Wind thermal economic emission dispatch data
m=2; % No of area
n=6; % Total No of Generators in all the area
NG=3; % No of Generators in each area
TL=1; % NO of Tie line

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PD=[757.8 505.2]; % Area power demand
%PD=[525 435 605 625]; % Area power demand
%%=====Multi area Generator fuel Cost coefficients=====
c=[550 350 310 240 200 126];
% c={c(1:3),c(4:6)};
b=[8.10 7.50 8.10 7.74 8.00 8.60];
% b={b(1:3),b(4:6)};
a = [0.00028 0.00056 0.00056 0.00324 0.00254 0.00284];
% a={a(1:3),a(4:6)};
%%=====Multi area Emission coefficients=====
d = [0.00683 0.00461 0.00461 0.00484 0.00754 0.00661];
% d={d(1:3),d(4:6)};
e=[-0.54551 -0.51160 -0.51160 -0.32767 -0.54551 -0.63262];
% e={e(1:3),e(4:6)};
f = [40.26690 42.89553 42.89553 33.85932 50.639310 45.83267];
% f={f(1:3),f(4:6)};
%%=====Multi area Generator real power limits=====
Pmin = [100 50 50 80 50 50];
% Pmin1={Pmin(1:3),Pmin(4:6)};
Pmax = [500 200 150 300 200 120];
% Pmax1={Pmax(1:3),Pmax(4:6)};
%%=====Intial Tie line values (Assumed)=====
% PT_mj=10;
% PT_jm=15;
%%=====Tie line limits=====
% PTmin_mj=5;
% PTmin_jm=5;
% PTmax_mj=100;
% PTmax_jm=100;
%%=====Tie line coefficients=====
% q_mj=rand(1,1);q_jm=rand(1,1);
%%=====Tie line Fractional loss rate values=====
% flr_jm=0.11;
% %%=====Tie line incremental value=====
% alpha_mj=0.000001;
% alpha_jm=0.00001;
%%=====Transmission loss coefficients=====
B_area=[ 0.000071 0.00003 0.000025
0.00003 0.000069 0.000032
0.000025 0.000032 0.00008
0.000056 0.000045 0.000015
0.000023 0.000042 0.000047
0.000032 0.000023 0.000027];
% B_area1={B_area((1:3),:),B_area((4:6),:)};
% =====Wind power data for each area=====
windData = {[9.891 10.785 6.861 14.482 12.184 4.602]...
[8.5 7.2 6.9 10.4 12.1 5.8]};

Prated = [ 555 0]; %Rated wind power per area in (MW)
Vin = 3; Vr = 12; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
for area = 1:m
    v0 = windData{area}';
    pwind = fitdist(v0,'Weibull');
    %%===== Power for each area=====
    pwvbins = zeros(size(vbins));
    pwvbins(vbins>=Vin & vbins<Vr)= Prated(area).*...
((vbins(vbins>=Vin & vbins<Vr).^3 - Vin^3) / (Vr^3 - Vin^3));
    pwvbins(vbins>=Vr & vbins<=Vout ) = Prated(area);
    % =====Expected wind power=====

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        pdfv = pdf(pwind,vbins);
        avgpower = trapz(vbins,pdfv .*pwvbins);
        fprintf('Area %d: Expected Wind = %.2f MW\n',area,avgpower);
for s =1:Ns
    v = random(pwind);
    if v<Vin
        Pw = 0;
    elseif v < Vr
        Pw = Prated(area) * ((v^3 - Vin^3)/(Vr^3 - Vin^3));
    elseif v < Vout
        Pw = Prated(area);
    else
        Pw = 0;
    end
TotalwindPower(area,s) = Pw;
end
end
%=====Expected wind power =====
Pwind_exp = mean(TotalwindPower,2);
% =====CEED with wind power=====
Pwind = Pwind_exp; % Expected wind power
%%=====WTEED=====
%% =====Price penalty factor h=====
h = (a.*Pmax.^2 + b.*Pmax + c)./(d.*Pmax.^2 + e.*Pmax+f);
%=====
%=====PSO parameters=====
nVar = n + 1; % 6 Generator output + 1 tie-line variable T
% Tie-line limits
%=====Tie line limits=====
Tmin = -100;
Tmax = 100;
%=====
%=====Search bounds limits=====
lb = [Pmin, Tmin];
ub = [Pmax, Tmax];
%=====
%=====PSO initialization=====
swarmSize = 80;
maxIter = 600;
w = 0.72;% Initial weight
c1 = 1.49; c2 = 1.49;%
velMax = 0.2*(ub-lb); velMin = -velMax;
% =====penalty coeefficient for power balance violations=====
penalty_factor = 1e6;
%=====initialization of PSO variable and preallocation=====
X = repmat(lb,swarmSize,1) + rand(swarmSize,nVar) .* (repmat(ub-lb,
swarmSize,1));
V = zeros(swarmSize,nVar);
pBest = X;
pBestVal = inf(swarmSize,1);
gBest = zeros(1,nVar);
gBestVal = inf;
convergence = zeros(maxIter,1);

%% =====PSO MAIN LOOP=====
rng('default');
for iter = 1:maxIter
    for i = 1:swarmSize
        % =====Max/Min bounds for P and T=====
        X(i,:) = max(X(i,:),lb);
        X(i,:) = min(X(i,:),ub);
        %=====

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%=====Evaluate the function =====
[val,~] =
objective_funPSO(X(i,:),n,Pmin,Pmax,Tmin,Tmax,PD,Pwind,a,b,c,d,e,f,h,B_area
,penalty_factor);
%===== update pBest=====
if val < pBestVal(i)
    pBestVal(i) = val;
    pBest(i,:) = X(i,:);
end
%=====update global best=====
if val < gBestVal
    gBestVal = val;
    gBest = X(i,:);
end
end

% =====Now update velocities and positions=====
for i = 1:swarmSize
    r1 = rand(1,nVar); r2 = rand(1,nVar);
    V(i,:) = w*V(i,:) + c1.*r1.*(pBest(i,:) -X(i,:)) +
c2.*r2.*(gBest - X(i,:));
%=====Constraints for velocity=====
V(i,:) = max(min(V(i,:), velMax), velMin);
X(i,:) = X(i,:) + V(i,:);
%=====Check bounds for min/max=====
X(i,:) = max(X(i,:),lb);
X(i,:) = min(X(i,:), ub);
end
% =====store convergence=====
convergence(iter) = gBestVal;
%=====
if mod(iter,50)==0 || iter==1
    fprintf('Iter %d best CEED+penalty = %.4f\n',iter, gBestVal);
end
end
%=====global and Personal best=====
best = gBest;
Pbest = best(1:n);
Tbest = best(n+1);
[~,details]=
objective_funPSO(best,n,Pmin,Pmax,Tmin,Tmax,PD,Pwind,a,b,c,d,e,f,h,B_area,p
enalty_factor);
%% =====Fuel cost,emissioncosts,ceed_per_gen,fuelcost_total=====
fuelcosts = a.*(Pbest.^2) + b.*Pbest + c;
emissioncosts = d.*(Pbest.^2) + e.*Pbest + f;
ceed_per_gen = fuelcosts + h.*emissioncosts;
fuelcost_total = sum(fuelcosts);
emission_total = sum(emissioncosts);
ceed_total = sum(ceed_per_gen);
% =====Transmission losses=====
try
    B_area11 = permute(reshape(B_area,3,2,[]),[1 3 2]);
    P_resch = reshape(Pbest,3,1,[]);
    PL_area = bsxfun(@times,P_resch,reshape(P_resch,1,3,[])).*B_area11;
    PLvec = sum(reshape(PL_area,[],2));
catch
    PLvec = [0.001, 0.001];
end
P1 = Pbest(1:3); P2 = Pbest(4:6);
sumP1 = sum(P1); sumP2 = sum(P2);

fprintf('\n=====PSO results summary=====\n');

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fprintf('Iterations performed: %d\n',maxIter);
fprintf('Best tie-line (T) = %.4f MW (positive: area1 -> area2\n',Tbest);
fprintf('Generator dispatch (P1..P6) [MW]:\n'); disp(Pbest');
fprintf('Area1 generation sum = %.4f MW, Area2 generation sum = %.4f MW\n',
sumP1,sumP2);
fprintf('Expected Wind per area (MW):\n'); disp(Pwind');
fprintf('Transmission losses per area (MW):'); disp(PLvec);
fprintf('Total Fuel cost = %.4f\n',fuelcost_total);
fprintf('Total Emission cost = %.4f\n',emission_total);
fprintf('Total CEED (fuel + h*emission) = %.4f\n', ceed_total);
fprintf('Power balance residuals area1, area2: [res1 res2] = [%.6f
%.6f\n',details.residuals);
toc
%=====  

figure  

plot(1:maxIter,convergence, 'lineWidth', 1.5);  

xlabel('Iteration'); ylabel('Best objective (CEED + penalties)');  

title('PSO Convergence');  

grid on;

finalvalue = [Pbest sum(Pwind(:,:)) sum(PLvec(:,:)) fuelcost_total  

emission_total ceed_total];
finalvalue'  

digits(6)  

vpa(finalvalue')
%=====  

MAWTEED_casePSO6units=====
function [objVal, details] =  

objective_funPSO(X,n,Pmin,Pmax,Tmin,Tmax,PD,Pwind,a,b,c,d,e,f,h,B_area,pena  

lty_factor)  

Pgen = X(1:n); % Generator outputs  

T = X(n+1);% Tie line flow  

%=====  

Pgen = max(Pgen,Pmin);  

Pgen = min(Pgen,Pmax);  

T = max(min(T,Tmax),Tmin);  

%=====  

%=====  

P1 = Pgen(1:3);  

P2 = Pgen(4:6);  

%=====  

%=====  

fuelcosts = a.*(Pgen.^2) + b.*Pgen + c;  

emission = d.*(Pgen.^2) + e.*Pgen + f;  

ceed_per_gen = fuelcosts+h.*emission;  

fuel_total = sum(fuelcosts);  

emission_total = sum(emission);  

ceed_total = sum(ceed_per_gen);  

%=====  

%=====  

try  

B_area11 = permute(reshape(B_area,3,2,[]),[1 3 2]);  

P_res = reshape(Pbest,3,1,[]);  

PL_area = bsxfun(@times,P_res,reshape(P_res,1,3,[])).*B_area11;  

PLvec = sum(reshape(PL_area,[],2));  

catch  

PLvec = [0.001, 0.001];  

end  

%=====  

%=====  

%=====  

balance1 = sum(P1) + Pwind(1)-PD(1)-PLvec(1)-T;  

%=====  

%=====  


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balance2 = sum(P2) + Pwind(2)-PD(2)-PLvec(2)+T;
residuals = [balance1, balance2];
%=====Calcualtion of penalty=====
penalty = penalty_factor*(residuals(1)^2 + residuals(2)^2);
%=====Final objective value=====
objVal = ceed_total + penalty;
%=====
%=====Values under variable name: details=====
details.fuel_total = fuel_total;
details.emission_total = emission_total;
details.ceed_total = ceed_total;
details.PLvec = PLvec;
details.residuals=residuals;
details.Pgen = Pgen;
details.T = T;
%=====
end

```

APPENDIX D2: MATLAB script file – MAWTEED_casePSO12units.m

```

%=====
%Main program name: MAWTEED_casePSO12units
%=====WTEED problem with 12 generators and 4 areas, 3 generators
%in each areas with wind power 330MW. This program isused to create table
%6.3, and used in table 6.4 as well. It is used with the function
%objective_funPSO_4area.m
clearvars;clc;close all;tic;
%=====Problem Data=====
m=4; % No of areas
n=12; % Total No of Generators in all the area
NG=3; % No of Generators in each area
TL=6; % NO of Tie lines
PD=[499.9280 410.0580 579.9750 600.0390]; % Area power demand

%=====Generator limits=====
Pmin = [35 130 125 10 35 125 15 30 50 15 30 50];
Pmax = [210 325 315 150 110 215 175 215 335 175 215 335];
%=====
%%=====Multi area Generator fuel Cost coefficients=====
a={[0.03546 0.02111 0.01799],[0.15247 0.02803 0.14834],...
  [0.10587 0.07505 0.11934],[0.10587 0.13552 0.08963]};
b={[38.30553 36.32782 38.27041],[38.53973 40.39655 38.34001],...
  [46.15916 43.83562 50.63211],[46.15916 41.03782 33.56211]};
c={[1243.5311 1658.5696 1356.6592],[0756.7989 0449.9977 0558.5696],...
  [0451.3251 0673.0267 0530.7199],[0851.3251 1038.533 1285.907]};
%=====Multi area Emission coefficients=====
d={[0.00683 0.00461 0.00461],[0.00484 0.00754 0.00661],...
  [0.00914 0.00533 0.00674],[0.00728 0.00479 0.00387]};
e={[ -0.54551 -0.51160 -0.51160],[ -0.32767 -0.54551 -0.63262],...
  [ -0.43211 -0.61173 -0.49731],[ -0.6821 -0.50660 -0.49340]};

f={[40.26690 42.89553 42.89553],[33.85932 50.639310 45.83267],...
  [48.21560 52.45210 41.10420],[30.36320 25.17650 27.75490]};
%=====Tie line limits=====
PTmin_mj=[5 5 5 5 5 5];
PTmax_mj=[60 50 60 60 60 50];
%=====
B_area=[ 0.000071 0.00003 0.000025
         0.00003 0.000069 0.000032
         0.000025 0.000032 0.00008
         0.000056 0.000045 0.000015

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0.000023 0.000042 0.000047
0.000032 0.000023 0.000027
0.00002 0.000028 0.000053
0.000086 0.000034 0.000016
0.000053 0.000016 0.000028
0.000074 0.000003 0.000025
0.000049 0.000069 0.000037
0.000022 0.000032 0.000083];
B_area1={B_area((1:3),:),B_area((4:6),:),B_area((7:9),:),B_area((10:12),:)}
;
%=====  

h = cell(1,m);
for i = 1:m
    h{i} = (a{i}.*Pmax((i-1)*NG+(1:NG)).^2 + b{i}.*Pmax((i-1)*NG+(1:NG)) +  

c{i})./... (d{i}.*Pmax((i-1)*NG+(1:NG)).^2 + e{i}.*Pmax((i-1)*NG+(1:NG)) +  

f{i});
end
%=====  

windData = {[9.891 10.785 6.861 14.482 12.184 4.602];...  

[8.5 7.2 6.9 10.4 12.1 5.8];...  

[7.3 8.6 6.2 11.0 9.8 4.5];...  

[6.5 7.9 5.1 9.2 8.7 4.0]};
Prated = [215 210 210 210]; %Rated wind power per area in (MW)
Vin = 5; Vr = 15; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
for area = 1:m
    v0 = windData{area}';
    pwind = fitdist(v0,'Weibull');
    %=====  

    pwvbins = zeros(size(vbins));
    pwvbins(vbins>=Vin & vbins<Vr)= Prated(area).*...  

((vbins(vbins>=Vin & vbins<Vr).^2 - Vin^2) / (Vr^2 - Vin^2));
    pwvbins(vbins>=Vr & vbins<=Vout) = Prated(area);
%=====  

    pdfv = pdf(pwind,vbins);
    avgpower = trapz(vbins,pdfv .*pwvbins);
    fprintf('Area %d: Expected Wind ≈ %.2f MW\n',area,avgpower);
    for s =1:Ns
        v = random(pwind);
        if v<Vin
            Pw = 0;
        elseif v < Vr
            Pw = Prated(area) * ((v^2 - Vin^2)/(Vr^2 - Vin^2));
        elseif v < Vout
            Pw = Prated(area);
        else
            Pw = 0;
        end
        TotalwindPower(area,s) = Pw;
    end
end
%=====  

Pwind_exp = mean(TotalwindPower,2);
Pwind = Pwind_exp; % Expected wind power

%%=====  

nVar = n +TL; % 12 generators + 6 tie-lines
lb = [Pmin,PTmin_mj]; ub = [Pmax,PTmax_mj];
swarmSize = 100; maxIter = 500; w = 0.9; c1 = 2; c2 = 2;

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Vmax = 0.2*(ub-lb); Vmin = -Vmax;
penalty_factor = 1e6;
%=====initialization of PSO variable and preallocation=====
X = repmat(lb,swarmSize,1) + rand(swarmSize,nVar) .* (repmat(ub-lb,
swarmSize,1));
V = zeros(swarmSize,nVar);
pBest = X;
pBestVal = inf(swarmSize,1);
gBest = zeros(1,nVar);
gBestVal = inf;
convergence = zeros(maxIter,1);
%%=====PSO main loop=====
rng('default');
for iter = 1:maxIter
    for i =1:swarmSize
        X(i,:) = max(X(i,:),lb);
        X(i,:) = min(X(i,:),ub);
%=====Evaluate the function =====
        [val, ~] =
objective_funPSO_4area(X(i,:),n,m,NG,TL,Pmin,Pmax,PTmin_mj,PTmax_mj,PD,Pwin
d,a,b,c,d,e,f,h,B_area1,penalty_factor);
%===== update pBest=====
        if val < pBestVal(i)
            pBestVal(i) = val;
            pBest(i,:) = X(i,:);
        end
%=====update global best=====
        if val < gBestVal
            gBestVal = val;
            gBest = X(i,:);
        end
    end
    % =====Now update velocities and positions=====
    for i = 1:swarmSize
        r1 = rand(1,nVar); r2 = rand(1,nVar);
        V(i,:) = w*V(i,:) + c1.*r1.*(pBest(i,:) -X(i,:)) + c2.*r2.*(gBest -
X(i,:));
%=====Constraints for
velocity=====
        V(i,:) = max(min(V(i,:), Vmax), Vmin);
        X(i,:) = X(i,:) + V(i,:);
%=====Check bounds for min/max=====
        X(i,:) = max(X(i,:),lb);
        X(i,:) = min(X(i,:), ub);
    end
    % =====store convergence=====
    convergence(iter) = gBestVal;
%=====
    if mod(iter,50)==0 || iter==1
        fprintf('Iter %d best CEED+penalty = %.4f\n',iter, gBestVal);
    end
end
%%=====Get the best solution=====
[~, details] =
objective_funPSO_4area(gBest',n,m,NG,TL,Pmin,Pmax,PTmin_mj,PTmax_mj,PD,Pwin
d,a,b,c,d,e,f,h,B_area1,penalty_factor);
fprintf('\n=====PSO Results Summary=====\n');
fprintf('Generator outputs [MW]:\n'); disp(details.Pgen);
fprintf('Tie-line flows[MW]:\n'); disp(details.Tlines);
fprintf('Expected Wind per area (MW):\n'); disp(Pwind');
fprintf('Transmission losses per area (MW):\n'); disp(details.PL_area);
fprintf('Total Fuel cost = %.4f\n',details.fuel_total);

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fprintf('Total Emission cost = %.4f\n',details.emission_total);
fprintf('Total CEED (fuel + h*emission) = %.4f\n', details.ceed_total);
fprintf('Losses = %.4f\n',details.PL_area);
% =====Convergence output
plot=====
figure
plot(1:maxIter,convergence, 'lineWidth', 1.5);
xlabel('Iteration'); ylabel('Best objective (CEED + penalties)');
title('PSO Convergence');
grid on;
% finalvalue = [gBest' sum(Pwind(:,:)) sum(PL_area(:,:)) fuel_total
emission_total ceed_total];
% finalvalue'
% digits(6)
% vpa(finalvalue')
toc
Totalwind = sum(Pwind(:,:))

%=====This is the objective function named: objective_funPSO_4area.m
%used with the main program: MAWTEED_casePSO12units
function [objVal, details] =
objective_funPSO_4area(X,n,m,NG,TL,Pmin,Pmax,PTmin_mj,PTmax_mj,PD,Pwind,a,b
,c,d,e,f,h,B_area1,penalty_factor)

%X =[P1..P12, T1..T6]
Pgen = X(1:n); % Generator outputs
Tlines = X(n+1:end);% Tie line flow
%=====Generator constraints=====
Pgen = max(Pgen,Pmin);
Pgen = min(Pgen,Pmax);
Tlines = max(min(Tlines,PTmax_mj),PTmin_mj);
%%=====Split generator outputs by area=====
P_area = cell(1,m);
% for i=1:m
for i =1:m
    idx = (i-1)*NG + (1:NG);
    P_area{i} = Pgen(idx);
end
%%=====Transmission losses=====
PL_area = zeros(1,m);
for i=1:m
    P_res = P_area{i}(:);
    PL_matrix = (P_res*P_res')*.B_area1{i};
    PL_area(i) = sum(PL_matrix(:));
end
%%=====Tie-line distribution to areas=====
T_area = zeros(1,m);
%=====distribution sum of tie lines=====
T_area(1) = sum(Tlines(1:TL/2)); % area1 receives or sends
T_area(2) = sum(Tlines(1:TL/2));% Area2
T_area(3) = sum(Tlines(TL/2+1:end)); %area3
T_area(4) = sum(Tlines(TL/2+1:end)); %area4

%%===== Calculation of the CEED problem=====
ceed_total=0;
fuel_total =0;
emission_total =0;
for i=1:m
    fuel = a{i}.*P_area{i}.^2 + b{i}.*P_area{i} + c{i};
    emission = d{i}.*P_area{i}.^2 + e{i}.*P_area{i} + f{i};
    ceed_per_gen = fuel + h{i}.*emission;
    fuel_total = fuel_total+ sum(fuel);

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```

    emission_total = emission_total + sum(emission);
    ceed_total = ceed_total + sum(ceed_per_gen);
end
%%=====Power balance equation=====
residuals = zeros(1,m);
for i=1:m
    residuals(i) = sum(P_area{i}) + Pwind(i) -PD(i)-PL_area(i)+T_area(i);
end
%%=====Penalty for power balance=====
penalty = penalty_factor*sum(residuals.^2);
%%=====Final objective=====
objVal = ceed_total + penalty;
%% =====Variables under details=====
details.Pgen = Pgen;
details.Tlines = Tlines;
details.P_area = P_area;
details.PL_area = PL_area;
details.residuals = residuals;
details.fuel_total = fuel_total;
details.emission_total = emission_total;
details.ceed_total = ceed_total;
end

```

APPENDIX D3: MATLAB script file – MAWTEED_casePSO40units.m

```

% Main program name: MAWTEED_casePSO40units. Program used in generating
% table 6.7 and also used in 6.8. Used with the function
named:objective_funPSO_2area
%%=====2-Area 40 Generator MAWTEED problem using
PSO=====
clearvars; clc; close all; tic;
%%=====Problem Data=====
m = 2; n = 40; TL =1;% arears, generators, and tie lines
PD = [7500 3000];% Power demand for both areas
%% =====Data are given in the reference paper (Basu, 2013)=====
%The data are given in the format[GenNum Pmin Pmax a b c d e f]=====
Data=[.....
1 36 114 0.0069 6.73 94.705 0.048 -2.22 60
2 36 114 0.0069 6.73 94.705 0.048 -2.22 60
3 60 120 0.02028 7.07 309.54 0.0762 -2.36 100
4 80 190 0.00942 8.18 369.03 0.054 -3.14 120
5 47 97 0.0114 5.35 148.89 0.085 -1.89 50
6 68 140 0.01142 8.05 222.33 0.0854 -3.08 80
7 110 300 0.00357 8.03 287.71 0.0242 -3.06 100
8 135 300 0.00492 6.99 391.98 0.031 -2.32 130
9 135 300 0.00573 6.6 455.76 0.0335 -2.11 150
10 130 300 0.00605 12.9 722.82 0.425 -4.34 280
11 94 375 0.00515 12.9 635.2 0.0322 -4.34 220
12 94 375 0.00569 12.8 654.69 0.0338 -4.28 225
13 125 500 0.00421 12.5 913.4 0.0296 -4.18 300
14 125 500 0.00752 8.84 1760.4 0.0512 -3.34 520
15 125 500 0.00752 8.84 1760.4 0.0496 -3.55 510
16 125 500 0.00752 8.84 1760.4 0.0496 -3.55 510
17 220 500 0.00313 7.97 647.85 0.0151 -2.68 220
18 220 500 0.00313 7.95 649.69 0.0151 -2.66 222
19 242 550 0.00313 7.97 647.83 0.0151 -2.68 220
20 242 550 0.00313 7.97 647.81 0.0151 -2.68 220
21 254 550 0.00298 6.63 785.96 0.0145 -2.22 290
22 254 550 0.00298 6.63 785.96 0.0145 -2.22 285
23 254 550 0.00284 6.66 794.53 0.0138 -2.26 295
24 254 550 0.00284 6.66 794.53 0.0138 -2.26 295

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25 254 550 0.00277 7.1 801.32 0.0132 -2.42 310
26 254 550 0.00277 7.1 801.32 0.0132 -2.42 310
27 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
28 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
29 10 150 0.52124 3.33 1055.1 1.842 -1.11 360
30 47 97 0.0114 5.35 148.89 0.085 -1.89 50
31 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
32 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
33 60 190 0.0016 6.43 222.92 0.0121 -2.08 80
34 90 200 0.0001 8.95 107.87 0.0012 -3.48 65
35 90 200 0.0001 8.62 116.58 0.0012 -3.24 70
36 90 200 0.0001 8.62 116.58 0.0012 -3.24 70
37 25 110 0.0161 5.88 307.45 0.095 -1.98 100
38 25 110 0.0161 5.88 307.45 0.095 -1.98 100
39 25 110 0.0161 5.88 307.45 0.095 -1.98 100
40 242 550 0.00313 7.97 647.83 0.0151 -2.68 220];
%% =====Multi area fuel cost coefficients=====
a=Data(:,4)'; a={a(1:20),a(21:40)};
b=Data(:,5)'; b={b(1:20),b(21:40)};
c=Data(:,6)'; c={c(1:20),c(21:40)};
%%=====Multi area Emmission coefficients=====
d=Data(:,7)'; d={d(1:20),d(21:40)};
e=Data(:,8)'; e={e(1:20),e(21:40)};
f=Data(:,9)'; f={f(1:20),f(21:40)};
%% =====Multi area Generator real power limits=====
Pmin=Data(:,2)'; Pmin1={Pmin(1:20),Pmin(21:40)};
Pmax=Data(:,3)'; Pmax1={Pmax(1:20),Pmax(21:40)};
%=====
% % Tie-line limits and coefficients
%=====Tie-line limits and coefficients=====
PTmin_mj = 100; PTmax_mj = 1500;
% PTmax_jm = 100; PTmax_jm = 1500;
% q_mj = rand; q_jm = rand;
% flr_jm = rand;
% alpha_mj = 0.01; alpha_jm = 0.01;
% =====Wind power data for each area=====
windData = {[9.891 10.785 6.861 14.482 12.184 4.602],[8.5 7.2 6.9 10.4 12.1
5.8]};
Prated = [220*3 0];
Vin = 3; Vr = 12; Vout = 25;
vbins = 0:0.5:30;
Ns = 50; %Number of scenarios
TotalwindPower = zeros(m,Ns);
Pwind_exp = zeros(m,1);
Pwind_limit = 330;% Wind power limits for system wind of 330MW
for area = 1:m
    v0 = windData{area}';
    pwind = fitdist(v0,'Weibull');
    %===== Power for each area=====
    pwvbins = zeros(size(vbins));
    pwvbins(vbins>=Vin & vbins<Vr)= Prated(area).*...
    ((vbins(vbins>=Vin & vbins<Vr).^2 - Vin^2) / (Vr^2 - Vin^2));
    pwvbins(vbins>=Vr & vbins<=Vout) = Prated(area);
    % =====Expected wind power=====
    pdfv = pdf(pwind,vbins);
    avgpower = trapz(vbins,pdfv .*pwvbins);
    Pwind_exp(area) = avgpower;
    fprintf('Area %d: Expected Wind = %.2f MW\n',area,avgpower);
    for s =1:Ns
        v = random(pwind);
        if v<Vin
            Pw = 0;

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elseif v < Vr
Pw = Prated(area) * ((v^2 - Vin^2)/(Vr^2 - Vin^2));
elseif v < Vout
Pw = Prated(area);
else
Pw = 0;
end
TotalwindPower(area,s) = Pw;
end
end
%=====Make sure the wind power doesnt reach 330MW==
totalExp = sum(Pwind_exp);
if totalExp > Pwind_limit
scaleFactor = Pwind_limit/totalExp;
Pwind_exp = Pwind_exp*scaleFactor;
TotalwindPower = TotalwindPower*scaleFactor;
fprintf('Whole wind limit: of the dispatch problem (%.2f)\n',scaleFactor);
end
%=====The expected wind power is =====
Pwind = Pwind_exp;
fprintf('Total expected wind after limit check: %.2f MW\n',sum(Pwind));
%% =====PSO Parameters=====
nVar = n +TL; % 12 generators + 6 tie-lines
lb = [Pmin,PTmin_mj]; ub = [Pmax,PTmax_mj];
swarmSize = 100; maxIter = 1000; w = 0.9; c1 = 2; c2 = 2;
Vmax = 0.2*(ub-lb); Vmin = -Vmax;
penalty_factor = 1000000;
%=====initialization of PSO variable and preallocation=====
X = repmat(lb,swarmSize,1) + rand(swarmSize,nVar) .* (repmat(ub-lb,
swarmSize,1));
V = zeros(swarmSize,nVar);
pBest = X;
pBestVal = inf(swarmSize,1);
gBest = zeros(1,nVar);
gBestVal = inf;
convergence = zeros(maxIter,1);
%%=====PSO main loop=====
rng('default');
for iter = 1:maxIter
for i =1:swarmSize
X(i,:) = max(X(i,:),lb);
X(i,:) = min(X(i,:),ub);
% [val, details] = objective_funPSO_2area(X(i,:), n, m, TL, PD,
Pwind, ...
% a,b,c,d,e,f,Pmin,Pmax, Pmin1,Pmax1,
q_mj,q_jm,alpha_mj,alpha_jm, flr_jm, penalty_factor);
[val, details] = objective_funPSO_2area(X(i,:), n, m, TL, PD, Pwind, ...
a,b,c,d,e,f,Pmin,Pmax,Pmin1,Pmax1,penalty_factor,PTmin_mj,PTmax_mj);
%===== update pBest=====
if val < pBestVal(i)
pBestVal(i) = val;
pBest(i,:) = X(i,:);
end
%=====update global best=====
if val < gBestVal
gBestVal = val;
gBest = X(i,:);
gBestDetails = details;
end
end
end
% =====Now update velocities and positions=====

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    for i = 1:swarmSize
        r1 = rand(1,nVar); r2 = rand(1,nVar);
        V(i,:) = w*V(i,:) + c1.*r1.*(pBest(i,:) -X(i,:)) + c2.*r2.*(gBest -
X(i,:));
        %=====Constraints for
velocity=====
        V(i,:) = max(min(V(i,:), Vmax), Vmin);
        X(i,:) = X(i,:) + V(i,:);
        %=====Check bounds for min/max=====
        X(i,:) = max(X(i,:),lb);
        X(i,:) = min(X(i,:), ub);
    end
    %=====store convergence=====
    convergence(iter) = gBestVal;
    %=====
    if mod(iter,50)==0 || iter==1
        fprintf('Iter %d best CEED+penalty = %.4f\n',iter, gBestVal);
    end
end
% [~, details] = objective_funPSO_2area(gBest', n, m, TL, PD, Pwind, ...
%     a,b,c,d,e,f,Pmin,Pmax, Pmin1,Pmax1, q_mj,q_jm,alpha_mj,alpha_jm,
flr_jm, penalty_factor);
[~, details] = objective_funPSO_2area(gBest', n, m, TL, PD, Pwind, ...
    a,b,c,d,e,f,Pmin,Pmax, Pmin1,Pmax1,
penalty_factor,PTmin_mj,PTmax_mj);
%%=====WTEED best solution=====
disp('=====PSO WTEED Results=====');
fprintf('Total Fuel cost = %.4f\n',gBestDetails.fuel_total);
fprintf('Total Emission cost = %.4f\n',gBestDetails.emission_total);
fprintf('Total CEED (fuel + h*emission) = %.4f\n',gBestDetails.ceed_total);
fprintf('Generator outputs per area [MW]:\n'); disp(gBestDetails.Pgen);
fprintf('Tie-line flows [MW]:\n'); disp(gBestDetails.Tlines);
fprintf('Expected Wind per area [MW]:\n'); disp(Pwind);
%=====Convergence output plot=====
figure
plot(1:maxIter,convergence, 'lineWidth', 1.5);
xlabel('Iteration'); ylabel('Best objective (CEED + penalties)');
title('PSO Convergence');
grid on;
%=====

%=====This is the objective function named: objective_funPSO_2area.m
%used with the main program: MAWTEED_casePSO40units

function [objVal, details] = objective_funPSO_2area(X, n, m, TL, PD, Pwind,
...
    a,b,c,d,e,f,Pmin,Pmax, Pmin1,Pmax1, penalty_factor,PTmin_mj,PTmax_mj)
%=====Objective function=====
Pgen = X(1:n);
T = X(n+1:end);% Tie line flows TL =1;
%=====Generator constraints=====
Pgen = max(Pgen,Pmin);
Pgen = min(Pgen,Pmax);
T = max(min(T,PTmax_mj),PTmin_mj);
%=====Split generator per area=====
P1 = Pgen(1:20);
P2 = Pgen(21:40);
%=====Fuel cost and Emission=====
fuelcosts = [a{1}.*P1.^2 + b{1}.*P1 + c{1},a{2}.*P2.^2 + b{2}.*P2 + c{2}];
emission = [d{1}.*P1.^2 + e{1}.*P1 + f{1},d{2}.*P2.^2 + e{2}.*P2 + f{2}];
%=====Penalty factor for the two areas=====

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h1 = (a{1}.*Pmax1{1}.^2 + b{1}.*Pmax1{1} + c{1})./ (d{1}.*Pmax1{1}.^2 +
e{1}.*Pmax1{1} + f{1});
h2 = (a{2}.*Pmax1{2}.^2 + b{2}.*Pmax1{2} + c{2})./ (d{2}.*Pmax1{2}.^2 +
e{2}.*Pmax1{2} + f{2});
h = [h1 h2];
ceed_per_gen = fuelcosts + h.*emission;
fuel_total = sum(fuelcosts);
emission_total = sum(emission);
ceed_total = sum(ceed_per_gen);
%=====Power balance residuals=====
balance1 = sum(P1)+ Pwind(1)+(-T)-PD(1); % Area 1 tie line export
balance2 = sum(P2)+ Pwind(2)+ (T)-PD(2); % Area 2 import tie line

residuals = [balance1, balance2];
%=====Penalty=====
penalty = penalty_factor* sum(residuals.^2);
%=====Objective value=====
objVal = ceed_total + penalty;

%=====Name under variable details=====
details.fuel_total = fuel_total;
details.emission_total = emission_total;
details.ceed_total = ceed_total;
details.residuals = residuals;
details.Pgen = {P1, P2};
details.Tlines = T;
end.
%=====

```